

# **Will It Support a Self-Propagating Fire?**

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**FM Global Research**

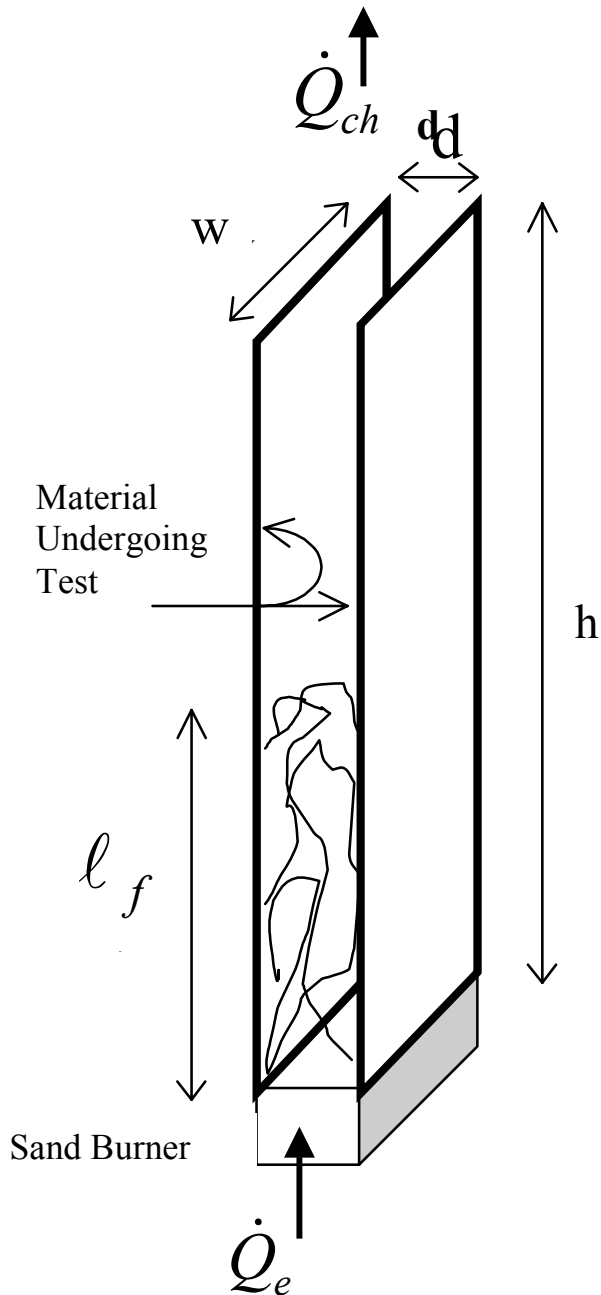
**NIST Workshop on Fire Growth and  
Spread on Objects**

**March 4-6, 2002**

## Regulators Desire

- Simple Tests
- Models Requiring a Minimum of Inputs
- Clear Pass/Fail Results

## Researchers Seek Understanding



Will the Fire Resistive Material Support a Self-Propagating Fire for a Given Exposure Fire  $\dot{Q}_e$  ?

A Quasi-Steady Model  
for the  
Parallel Panel Test.

## *Model Assumptions*

1. Heat Release per Unit Volume  $\dot{q}_{ch}''' = \text{const} = 2000 \text{ kW} / \text{m}^3$
2. Flame Volume and Height  $V_f = l_f w d$   $l_f = \frac{V_f}{w d} = \frac{\dot{Q}_{ch}}{\dot{q}_{ch}''' w d}$
3. Area of Sidewalls  $A_{sw} = 2 l_f w$   
Total Flame Area  $A_f = 2 l_f w + 2 l_f d + 2 w d$
4. Heat Transfer to Walls  $\frac{\dot{Q}_{sw}}{\dot{Q}_{ch}} = \frac{A_{sw}}{A_f} \chi$
5. Flame Heat Flux  $\dot{q}_f'' = \dot{Q}_{sw} / A_{sw}$

6. Fuel Mass Flux  $\dot{m}'' = (\dot{q}''_f - \dot{q}''_{loss}) / L$

7. Conservation of Energy  $\dot{Q}_{ch} = \dot{Q}_e + \Delta H_{ch} A_{sw} \dot{m}''$

## *Non-Dimensionalization*

$$\dot{Q}_{ch} = \dot{Q}_e + (\dot{q}''_f - \dot{q}''_{loss}) A_{sw} \Delta H_{ch} / L$$

$$\dot{Q}_{ch} = \dot{Q}_e + \dot{Q}_{ch} \chi \left( \frac{A_{sw}}{A_f} \right) \frac{\Delta H_{ch}}{L} - \dot{q}''_{loss} A_{sw} \frac{\Delta H_{ch}}{L}$$

$$\frac{\dot{Q}_{ch}}{\dot{q}'''_{ch} w^2 d} = \frac{\dot{Q}_e}{\dot{q}'''_{ch} w^2 d} + \frac{\dot{Q}_{ch} \chi}{\dot{q}'''_{ch} w^2 d} \left( \frac{A_{sw}}{A_f} \right) \frac{\Delta H_{ch}}{L} - \frac{\dot{q}''_{loss} A_{sw}}{\dot{q}'''_{ch} w^2 d} \frac{\Delta H_{ch}}{L}$$

Fire Size

$$\zeta_f = \frac{\ell_f}{w} = \frac{\dot{Q}_{ch}}{\dot{q}_{ch}''' w^2 d}$$

Exposure Fire Size

$$\zeta_e = \frac{\dot{Q}_e}{\dot{q}_{ch}''' w^2 d}$$

Surface Heat Loss

$$\gamma_{loss} = \frac{\dot{q}_{loss}''}{\dot{q}_{ch}''' d}$$

Parallel Panel Aspect Ratio

$$\alpha = d / w$$

Combustion Heat Gain

$$\Gamma = \frac{\Delta H_{ch}}{L}$$

## *Scaling the Aspect Ratio*

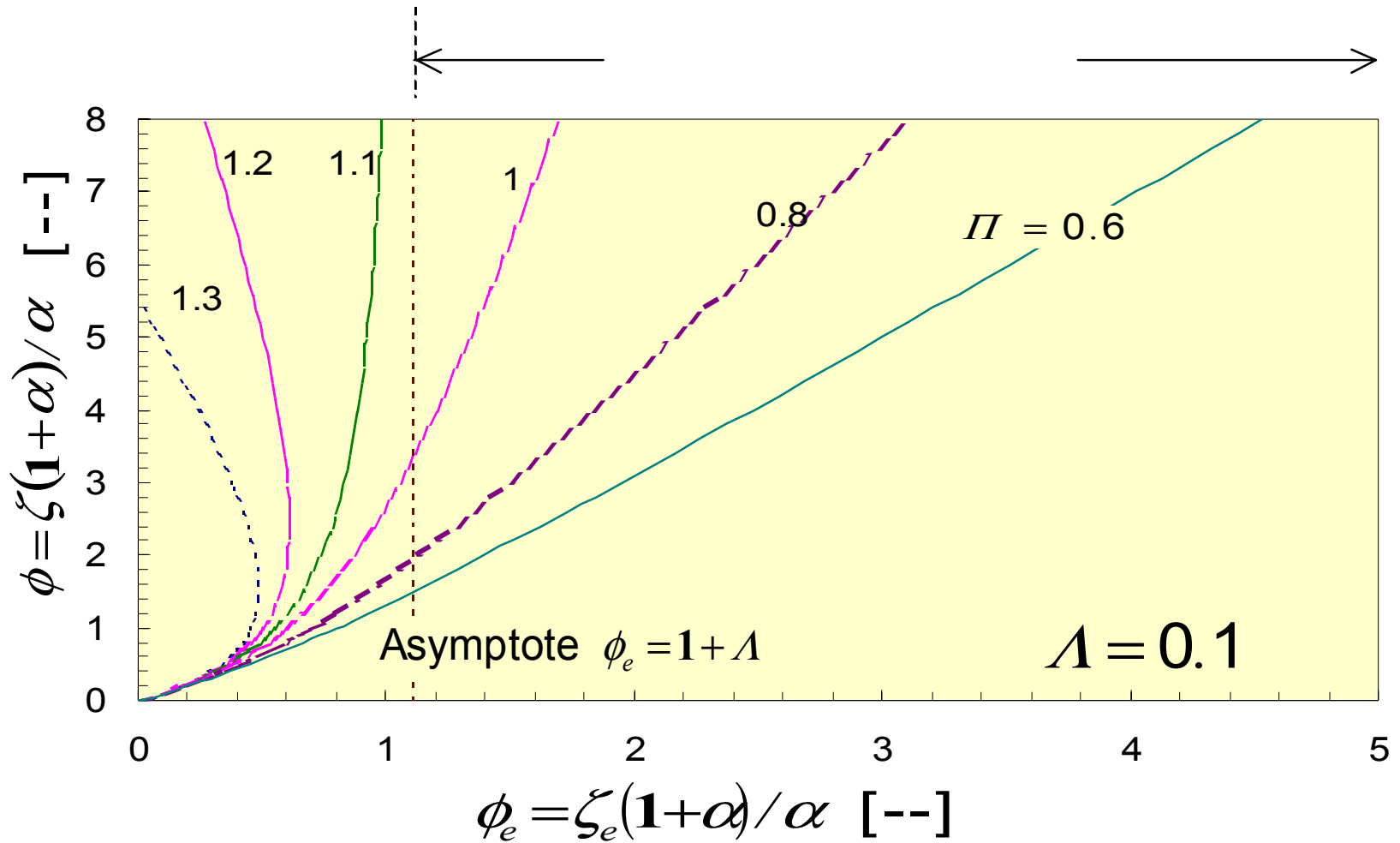
Scaled Fire Size  $\phi = \zeta_f (1 + \alpha) / \alpha$

Scaled Exposure Fire Size  $\phi_e = \zeta_e (1 + \alpha) / \alpha$

Scaled Flame Heat Flux  $\Pi = \frac{\chi \Gamma}{1 + \alpha}$

Scaled Heat Loss  $\Lambda = 2 \Gamma \gamma_{loss}$

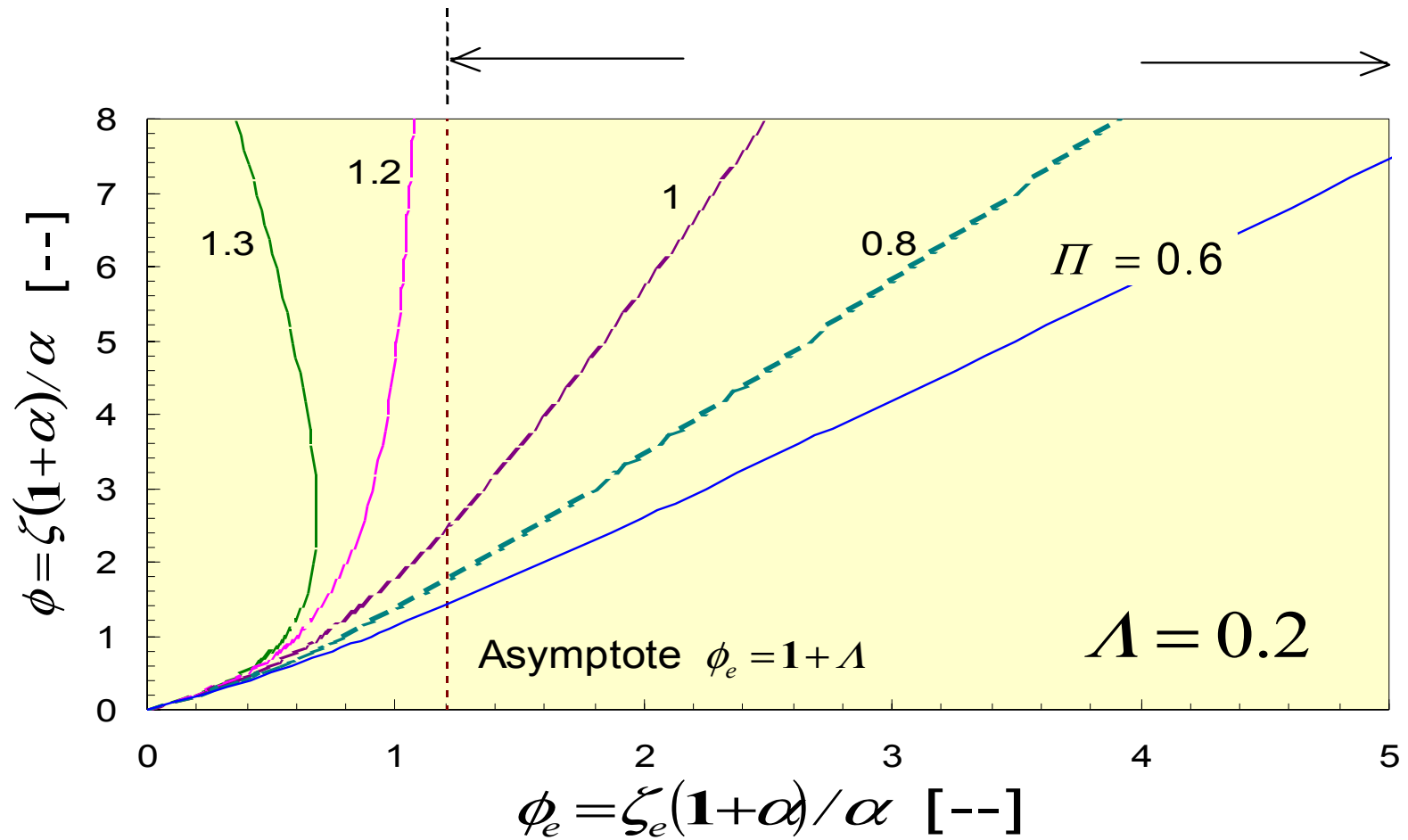
Governing Equation  $\phi = \phi_e + \frac{\phi^2 \Pi}{\phi + 1} - \Lambda \phi$



## Scaled Fire Size vs. Scaled Exposure Fire Size

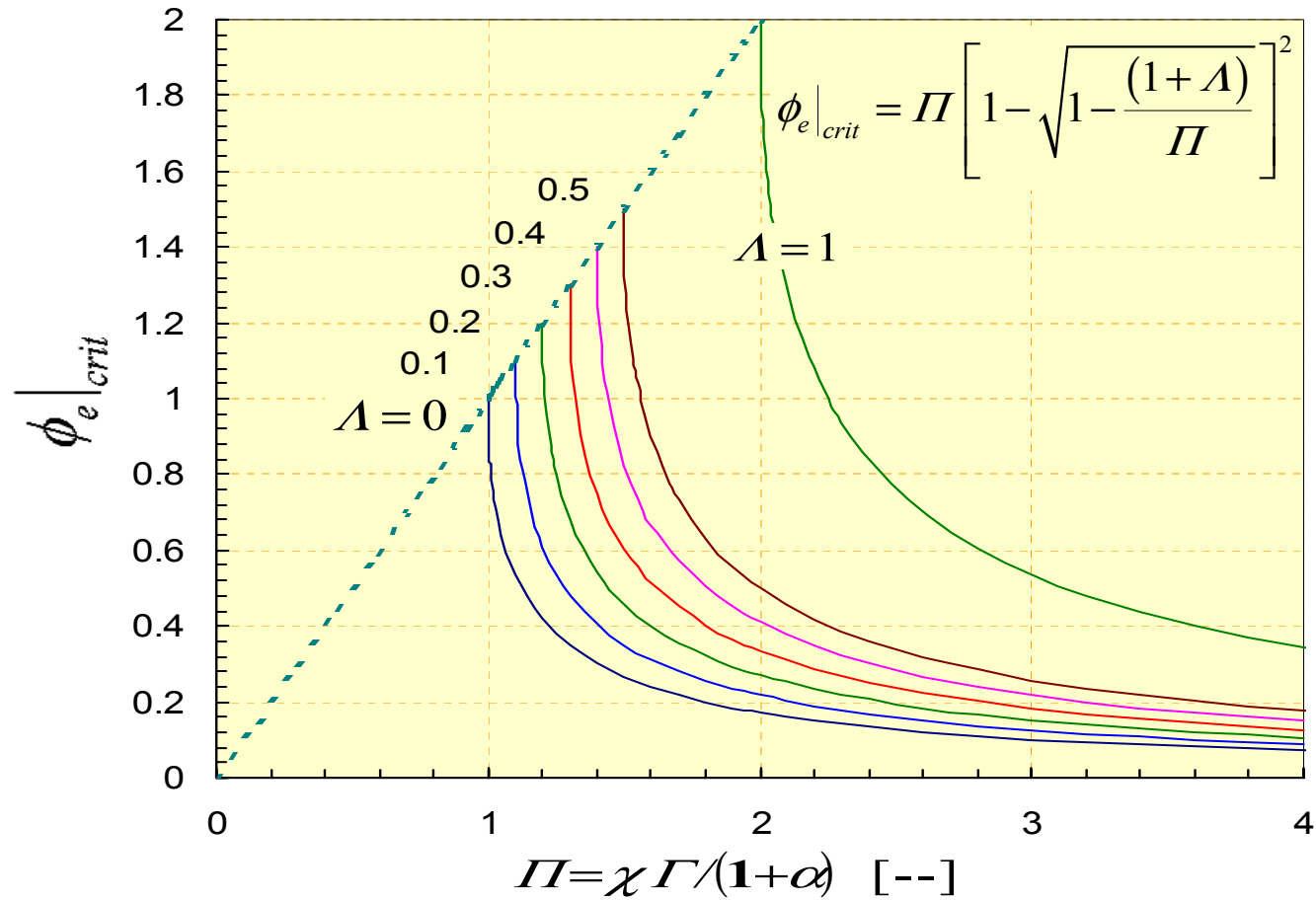
for Various Scaled Flame Heat Fluxes  
 and a Fixed Scaled Heat Loss  $\Lambda=0.1$





## Scaled Fire Size vs. Scaled Exposure Fire Size

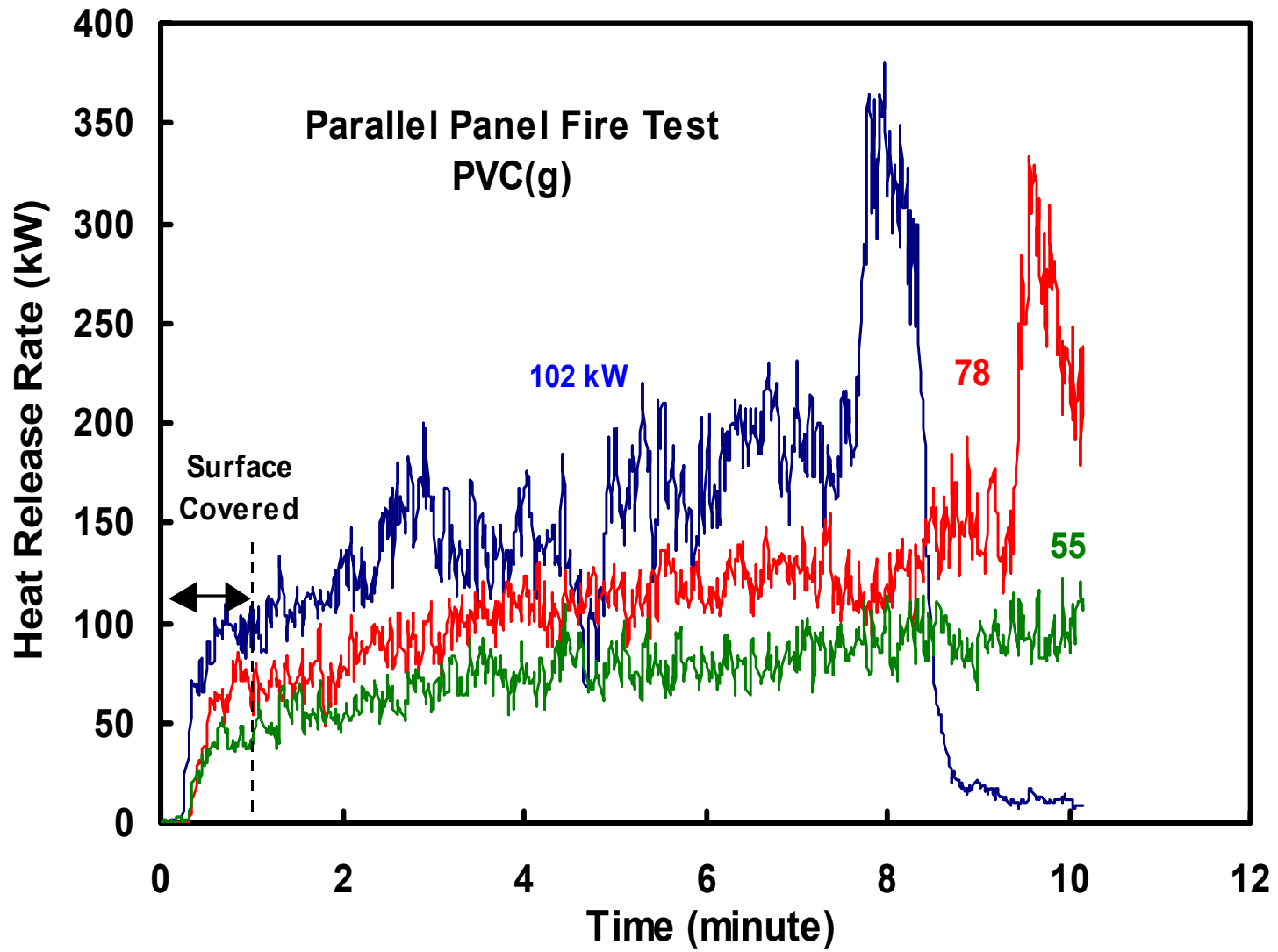
for Various Scaled Flame Heat Fluxes  
 and a Fixed Scaled Heat Loss  $\Lambda=0.2$

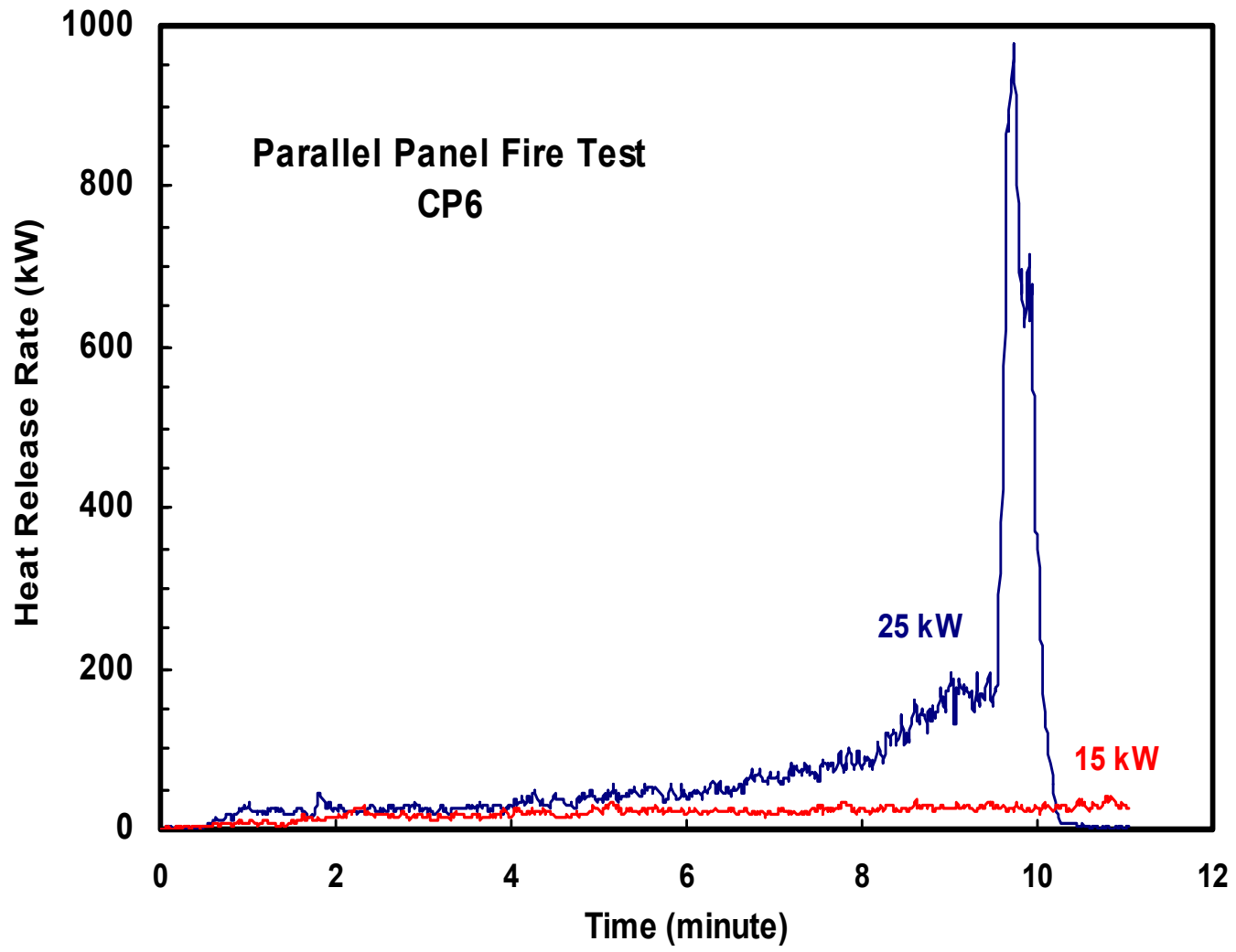


Critical Scaled Exposure Size Leading to Run Away Fire Growth

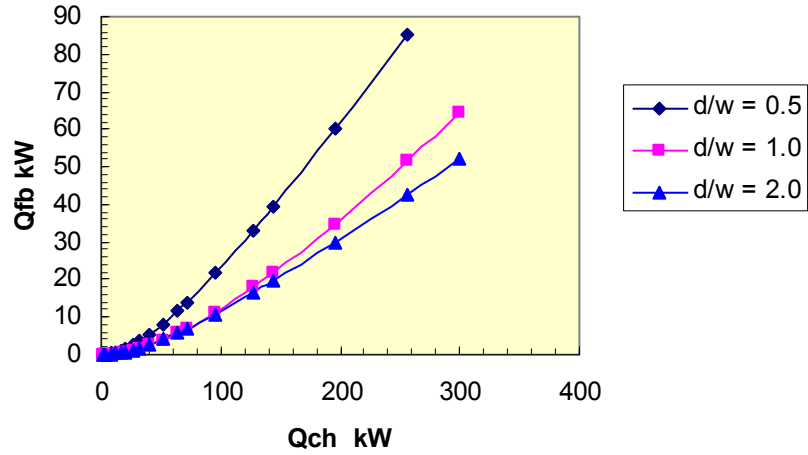
$T_s$ 

Property	Symbol	Unit	PMMA	PVC(g)	CP-6
Heat of Combustion	$\Delta H_{ch}$	kJ/g	24.9	7.0	19.0
Heat of Gasification	$L$	kJ/g	1.61	2.63	5.9
Heat Gain	$\Gamma = \Delta H_{ch} / L$	[ -- ]	15.5	2.66	3.22
Surface Heat Loss	$\dot{q}''_{loss}$	kW/m <sup>2</sup>	10.7	12.5	18.4
Surface Temperature	$T_s$	K	658	685	755
Surface Enthalpy	$C_p (T_s - T_\infty)$	kJ/g	0.46	0.48	0.57
B-Number	$B = [\Delta H_{air} - C_p (T_s - T_\infty)] / L$	[ -- ]	1.57	0.96	.41
Blockage	$\chi = \ln(1 + B) / B$	[ -- ]	0.60	0.70	0.84
Smoke Yield	$y_s = \dot{g}_{smoke} / \dot{g}_{fuel-vaporized}$	[ -- ]	.02	0.116	0.090
Surface Loss	$\gamma_{loss} = \frac{\dot{q}''_{loss}}{\dot{q}'''_{ch} d}$ for $d = 0.3$ m, $\dot{q}'''_{ch} = 2000$ kW / m <sup>3</sup>	[ -- ]	0.017	0.0208	0.0307
<b>Scaled Heat Flux</b>	$\Pi = \frac{\chi \Gamma}{1 + \alpha}$ for $\alpha = 0.5$	[ -- ]	<b>6.2</b>	<b>1.24</b>	<b>1.8</b>
<b>Scaled Heat Loss</b>	$\Lambda = 2 \Gamma \gamma_{loss}$	[ -- ]	<b>0.53</b>	<b>0.11</b>	<b>0.20</b>

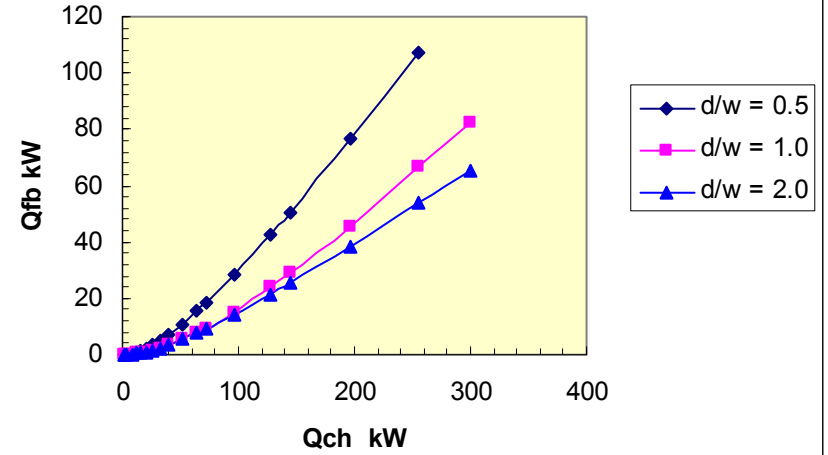




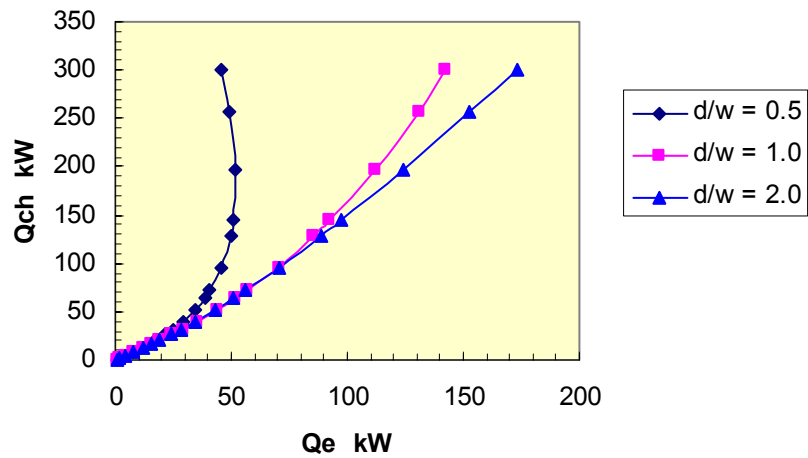
### Heat Feedback to Walls - PVC(g)



### Heat Feedback to Walls - CP-6



### Overall Heat Release - PVC(g)



### Overall Heat Release - CP-6

