

# Simulation of Runoff and Water Quality for 1990 and 2008 Land-Use Conditions in the Reedy Creek Watershed, East-Central Florida

**U.S. GEOLOGICAL SURVEY**

Water-Resources Investigations Report 02-4018

Prepared in cooperation with the  
**Reedy Creek Improvement District**



Cover photographs by Eddie Snell,  
Reedy Creek Improvement District, Florida.

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By Shaun M. Wicklein and Donna M. Schiffer

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Tallahassee, Florida  
2002

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For additional information write to:

District Chief  
U.S. Geological Survey, WRD  
Suite 3015  
227 North Bronough Street  
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CONVERSION FACTORS, VERTICAL DATUM, ABBREVIATIONS AND ACRONYMS

Multiply	By	To obtain
<i>Length</i>		
inch (in.)	2.54	centimeter
foot (ft)	0.3048	meter
mile (mi)	1.609	kilometer
<i>Area</i>		
square foot (ft <sup>2</sup> )	0.0929	square meter
square mile (mi <sup>2</sup> )	2.590	square kilometer
square mile (mi <sup>2</sup> )	259	hectare
acre	0.405	hectare
<i>Mass</i>		
pound (lb)	0.4536	kilogram
<i>Flow</i>		
cubic foot per second (ft <sup>3</sup> /s)	0.02832	cubic meter per second
inch per year (in/yr)	25.4	millimeter per year

Temperature in degrees Fahrenheit (°F) may be converted to degrees Celsius (°C) as follows: °C=(°F-32)/1.8

**Sea level:** In this report, “sea level” refers to the National Geodetic Vertical Datum of 1929 (NGVD of 1929)-- a geodetic datum derived from a general adjustment of the first-order level nets of both the United States and Canada, formerly called Sea Level Datum of 1929.

**Altitude:** In this report, altitude refers to distance above or below sea level.

Horizontal coordinate information is referenced to the North American Datum of 1927 (NAD27).

Acronyms and additional abbreviations used in report:

BASINS	Better Assessment Science Integrating Point and Nonpoint Sources
BMP	best management practices
BOD	biochemical oxygen demand
DO	dissolved oxygen
ET	evapotranspiration
GIS	Geographic Information System
HSPF	Hydrologic Simulation Program-Fortran
HSPEXP	Hydrological Simulation Program-Fortran EXPert system
IMPLND	impervious land surfaces
mg/L	milligrams per liter
NAPD/NTN	National Atmospheric Deposition Program/National Trends Network
NURP	Nationwide Urban Runoff Project
NOAA	National Oceanic and Atmospheric Administration
PERLND	pervious land surfaces
R <sup>2</sup>	a coefficient of determination
RCID	Reedy Creek Improvement District
RIBS	rapid infiltration basins
USEPA	U.S. Environmental Protection Agency
USGS	U.S. Geological Survey
UCI	user control input

# Simulation of Runoff and Water Quality for 1990 and 2008 Land-Use Conditions in the Reedy Creek Watershed, East-Central Florida

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## ABSTRACT

Hydrologic and water-quality data have been collected within the 177-square-mile Reedy Creek, Florida, watershed, beginning as early as 1939, but the data have not been used to evaluate relations among land use, hydrology, and water quality. A model of the Reedy Creek watershed was developed and applied to the period January 1990 to December 1995 to provide a computational foundation for evaluating the effects of future land-use changes on hydrology and water quality in the watershed.

The Hydrological Simulation Program-Fortran (HSPF) model was used to simulate hydrology and water quality of runoff for pervious land areas, impervious land areas, and stream reaches. Six land-use types were used to characterize the hydrology and water quality of pervious and impervious land areas in the Reedy Creek watershed: agriculture, rangeland, forest, wetlands, rapid infiltration basins, and urban areas. Hydrologic routing and water-quality reactions were simulated to characterize hydrologic and water-quality processes and the movement of runoff and its constituents through the main stream channels and their tributaries.

Because of the complexity of the stream system within the Reedy Creek Improvement District (RCID) (hydraulic structures, retention ponds) and the anticipated difficulty of modeling the system, an approach of calibrating the model parameters for a subset of the gaged watersheds and confirming the usefulness of the parameters by simulating the remainder of the gaged sites was selected for this study. Two sub-watersheds (Whittenhorse Creek and Davenport Creek) were selected for calibration because both have similar land use to watersheds within the RCID (with the exception of urban areas). Given the lack of available rainfall

data, the hydrologic calibration of the Whittenhorse Creek and Davenport Creek sub-watersheds was considered acceptable (for monthly data, correlation coefficients, 0.86 and 0.88, and coefficients of model-fit efficiency, 0.72 and 0.74, respectively). The hydrologic model was tested by applying the parameter sets developed for Whittenhorse Creek and Davenport Creek to other land areas within the Reedy Creek watershed, and by comparing the simulated results to observed data sets for Reedy Creek near Vineland, Bonnet Creek near Vineland, and Reedy Creek near Loughman. The hydrologic model confirmation for Reedy Creek near Vineland (correlation coefficient, 0.91, and coefficient of model fit efficiency, 0.78, for monthly flows) was acceptable. Flows for Bonnet Creek near Vineland were substantially under simulated. Consideration of the ground-water contribution to Bonnet Creek could improve the water balance simulation for Bonnet Creek near Vineland. On longer time scales (monthly or over the 72-month simulation period), simulated discharges for Reedy Creek near Loughman agreed well with observed data (correlation coefficient, 0.88). For monthly flows the coefficient of model-fit efficiency was 0.77. On a shorter time scale (less than a month), however, storm volumes were greatly over simulated and low flows (less than 8 cubic feet per second) were greatly under simulated. A primary reason for the poor results at low flows is the diversion of an unknown amount of water from the RCID at the Bonnet Creek near Kissimmee site.

Selection of water-quality constituents for simulation was based primarily on the availability of water-quality data. Dissolved oxygen, nitrogen, and phosphorus species were simulated. Representation of nutrient cycling in HSPF also required simulation of biochemical oxygen demand and phytoplankton



populations. The correlation coefficient for simulated and observed daily mean dissolved oxygen concentration values at Reedy Creek near Vineland was 0.633. Simulated time series of total phosphorus, phosphate, ammonia nitrogen, and nitrate nitrogen generally agreed well with periodically observed values for the Whittenhorse Creek and Davenport Creek sites. Simulated water-quality constituents at the Bonnet Creek and Reedy Creek near Vineland sites varied as to how well the values agreed with periodically observed constituent concentrations. Simulated water-quality constituent concentrations for the Reedy Creek near Loughman site generally agreed well with observed constituent concentrations.

Simulation of a future land-use scenario for the Reedy Creek watershed was based on the hydrologic and water-quality simulations, projected 2008 land use within the RCID, and assuming no change in existing land use for other areas within the Reedy Creek watershed but external to the RCID. The percentages of forest and urban-impervious land use showed the most change between existing and future land use; forest areas decreased by 50 percent and urban-impervious areas increased by 300 percent. Simulated values of mean total phosphorus, phosphate, ammonia nitrogen, and nitrate nitrogen concentrations for existing and future land-use simulations were within 0.01 milligrams per liter of each other. The simulated maximum daily load increased an average of 10 percent for all constituents. Maximum daily nitrate nitrogen load increased about 17 percent, the greatest increase of all daily constituent loads. Duration curves of daily total phosphorus, phosphate, ammonia nitrogen, and nitrate nitrogen load indicated an increase in the likelihood of exceeding a given load throughout the range of daily constituent loads at Reedy Creek near Loughman.

## INTRODUCTION

Land use in central Florida has been greatly modified as a result of population increases and industrial growth. Since the 1960's, one of the most intensely modified land areas in central Florida has been the 177-square-mile (mi<sup>2</sup>) Reedy Creek watershed, in southwest Orange, northwest Osceola, northeast Polk, and southwest Lake Counties. The Reedy Creek Improvement District (RCID) is an area of about 45 mi<sup>2</sup> within the Reedy Creek watershed (fig. 1). Land use affects both the hydrology and water

quality of runoff from the watershed, but the effects are not easily quantified.

Although hydrologic and water-quality data have been collected within the Reedy Creek watershed and the RCID since as early as 1939, the data have not previously been used to evaluate the relations among land use, hydrology, and water quality. Changes in land use over time, due to land development, in the Reedy Creek watershed make predicting changes in hydrology and water quality difficult. Because of the natural variability of hydrologic and water-quality data, the spatial variability within watersheds, and the complexity of nutrient runoff and transport relations, it is difficult to relate specific watershed properties to conditions downstream unless the watershed is analyzed as a system. Watershed modeling can be used to better understand the relation of land use to hydrologic and water-quality processes occurring within a watershed. A continuous-simulation watershed model can provide the framework for understanding the relations among land use and water quantity and quality within the Reedy Creek watershed and the RCID. The U.S. Geological Survey (USGS) began a 5-year study in 1996 in cooperation with the RCID to better define the relations among land use, hydrology, and water quality in the Reedy Creek watershed.

## Purpose and Scope

This report presents results of a study to evaluate and simulate rainfall-runoff relations and nutrient concentrations and loads within the Reedy Creek watershed, including the RCID. The Reedy Creek watershed was divided into sub-watersheds, and the hydrologic characteristics that control runoff were determined. Although the primary focus of the study was to simulate the hydrology and water quality within the RCID, the hydrology and water quality of the Reedy Creek watershed was modeled because changes outside the RCID also affect nutrient concentrations and loads within and downstream from the RCID. This report presents land-use, hydrologic, meteorological, and water-quality data used to calibrate and confirm the watershed model. Calibration and confirmation of a rainfall-runoff model, the Hydrological Simulation Program-Fortran (HSPF) (Bicknell and other, 1993), are described. Building on the hydrologic model, results of the water-quality simulation of the watershed are described. The period from January 1990 to December 1995 was simulated.

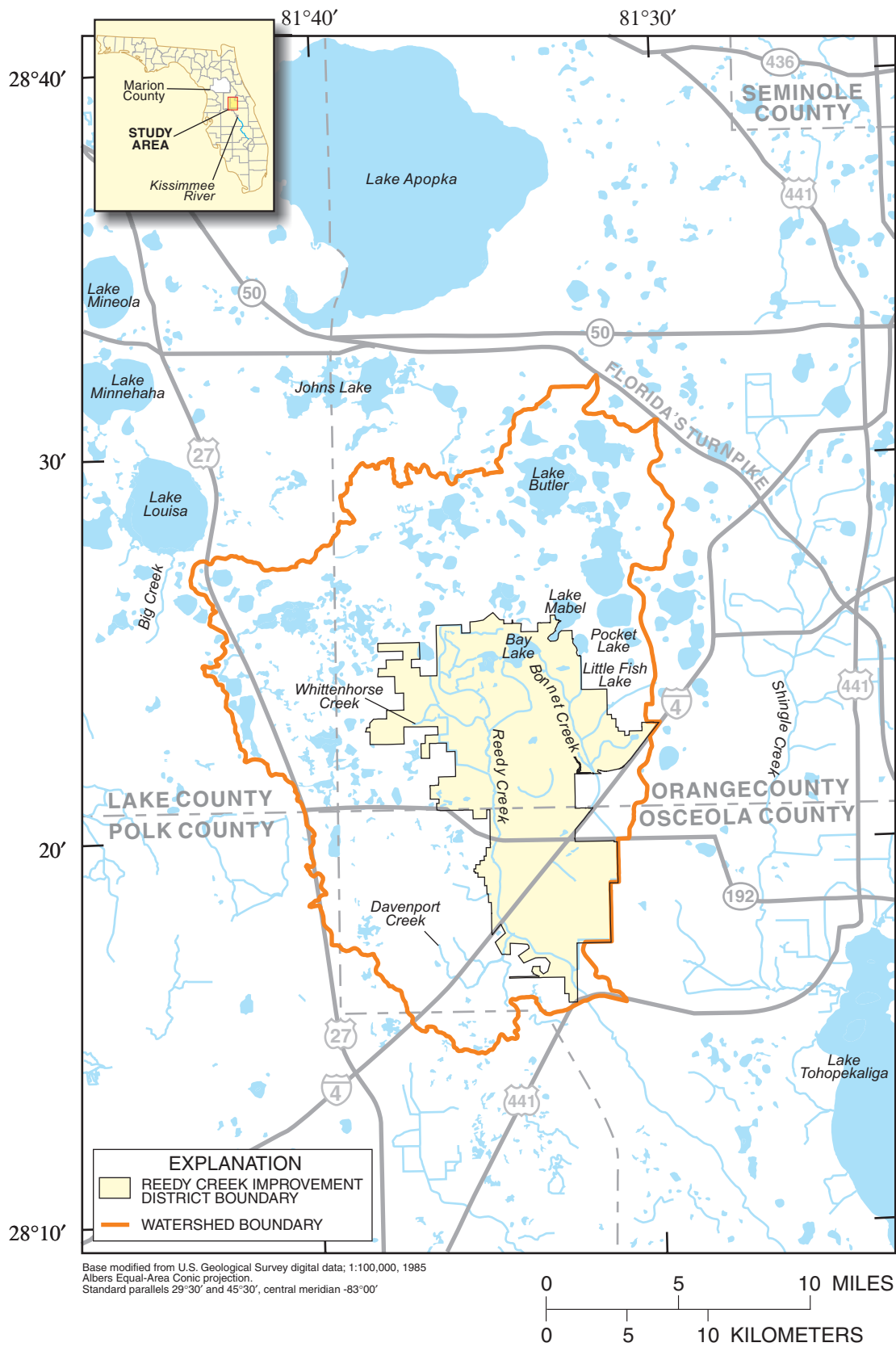


Figure 1. Location of study area.

The effects of projected future land-use changes within the RCID were evaluated by revising the calibrated model to reflect projected 2008 land use and comparing the output with the results obtained from simulation of hydrology and water quality of runoff from existing land use (1990). An overall evaluation of modeling results and a discussion of possible ways to improve the model are presented.

## Previous Investigations

Putnam (1975) summarized the hydrology and water quality of the Reedy Creek watershed and the RCID, along with effects of development from 1966 to 1973. German (1986) continued the appraisal of water resources and effects of land-use changes in the RCID from 1966 to 1980. Estimated daily loads of dissolved solids and selected nutrient species into and out of an undeveloped area in the Reedy Creek watershed south of the developed areas from June 1986 through May 1987 were described by German (1989). Hampson (1993) described the hydrology and water quality of Reedy Creek within the RCID for the period 1986-89, and investigated the input and output nutrient loads for a wetland conservation area in the southern part of the RCID resulting from wastewater discharges. Hampson's (1993) work also included several reaeration studies on Reedy Creek downstream from developed areas. German (1990) investigated the effects of land application of treated wastewater on ground-water quality in part of the RCID. Sumner and Bradner (1996) investigated the effects of reclaimed wastewater disposal through rapid infiltration basins (RIBS) on nutrients in ground water and in the unsaturated zone. A ground-water flow model of the western part of the RCID in an area affected by disposal of treated wastewater through irrigation and through RIBS was used to evaluate effects on the surficial aquifer system and surface water as well as the Floridan aquifer system (O'Reilly, 1998). Gee and Jenson (1990) produced a Master Drainage Plan for the RCID stormwater facilities, which the RCID Planning and Engineering Department periodically updates.

Numerous reports on the surface- and ground-water resources of central Florida, including the Reedy Creek watershed, also are available. Tibbals (1990) simulated ground-water flow in the Floridan aquifer system in east-central Florida. Murray and Halford (1996) described hydrogeologic conditions in east-central Florida, calibrated a ground-water flow model

to steady-state 1988 conditions, and evaluated the effects of projected 2010 withdrawals on the Floridan aquifer system.

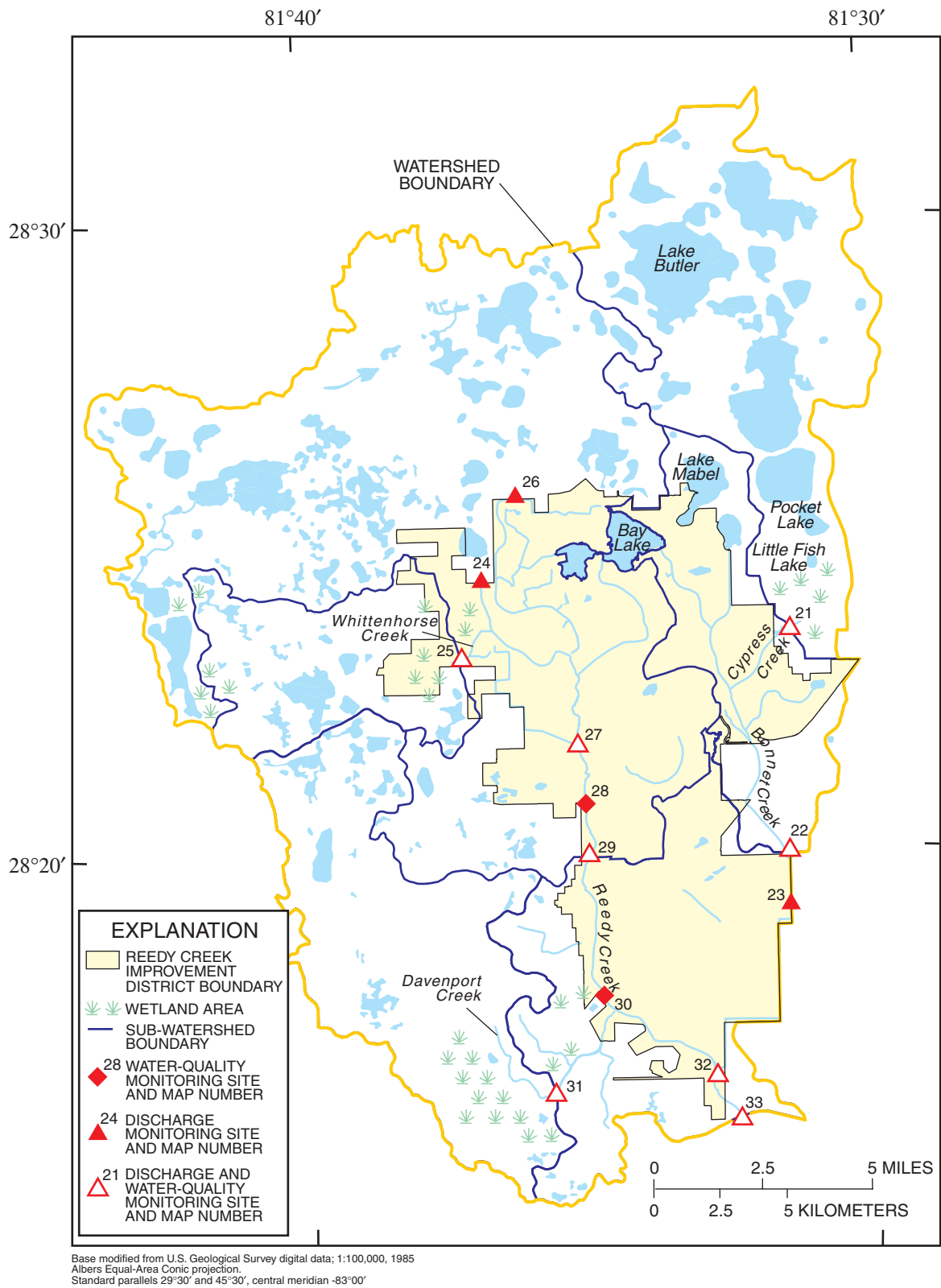
## Acknowledgements

The authors thank RCID staff members Mahmoud Elsabagh for providing data and information about hydraulic modeling of the RCID using the model UNET; Rebecca Gubert, who provided extensive water-quality data; Eddie Snell for providing data and insight into the field data collection of the RCID; and other staff members who provided Geographic Information System (GIS) land-use and land-cover data of the RCID. E.R. German, USGS, Altamonte Springs, Florida, is gratefully acknowledged for his willingness to share his insight and experience in the investigation of the hydrology of the RCID area. C.S. Melching, Marquette University, Wisconsin, provided guidance in the modeling approach to the project and the application of the HSPF model. The authors also wish to extend appreciation to Tom Jobes, AQUA TERRA, for assistance on all matters related to HSPF; and A.M. O'Reilly, USGS, Altamonte Springs, Florida, for his guidance and instruction in the application of GIS for the project.

## Description of Study Area

The Reedy Creek watershed forms the headwaters of the Kissimmee River and is located in Lake, Orange, Osceola, and Polk Counties in central Florida (fig. 1). The Reedy Creek watershed is composed of five sub-watersheds: Cypress Creek, Bonnet Creek, Reedy Creek, Whittenhorse Creek, and Davenport Creek (fig. 2). Low undulating hills and wide swampy valleys with numerous lakes and ponds of various sizes characterize the Reedy Creek watershed. A large part of the watershed is covered by forested wetlands where the water table is above or near the land surface for a substantial part of the year. Because drainage in the wetlands is poorly developed, water commonly remains in the watershed for long periods of time before flowing to creeks that drain the watershed.

Dominant land uses in the Reedy Creek watershed include urban areas (including recreational parks, parking lots, commercial and industrial developments), residential areas, forested wetlands, cropland (primarily citrus), pasture and shrub rangeland, and surface-water features such as lakes, streams, and



**Figure 2.** Sub-watersheds and data collection sites in the Reedy Creek watershed, Florida (discharge and water quality monitoring sites, table 4).

canals. The distribution of land uses differs among the sub-watersheds of Reedy Creek, with more urban areas concentrated in the southern and eastern parts of the watershed: central Reedy Creek, Cypress Creek, and Bonnet Creek. Large tracts of land have been established within the watershed for conservation purposes. These conservation areas provide storage for stormwater runoff and aid in the improvement of downstream water quality.

In 1990, the RCID implemented the use of RIBS for the disposal of treated wastewater. The RIBS are shallow excavated depressions in sandy soils where the treated wastewater is disposed. RIBS are concentrated in the Whittenhorse Creek watershed and have affected the base flow of the creek (O'Reilly, 1998). Treated wastewater also is applied to the land surface through irrigation of citrus in the upper Reedy Creek and Whittenhorse Creek watersheds, which also can affect the watershed hydrology and water quality. Wastewater used for irrigation in the Reedy Creek watershed may originate from municipal wastewater treatment plants outside of the watershed; this was accounted for in the watershed model.

Climate of the study area is humid subtropical. The average annual rainfall in central Florida for the period 1913-92 was 51 inches (in.) (Murray and Halford, 1996). Average annual rainfall for the study period (1990-95) was about 50 in. based on rainfall data collected by the National Oceanic and Atmospheric Administration (NOAA) at Orlando International Airport. Rainfall within the study area varies annually, seasonally, and spatially. Seasonal rainfall variability, evident from inspection of long-term monthly rainfall data, produces substantial seasonal trends in surface- and ground-water levels and stream discharge. Daily rainfall during summer months (June through September) varied among sites within the study area during the simulated period (1990-95), on average, from 1 in. to as much as 5 in. Rainfall represents the largest input of water to the study area.

The largest loss of water from the study area is through evapotranspiration (ET). The two processes involved in ET, evaporation and transpiration, are difficult to separate and typically are treated as one. Knowles (1996) indicated that losses due to ET in Marion County, about 70 miles (mi) northwest of the Reedy Creek watershed (fig. 1), averaged about 38 in. per year. ET can vary considerably, both spatially and temporally, across the study area. Spatial variation primarily is the result of differences in vegetation and

water availability; temporal variation primarily is the result of plant growth characteristics and climatological variables such as rainfall, solar radiation, wind speed, and humidity.

The ground-water flow system beneath the study area is a multi-aquifer system consisting of a thick sequence of carbonate rock overlain by unconsolidated deposits of sand, silt, and clay (O'Reilly, 1998). The surficial aquifer system is the uppermost water-bearing unit in the study area. The upper boundary of the ground-water system is defined by the water table, which in most areas is a subdued reflection of the land-surface topography. Modeling hydrologic processes that determine overland flow and interactions with the upper soil zones is complicated by the presence of a high water table in many parts of Florida, including the Reedy Creek watershed. The Floridan aquifer system underlies the surficial aquifer system in the study area and consists of two major permeable zones separated by a less permeable zone of highly variable water-transmitting characteristics. The depth to the top of the Floridan aquifer system is less than 100 feet (ft) and the aquifer ranges from 2,200-2,400 ft in thickness in the study area (Tibbals, 1990, figs. 10 and 11).

The Reedy Creek watershed includes a number of sub-watersheds including Cypress Creek, Davenport Creek, Whittenhorse Creek, and Bonnet Creek (fig. 2). The watershed also contains land and water areas that do not contribute flow to the stream channel system. Areas of non-contributing flow generally are located in sub-watersheds north and west of the RCID: upper Cypress Creek, upper east and upper west Reedy Creek, Whittenhorse Creek, and Davenport Creek. The natural drainage systems of Reedy and Bonnet Creeks were altered within the RCID as a result of development. Urbanization in the Reedy Creek watershed outside the RCID also altered streamflow characteristics.

The Cypress Creek sub-watershed is in the northeastern part of the Reedy Creek watershed and is a tributary to Bonnet Creek. Cypress Creek has a drainage area of 29.3 mi<sup>2</sup> or about 16 percent of the total watershed. Land and water areas that do not contribute flow to the stream channel system comprise about 4 percent (1.3 mi<sup>2</sup>) of the Cypress Creek drainage area and are located in the northern and western parts of the sub-watershed. The creek receives outflow from a large chain of lakes, the largest of which is Lake Butler (fig. 2). Water from the chain of lakes



overflows from Pocket Lake and Little Fish Lake into a large wetland area. The Cypress Creek stream channel is poorly defined to just upstream from the USGS gaging station Cypress Creek at Vineland (USGS site number 02264000; map number 21 in fig. 2). Downstream from this gaging station, Cypress Creek enters the RCID and flows through a series of control structures to Bonnet Creek.

The Bonnet Creek sub-watershed, which includes Cypress Creek, is in the eastern part of the Reedy Creek watershed. Bonnet Creek has a drainage area of 44.7 mi<sup>2</sup> or about 25 percent of the total watershed. Bonnet Creek is highly channelized within the RCID and flows through a conservation area south of the USGS gaging station Bonnet Creek near Vineland (USGS site number 02264100; map number 22 in fig. 2). Water is diverted out of the Bonnet Creek sub-watershed through a regulated outlet structure at the USGS Bonnet Creek near Kissimmee gaging station (USGS site number 02264140; map number 23 in fig. 2). Most discharge from Bonnet Creek flows into Reedy Creek upstream from the USGS gaging station Reedy Creek at S-40 near Loughman (USGS site number 02266495; map number 32 in fig. 2).

The Whittenhorse Creek sub-watershed is located in the west-central part of the Reedy Creek watershed. Whittenhorse Creek has a drainage area of 12.4 mi<sup>2</sup> or about 7 percent of the total watershed. Much of the Whittenhorse Creek sub-watershed is characterized by low topographic relief and forested wetlands, but other areas in the watershed that are at higher altitudes and areas with sandier soils have been used for citrus cultivation. Land and water areas that do not contribute flow to the stream channel system comprise less than 0.1 percent of the Whittenhorse Creek drainage area. The distribution of treated wastewater to RIBS contributes to baseflow (through ground-water inflows to the streambed) in Whittenhorse Creek in the reaches upstream from the USGS gaging station Whittenhorse Creek near Vineland (USGS site number 02266200; map number 25 in fig. 2).

Davenport Creek has a drainage area of 23.0 mi<sup>2</sup> or about 13 percent of the total watershed. Davenport Creek is poorly defined near its confluence with Reedy Creek and drains into a wetland area upstream from the USGS gaging station Reedy Creek at S-40 near Loughman (USGS site number 02266495; map number 32 in fig. 2). The Davenport Creek sub-watershed contains flat, swampy, wetland areas. A large

percentage of higher ground in the watershed is used for agricultural purposes, mainly cultivation of citrus. Land and water areas not contributing flow to the Davenport Creek stream channel system comprise about 8 percent (1.9 mi<sup>2</sup>) of the total drainage area. As with the other sub-watersheds of Reedy Creek, the drainage basin boundaries of the upper reaches of the Davenport Creek, upstream from the USGS gaging station Davenport Creek near Loughman (USGS site number 02266480; map number 31 in fig. 2), are not well defined.

Reedy Creek originates in wetlands in the northern and northwestern parts of the watershed. The watershed boundary is poorly defined in the upper part of the basin (Hampson, 1993). Land and water areas in the upper part of the watershed that do not contribute flow to channel system comprise approximately 6 percent (10.6 mi<sup>2</sup>) of the entire 177-mi<sup>2</sup> Reedy Creek watershed. Non-contributing drainage areas in the upper part of the watershed are mainly citrus groves and small lakes. Wetlands that form the headwaters of Reedy Creek drain into the RCID north of USGS gaging stations Reedy Creek at S46 near Vineland and Lateral 405 at S-405A near Doctor Phillips (USGS site numbers 02266025 and 02266291; map numbers 24 and 26, respectively, in fig. 2). Within the RCID, the channel of Reedy Creek has been altered; many reaches have been channelized and numerous control structures are in place, primarily to regulate water levels of the creek. About 1.9 mi north of the USGS gaging station Reedy Creek near Vineland (USGS site number 02266300; map number 29 in fig. 2), the channelized stream section ends. Reedy Creek flows in a southerly direction before entering a large wetland conservation area upstream from the USGS gaging station Reedy Creek at S-40 near Loughman (USGS site number 02266495; map number 32 in fig. 2). Downstream from the USGS gaging station Reedy Creek at S-40 near Loughman, the creek flows through a natural channel past the USGS gaging station Reedy Creek near Loughman (USGS site number 02266500; map number 33 in fig. 2).

## Study Approach

Although hydrologic and water-quality data have been collected within the Reedy Creek watershed, these data have not previously been used to evaluate the relations among land use, hydrology, and water quality. Because of the natural variability of

hydrologic and water-quality data, the spatial variability within watersheds, and the complexity of nutrient runoff and transport relations, it is difficult to relate specific watershed characteristics to conditions downstream unless the watershed is evaluated and analyzed as a system.

The HSPF model was used to simulate runoff from land surfaces and, subsequently, nutrient concentrations in the watershed. Although data-intensive and complex, HSPF is the only available model that can simulate the continuous, dynamic event or steady-state behavior of both hydraulic and water-quality processes in a watershed (Singh, 1995). HSPF was selected for modeling Reedy Creek because of the model characteristics previously described, and also because of its modular structure and capacity for modifications or enhancements to meet specific needs in assessing effects of changes in the watershed. HSPF, jointly developed by the U.S. Environmental Protection Agency (USEPA) and USGS, is used widely and continues to undergo refinements and enhancements, ensuring that it will remain a viable and relevant tool in watershed modeling.

In order to develop rainfall-runoff and water-quality relations, climatic conditions and physical characteristics of the watershed must be quantified. To define rainfall-runoff and water-quality relations, data collected over the simulated period (January 1, 1990, to December 31, 1995) were compiled, evaluated, and processed into time series or other appropriate formats required for input to the model. These time series data provided inputs and fluxes necessary for calibration and confirmation of the model simulation. The time period simulated represents a 6-year period in which rainfall ranged from below average in the early part of the simulation to above average in the later years of simulation. Although the range in rainfall data and associated hydrologic conditions presented a challenge for developing a model, the resulting model generally is more applicable to a broader range of hydrologic conditions because of the extremes in rainfall that were included.

## **SIMULATION OF HYDROLOGY AND WATER QUALITY**

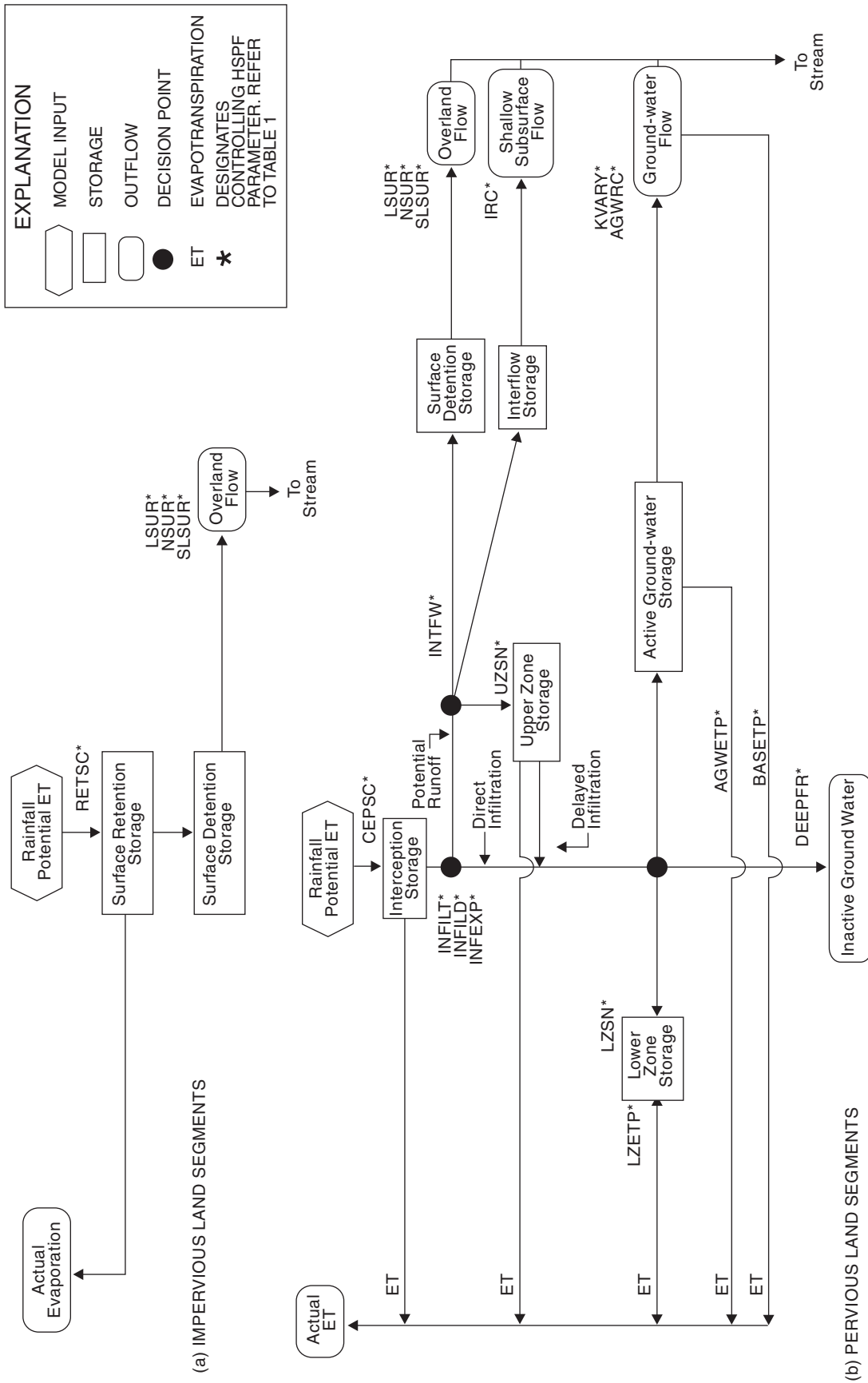
The HSPF model was used to simulate rainfall-runoff relations and nutrient concentrations in the Reedy Creek watershed. HSPF is a comprehensive watershed model used to simulate hydrology, nonpoint

runoff and soil processes, and in-stream water quality in complex agricultural, rural, and urban watersheds (Donigian and others, 1995). The HSPF model allows continuous simulation of the quantity and quality of land-based runoff linked with hydraulic routing and in-stream water-quality processes.

HSPF is an empirical model; conceptually, the model parameters have physical meaning but are not physically measurable and must be determined by calibration. The HSPF model is divided into three components to simulate the hydrology and water quality of a watershed: pervious land areas, impervious land areas, and stream reaches. The pervious land part of the hydrologic cycle is represented conceptually within HSPF by a series of interconnected water storage zones: an upper zone, a lower zone, and a groundwater zone (Duncker and others, 1995). Simple surface processes represent the impervious land part of the hydrologic cycle. The stream reaches simulate processes that occur in open or closed channel reaches, and they represent unidirectional flow through the channel network. Figure 3 is a schematic of how the model routes land-based runoff for both pervious and impervious areas. In pervious areas, the amount of water contained in the three storage zones and the flux of water between these zones and the stream or atmosphere are simulated on a continuous basis for a sub-area having a given land cover and precipitation input. The flux of water between the storage zones and the stream or atmosphere is affected by a large number of model parameters, which are listed in table 1.

The Hydrological Simulation Program-Fortran EXPert system (HSPEXP) was used to assist in calibration of the hydrology of the Reedy Creek watershed model (Lumb and others, 1994). HSPEXP consists of a set of hierarchical rules designed to guide calibration of the model through a systematic evaluation of model parameters. Simulation errors are evaluated based on seven criteria: total volume, low-flow recession, 50 percent lowest flows, 10 percent highest flows, storm volumes, seasonal volume, and summer storm volume. Statistics calculated by HSPEXP provide the modeler with an evaluation of the agreement between simulated and observed runoff values.

Water-quality subroutines within HSPF simulate constituent processes and fluxes associated with pervious and impervious land surfaces, water-quality processes occurring within the stream reach, and advection of constituents downstream as water is



**Figure 3.** Hydrological Simulation Program-Fortran flowchart for (a) impervious and (b) pervious land segments (modified from Berris, 1995).

**Table 1.** Hydrological Simulation Program-Fortran (HSPF) parameters used to simulate hydrology

[land area: PERLND, pervious; IMPLND, impervious. Modified from Jarret and others, 1998, table 6]

Abbreviation	Explanation	Land area
LZETP	Lower zone evapotranspiration. An index value (ranging from 0 to 0.99) representing the density of deep rooted vegetation	PERLND
INFILT	Infiltration capacity. An index to the infiltration capacity of soils. This parameter also affects percolation to the ground-water zone	PERLND
INFEXP	Exponent for the infiltration equation. Controls the rate of infiltration decrease as a function of increasing soil moisture	PERLND
INFILD	Ratio of maximum to mean infiltration rate	PERLND
INTFW	Interflow index. An index that controls the amount of infiltrated water that flows as shallow subsurface runoff	PERLND
IRC	Interflow recession coefficient. An index for the rate of shallow subsurface flow	PERLND
CESPC	Interception storage capacity	PERLND
RETSC	Retention storage capacity	IMPLND
LZSN	Lower zone nominal storage. An index to the soil moisture holding capacity of the unsaturated zone	PERLND
UZSN	Upper zone nominal storage. An index to the amount of surface storage in depressions and the upper few inches of soil	PERLND
BASETP	Fraction of available potential-evapotranspiration demand that can be met from ground-water outflow. Simulates evapotranspiration from riparian vegetation	PERLND
AGWETP	Fraction of available potential-evapotranspiration demand that can be met from stored ground water. Simulates evapotranspiration from phreatophytes, in general	PERLND
AGWRC	Ground-water recession parameter. An index of the rate at which ground water drains from the land	PERLND
KVARY	Ground-water outflow modifier. An index of how much effect recent recharge has on ground-water outflow	PERLND
DEEPPFR	Fraction of ground water that does not discharge to the surface within the boundaries of the modeled area	PERLND
LSUR	Average length of the overland flow plane	PERLND or IMPLND
SLSUR	Average slope of the overland flow plane	PERLND or IMPLND
NSUR	Average roughness of the overland flow plane	PERLND or IMPLND

routed through the channel system. HSPF simulates the contribution of water-quality constituents transported from land surfaces to stream reaches by overland flow, outflow from the interflow (shallow subsurface flow) storage zone, and outflow from the ground-water storage zone. Water-quality constituent concentrations transported from land surfaces can be simulated by a simple build-up and wash-off model of the constituent from the land surface or by a series of cycling reactions such as volatilization, denitrification, fixation, or mineralization of a constituent on the land surface. The simple build-up and wash-off model was used for the Reedy Creek watershed model. Outflow concentration of a water-quality constituent from the interflow and ground-water storage zones can be controlled by parameters affecting contribution of constituent concentration to the stream reach for each individual storage zone. In the Reedy Creek watershed model, constant constituent concentrations were

applied to the interflow and ground-water flow for each pervious land cover type. HSPF has the ability to apply variable monthly concentrations to interflow and ground-water flow, but this was not applied to the Reedy Creek watershed model because monthly trends were not apparent in the observed in-stream water-quality concentrations.

Water-quality constituent loads simulated for pervious and impervious areas in HSPF are routed to the stream channel network. Physical processes such as longitudinal advection, heat balances; dissolved oxygen (DO), biochemical oxygen demand (BOD), and inorganic nitrogen and phosphorus balances; plankton populations; inorganic sediment deposition, scour, and transport; and other chemical reactions and processes are simulated within a single open- or closed-channel reach or a completely mixed lake (water-based processes). Precipitation, evaporation, and other fluxes influence the processes that occur in a

stream reach. Water-quality processes occurring within the stream reach and simulated by HSPF are compartmentalized into subroutines for different constituent types that simulate constituent reactions, cycling, and interactions with other constituent types.

## Data Collection and Compilation

Input data for the HSPF model include spatial data (land use, topography, and drainage characteristics such as reach length and cross section data) and time series data (air and water temperatures, wind speed, atmospheric deposition rates of ammonia and nitrate nitrogen, rainfall, potential ET, solar radiation, and application rates of irrigation and treated wastewater). Time series of daily mean discharge, daily mean DO concentration, and periodic observations of water-quality constituent concentrations were used for calibration and confirmation of the model.

### Spatial Data

Land-use and topographic data for the Reedy Creek watershed were derived using GIS data provided by the St. Johns River Water Management District, South Florida Water Management District,

Southwest Florida Water Management District, and RCID. Land-use data were available for the period of 1986-90 and land-cover attributes from GIS data sources were correlated with the USGS land-use and land-cover classification system for use with remote sensor data (U.S. Geological Survey, 1990). GIS land-use data were adjusted, based on land-cover type and additional land-use information obtained by ground truth observation and data from the U.S. Department of Agriculture, National Agricultural Statistics Service (1999), to represent the distribution of land use in the Reedy Creek watershed as it existed in January 1990. No adjustments were made to the land-use or land-cover data for changes that might have occurred during the simulated period (January 1990-December 1995). This period was selected, however, because relatively little development occurred in the Reedy Creek watershed during that time.

### Time Series Data

Meteorologic data compiled and used as input to the Reedy Creek watershed model include air temperature, wind speed, atmospheric deposition of ammonia and nitrate nitrogen, rainfall, solar radiation, and pan evaporation (used to calculate potential ET) (table 2).

**Table 2.** Meteorologic and atmospheric-deposition sites used for the Hydrological Simulation Program-Fortran model of the Reedy Creek watershed, Florida

[Abbreviation for data type: D, atmospheric deposition; S, solar radiation; P, pan evaporation; W, wind speed; T, air temperature; R, rainfall. Abbreviation for source of data: NADP, National Atmospheric Deposition Program/National Trends Network; NOAA, National Oceanic and Atmospheric Administration; M&E, Metcalf and Eddy Services, Inc.; USGS, U.S. Geological Survey. --, not applicable or no data. Sites listed in figure 4]

Map number	Site name	Site number	Latitude	Longitude	Data type	Frequency	Source of data
1	Kennedy Space Center	FL99	28° 32' 34"	80° 38' 40"	D	Quarterly	NADP
2	Daytona Beach International Airport	082158	29° 11' --"	81° 03' --"	S	Hourly	NOAA
3	Lisbon	085076	28° 52' --"	81° 47' --"	P	Daily	NOAA
4	Orlando International Airport	086628	28° 26' 02"	81° 19' 30"	W	Hourly	NOAA
5	Orlando International Airport	086628	28° 26' 02"	81° 19' 30"	T	Hourly	NOAA
6	Orlando International Airport	086628	28° 26' 02"	81° 19' 30"	R	Hourly	NOAA
7	Clermont 7 S	081641	28° 27' --"	81° 45' --"	R	Daily <sup>1</sup>	NOAA
8	Lake Alfred Exp Station	084707	28° 06' --"	81° 43' --"	R	Daily <sup>1</sup>	NOAA
9	Kissimmee 2	084625	28° 17' --"	81° 25' --"	R	Daily <sup>1</sup>	NOAA
10	Water Conserv II Rain Gage 6-1	--	28° 29' 56"	81° 36' 57"	R	Daily <sup>1</sup>	M&E
11	Water Conserv II Rain Gage 6-2	--	28° 29' 28"	81° 37' 03"	R	Daily <sup>1</sup>	M&E
12	Water Conserv II Rain Gage 6-3	--	28° 29' 15"	81° 37' 27"	R	Daily <sup>1</sup>	M&E
13	Water Conserv II Rain Gage 6-4	--	28° 29' 25"	81° 37' 53"	R	Daily <sup>1</sup>	M&E
14	Water Conserv II Rain Gage 7-1	--	28° 27' 18"	81° 38' 05"	R	Daily <sup>1</sup>	M&E
15	Water Conserv II Rain Gage 7-2	--	28° 27' 05"	81° 37' 34"	R	Daily <sup>1</sup>	M&E
16	Water Conserv II Rain Gage 9-1	--	28° 26' 15"	81° 37' 54"	R	Daily <sup>1</sup>	M&E
17	Lateral 101 at S-101 near Lake Buena Vista	02264060	28° 22' 28"	81° 31' 01"	R	Hourly	USGS
18	Lateral 410 at S-410 near Vineland	02266295	28° 21' 58"	81° 35' 55"	R	Hourly	USGS

<sup>1</sup>Data collected at least daily but typically hourly.



Daily maximum and minimum air temperature and daily wind speed collected by the National Oceanic and Atmospheric Administration (NOAA) at the Orlando International Airport weather station (fig. 4, map numbers 4-5) were compiled (National Oceanic and Atmospheric Administration, National Climatic Data Center, 1999). Total atmospheric deposition of ammonia nitrogen and nitrate nitrogen collected seasonally by the National Atmospheric Deposition Program/National Trends Network (NADP/NTN) at the Kennedy Space Center atmospheric deposition station (fig.4, map number 1) also were compiled for use in the watershed model (National Atmospheric Deposition Program/National Trends Network, 1999).

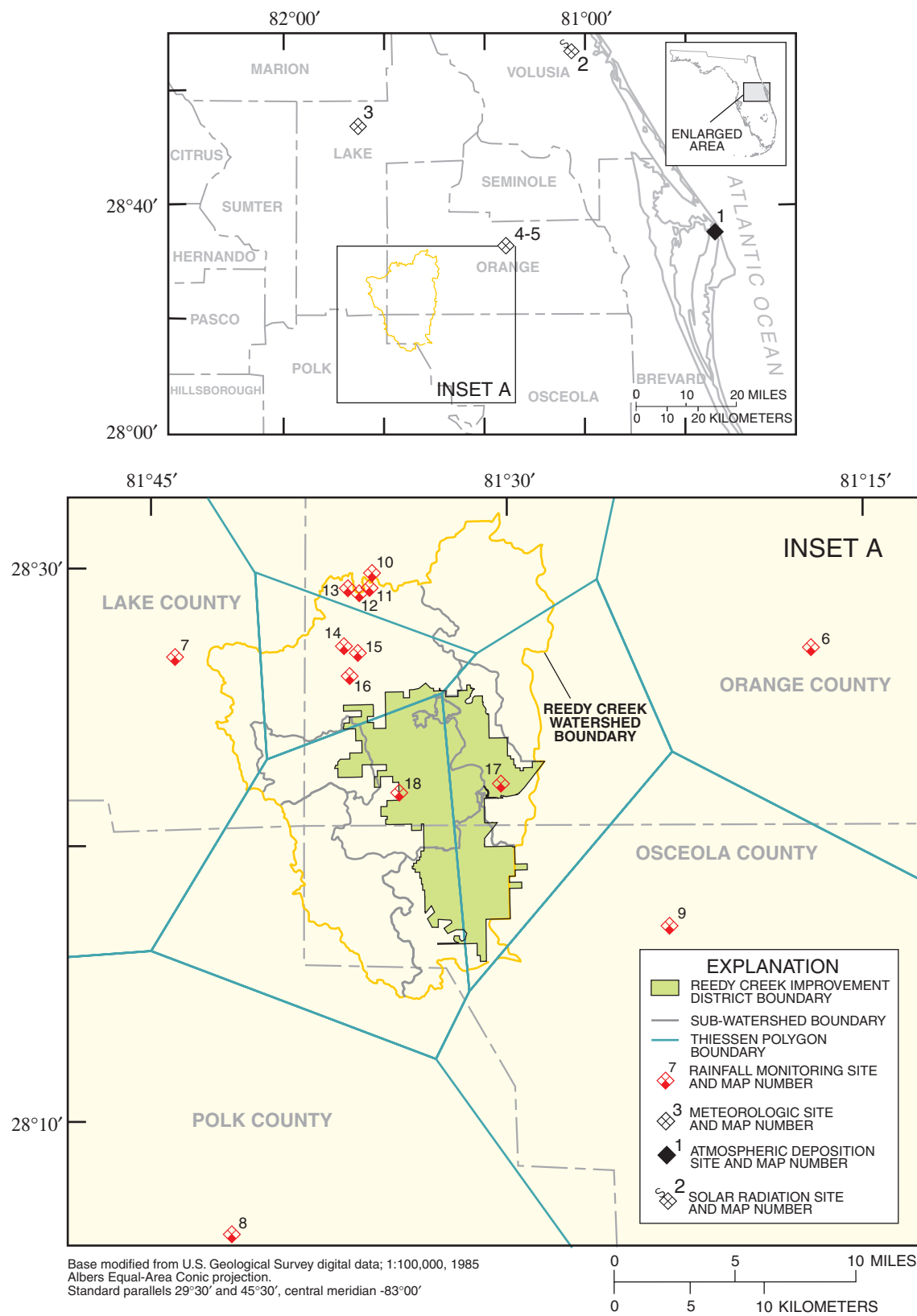
Because of the uneven distribution of rainfall data-collection sites, a Thiessen polygon analysis (Thiessen, 1911) was required to determine the spatial distribution of rainfall data for model input. Rainfall data for numerous sites in central Florida around the 177-mi<sup>2</sup> study area were examined for length of available record and missing record. Sites considered for use in the model included seven sites in the northern and northwestern parts of the watershed (fig. 4, table 2, map numbers 10-16), two in the central part of the watershed (fig. 4, table 2, map numbers 17-18), and four sites located outside of the watershed (fig. 4, table 2, map numbers 6-9). Rainfall data at these sites were evaluated for missing record, and compared for variability in daily, monthly, and annual totals. Before using the rainfall sites for the Thiessen polygon analysis, further analysis was done to determine whether redundancies existed in data at the rainfall sites because of the close proximity of some of the rainfall sites relative to others used in the analysis. If redundancies were detected based on the analysis, data from these sites could be grouped together, and an average rainfall total used for the model input.

Possible redundancies in the data at closely located rainfall sites were evaluated by analyzing rainfall totals between rainfall sites, and the effect of distance on the correlation of rainfall totals. For the analysis, 5 years of daily rainfall record were evaluated and correlation coefficients were computed between pairs of rainfall sites based on daily, 7-day, 14-day, 21-day, and 30-day cumulative rainfall totals. The correlation coefficients for pairs of rainfall sites were plotted as a function of distance between sites to determine whether there was redundancy in the data among the sites.

Results of the correlation analysis between rainfall totals at sites as a function of distance varied depending on the period of time over which the rainfall was being summed, as well as by distance. In general, higher correlations between sites resulted when summed over longer periods of time (14 to 30 days) or for shorter distances when summed for shorter time periods (1 to 7 days). For example, the correlation between daily total rainfall at sites only 1 mi apart was 0.92, but at a distance of 6 mi or more, the correlation coefficient decreased to only 0.5. For 7-day rainfall sums, sites located 2 mi apart or closer had a correlation coefficient of 0.9 or better; the correlation coefficients decreased to 0.83 where sites were 3.8 mi apart or more, and to 0.71 where sites were 5.3 mi apart. For 14-day rainfall totals, the correlation coefficients ranged from 0.97 for sites less than 0.5 miles apart to 0.73 for sites 5.3 mi apart. At a summing interval of 30 days, stations 3.77 mi or closer were correlated at 0.9 or better; but at distances of 5.3 mi or greater, correlations ranged from 0.8 to 0.4.

Rainfall data for the USGS sites within the RCID were the most poorly correlated (fig. 4, table 2, map numbers 17-18); these daily values were closely examined and the records compared to the NOAA and Water Conserv II sites (fig. 4, table 2, map numbers 6-9 and 10-16, respectively). Even though rainfall data at the USGS sites were poorly correlated, those sites have the advantage of being located within the central part of the watershed and thus better suited for generation of rainfall-runoff in the watershed than sites near the boundaries or external to the watershed. Although the RCID currently (2001) maintains a rainfall data network, no data were available for the first 2 years of the simulation period. When available, however, RCID data were used to supplement data collected at nearby USGS rainfall sites.

Thiessen polygon analysis was combined with the correlation-distance analysis to determine which Thiessen polygon scenario to apply to the watershed model. Several analyses were tried based on distances between sites, using the correlation-distance analysis as a guide for initial trials. Thiessen polygons were determined using distances ranging from 1 to 8 mi. At a distance of 5 mi or greater, the resulting Thiessen polygons for the study area were identical using a set of 13 rainfall sites. Based on these analyses, Thiessen polygons based on a distance between sites of greater than 4 mi were used for the spatial distribution of rainfall data in the model. Data for rainfall sites located



**Figure 4.** Meteorologic and atmospheric deposition sites (top), and rainfall sites and Thiessen polygons (Inset A) used for the Hydrological Simulation Program-Fortran model of the Reedy Creek watershed, Florida (map numbers are listed in table 2).

within one Thiessen polygon were averaged for that polygon. This was done for sites located at map numbers 10-13, and map numbers 14-16 (fig. 4, Inset A). For all other Thiessen polygons, a single rainfall site was available for use as input to the model.

Using the Thiessen polygon analysis, the Reedy Creek watershed was divided into four major rainfall areas: (1) the upper Reedy Creek watershed (fig. 4, map numbers 10-13); (2) upper Reedy Creek watershed south (fig. 4, map numbers 14-16); (3) southern Reedy Creek watershed east, represented by rainfall at Lateral 101 at S101 near Lake Buena Vista (fig. 4, map number 17); and (4) southern Reedy Creek watershed west, represented by rainfall at Lateral 410 at S-410 near Vineland (fig. 4, map number 18). Rainfall from the NOAA weather station at Orlando International Airport (fig. 4, map number 6) was used for data comparison and disaggregation of non-hourly rainfall to hourly rainfall data. A summary of rainfall data used for Thiessen polygon areas used in the watershed model is given in table 3.

Evapotranspiration is a function of many variables including vegetation type, net radiation, solar radiation, wind speed, and air temperature. Results from several studies in and near the study area provided information on which to base ET estimates (Tibbals, 1990; Lee and Swancar, 1994; and Phelps and others, 1995). Pan evaporation data collected at a NOAA station at Lisbon (fig. 4 and table 2, map number 3) were determined to best represent conditions for the entire watershed. Pan evaporation data were corrected using pan coefficients determined in studies at Belle Glade, near Lake Okeechobee (Kohler, 1954), so as to represent potential ET across the watershed.

Irrigation of agricultural areas using ground water and application of treated wastewater are sources of water applied to the watershed but not included in rainfall totals. Data on irrigation practices and application rates were obtained from Orange County, the City of Orlando, O'Reilly (1998), and the files of the USGS, Altamonte Springs, Florida. A monthly time series of irrigation applied to agricultural areas was developed for the study period, January 1990 to December 1995. Application rates of treated wastewater applied to RIBS for the study period were supplied by the RCID. A time series of total monthly application of wastewater to the RIBS was developed for use in the model.

Streamflow data have been collected by the USGS at sites within the Reedy Creek watershed for many years. Daily discharge data for 10 sites (table 4, fig. 2) in the basin are available for the 6-year study period, January 1990 to December 1995 (U.S. Geological Survey, 2000). Data for six sites were used to develop, calibrate, and confirm model parameters for the watershed: Cypress Creek at Vineland, Bonnet Creek near Vineland, Whittenhorse Creek near Vineland, Reedy Creek near Vineland, Davenport Creek near Loughman, and Reedy Creek near Loughman (USGS site numbers 02264000, 02264100, 02266200, 02266300, 02266480, and 02266500; map numbers 21, 22, 25, 29, 31, and 33 in fig. 2, respectively). Four sites are located at hydrologic structures where collection of representative hydrologic data is difficult: Reedy Creek at S46 near Vineland, Lateral 405 at S-405A near Doctor Phillips, Lateral 405 below S-405 near Vineland, and Reedy Creek at S-40 near

**Table 3.** Representative rainfall areas used for the Hydrologic Simulation Program-FORTRAN model of the Reedy Creek watershed, Florida

[Thiessen polygon areas are shown in fig. 4]

Site name	Maximum daily rainfall (inches)	Date of maximum rainfall	Annual rainfall total (inches)						Annual mean rainfall (inches)
			1990	1991	1992	1993	1994	1995	
Southern Reedy Creek watershed east <sup>1</sup>	5.21	8-2-95	39.27	46.84	55.63	57.28	45.57	67.61	52.03
Southern Reedy Creek watershed west <sup>2</sup>	3.76	6-16-94	39.41	60.97	55.21	52.14	58.37	53.08	53.20
Upper Reedy Creek watershed <sup>3</sup>	3.82	6-17-94	36.46	50.48	43.36	37.16	68.30	51.02	47.80
Upper Reedy Creek watershed south <sup>4</sup>	3.35	9-30-90	39.27	51.40	44.26	40.05	62.82	51.51	48.22

<sup>1</sup>Lateral 101 at S-101 near Lake Buena Vista.

<sup>2</sup>Lateral 410 at S-410 near Vineland.

<sup>3</sup>Composite of Water Conserv II rain gage sites 6-1, 6-2, 6-3, and 6-4.

<sup>4</sup>Composite of Water Conserv II rain gage sites 7-1, 7-2, and 9-1.

**Table 4.** Streamflow and water-quality data-collection sites, Reedy Creek watershed, Florida

[USGS, U.S. Geological Survey; data type: D, discharge; De, estimated daily discharge; P, periodic water-quality; T, continuous water temperature; O, continuous dissolved oxygen. --, not available. Map number shown in figure 2]

Map number	Site name and USGS identification number	Latitude	Longitude	Date established	Drainage area <sup>1</sup> (square miles)	Data type
21	Cypress Creek at Vineland (02264000)	28° 23' 25"	81° 31' 11"	August 1954	29.3	D, P
22	Bonnet Creek near Vineland (02264100)	28° 19' 30"	81° 31' 15"	May 1966	44.7	D, P
23	Bonnet Creek near Kissimmee (02264140)	28° 18' 28"	81° 31' 28"	June 1986	--	De
24	Reedy Creek at S46 near Vineland (02266025)	28° 24' 18"	81° 36' 42"	October 1986	25.4	D
25	Whittenhorse Creek near Vineland (02266200)	28° 23' 05"	81° 37' 00"	May 1966	12.4	D, P
26	Lateral 405 at S-405A near Doctor Phillips (02266291)	28° 25' 37"	81° 36' 19"	October 1986	19.6	D
27	Lateral 405 below S-405 near Vineland (02266294)	28° 23' 39"	81° 35' 07"	October 1970	indeterminate	D, P
28	Reedy Creek above Hwy 192 near Vineland (02266298)	28° 20' 54"	81° 34' 53"	May 1986	--	T
29	Reedy Creek near Vineland (02266300)	28° 19' 57"	81° 34' 48"	May 1966	84.6	D, P, T, O
30	Reedy Creek at I-4 near Loughman (02266320)	28° 17' 54"	81° 34' 40"	May 1986	--	T
31	Davenport Creek near Loughman (02266480)	28° 16' 15"	81° 35' 28"	January 1969	23.0	D, P
32	Reedy Creek at S-40 near Loughman (02266495)	28° 16' 32"	81° 32' 39"	October 1986	174	D, T, O
33	Reedy Creek near Loughman (02266500)	28° 15' 48"	81° 32' 12"	October 1939	177	D, P

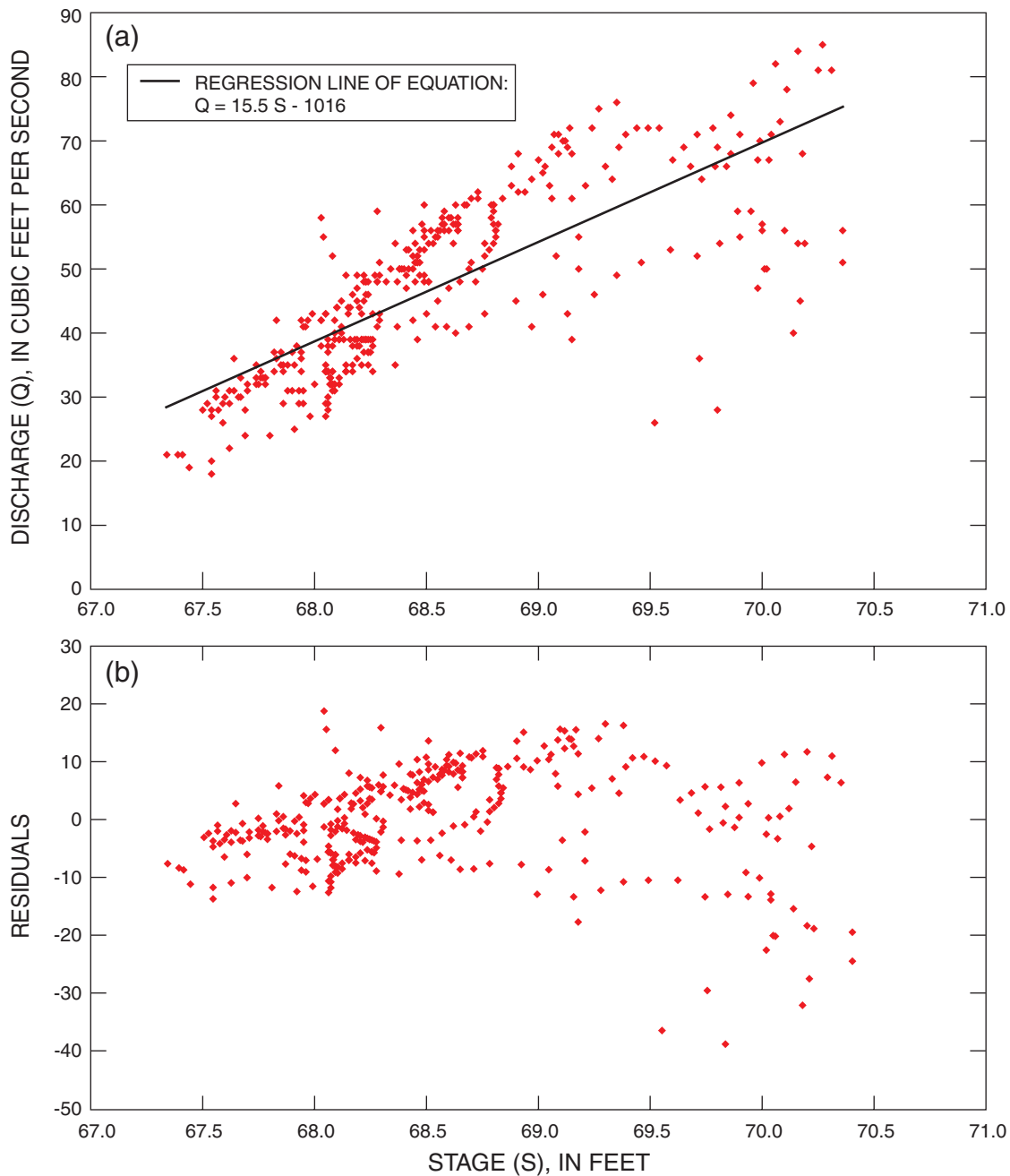
<sup>1</sup>Drainage area from U.S. Geological Survey, 2000, Water resources data, Florida, water year 1999, volume 1A.

Loughman (USGS site numbers 02266025, 02266291, 02266294, and 02266495; map numbers 24, 26, 27, and 32 in fig. 2, respectively). Data for these four sites are of relatively poor quality in comparison to sites used for model parameter development, calibration, and confirmation, so these data were not directly used in model development, calibration, or confirmation.

Flow is diverted from the Reedy Creek watershed to the east through a pair of gated culverts at the USGS gaging station Bonnet Creek near Kissimmee (USGS site number 02264140; map number 23 in fig. 2). Data for the site were not available for the modeled period; however, German (1989) collected flow data and computed discharge at the site for the period June 1986 to May 1987. These data were used to estimate the flow diversion for the modeled time period by using a linear regression. Discharge values calculated by German (1989) at this location and recorded values for water-surface elevation at Reedy Creek at S-40 near Loughman were correlated (fig. 5).

The regression yielded a coefficient of determination ( $R^2$ ) of 0.60, a standard error of estimate of 8.74 cubic feet per second ( $\text{ft}^3/\text{s}$ ), and relatively normal distribution of residuals (fig. 5). The daily amount of water diverted from Bonnet Creek for the simulated time period was calculated based on this regression.

Water-quality time series data suitable for simulation of water-quality reactions and comparison with simulation results are available for several locations in the Reedy Creek watershed (fig. 2, table 4). Continuous water temperature and DO concentration data have been collected by the USGS at sites within the Reedy Creek watershed since 1977 (U.S. Geological Survey, 2000). Hourly water temperature data were used to represent water temperatures in the watershed, and mean daily DO concentrations were used for comparison to simulation results. Periodic water samples have been collected and analyzed for nutrient concentrations by the USGS and RCID at sites within the Reedy Creek watershed and were used for comparison



**Figure 5.** Relations between (a) discharge and stage and (b) regression residuals and stage for Bonnet Creek near Kissimmee, Florida.

to simulation results. Observed water-quality data were used for adjustment of model parameters and for evaluation of the goodness-of-fit of the model.

Solar radiation data available from the USEPA, Better Assessment Science Integrating Point and Non-point Sources (BASINS) system, were used in the Reedy Creek watershed model for simulation of water-quality processes occurring within a stream reach

(U.S. Environmental Protection Agency, 1999). Atmospheric deposition data available from the National Atmospheric Deposition Program/National Trends Network (NADP/NTN) were used in the Reedy Creek watershed model to simulate build-up and wash-off of a constituent from pervious and impervious land areas (National Atmospheric Deposition/National Trends Network, 1999). Quarterly total



atmospheric deposition data of ammonia nitrogen and nitrate nitrogen for a site in east-central Florida at the Kennedy Space Center (fig. 4 and table 2, map number 1) were compiled from data available on the World Wide Web. Hourly solar radiation data for a site in east-central Florida at Daytona Beach International Airport (fig. 4 and table 2, map number 2) were compiled from data sources available in the BASINS system.

## Model Development

The major steps for simulating runoff quantity and quality for the Reedy Creek watershed during this study included: simulation plan development; database development; watershed segmentation; parameter estimation and input preparation; hydrology and water-quality calibration and confirmation; and simulation of an alternative scenario. The initial steps in model development were simulation planning and database development. The watershed model provided the computational foundation for evaluating the effects of changes in land use on hydrology and water quality. Data were compiled, evaluated, and processed to define the watershed characteristics, and to provide inputs and fluxes necessary for calibration and confirmation of the model.

The classification of watershed characteristics and the division of the land surface into land-use types is called watershed segmentation (Donigian and others, 1995). The Reedy Creek watershed was segmented into three components for runoff and water-quality simulation by HSPF: land-use types, land segments based on drainage basin characteristics, and channel reaches. This division allows the assignment

of parameter values to discrete land parcels and channel reaches, the assignment of runoff volumes to specific destinations, the representation of build-up and wash-off of constituents from the land surface, and the simulation of in-stream water-quality processes.

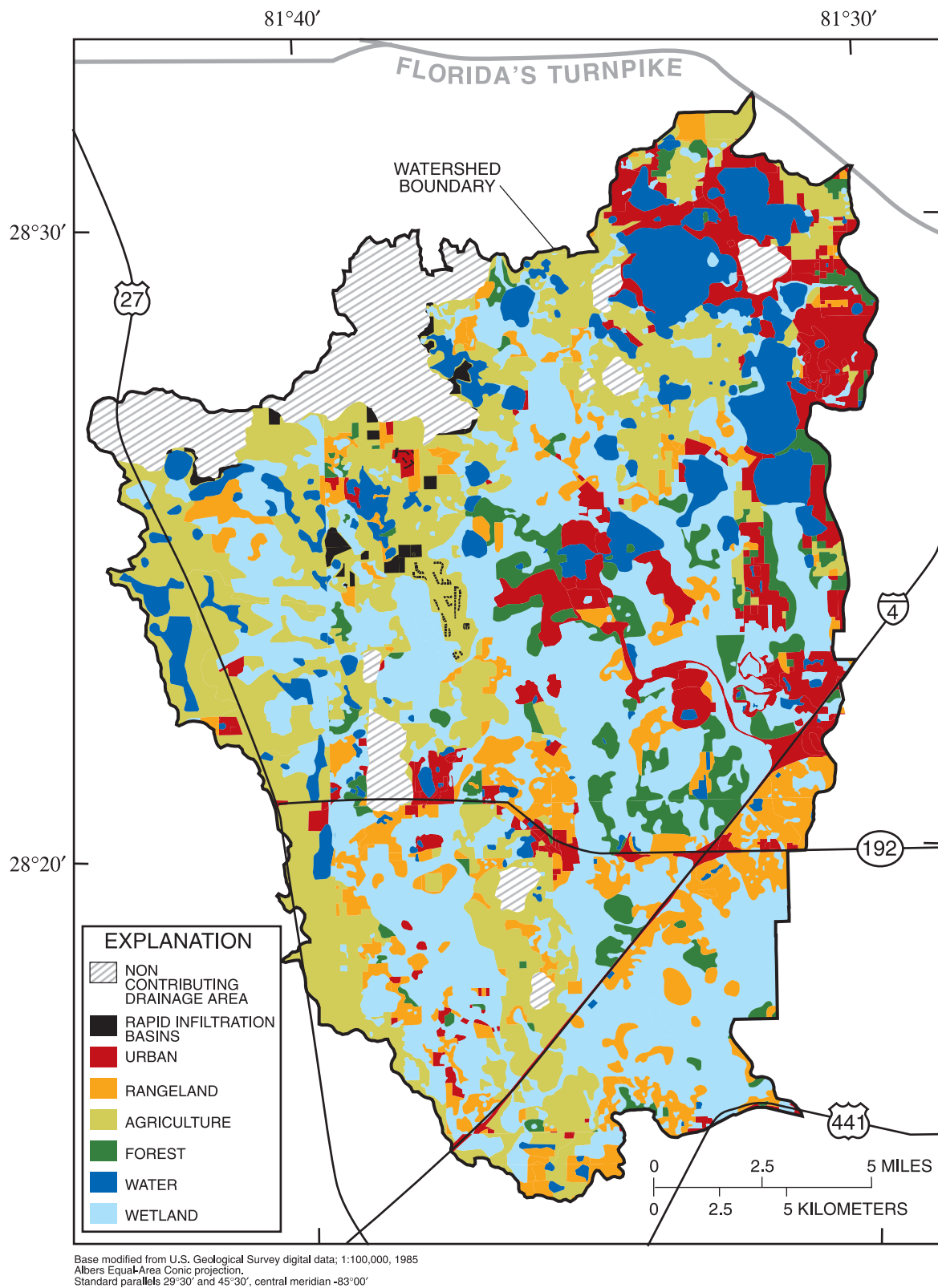
Based on the available spatial data, it was determined that six land-use types characterize the Reedy Creek watershed: agriculture, rangeland, forest, wetlands, RIBS, and urban areas (fig. 6). HSPF simulates runoff from pervious and impervious land surfaces, so the land-use types defined for the Reedy Creek watershed were grouped into pervious and impervious categories. Agriculture, rangeland, forest, wetlands, and RIBS land-use types are considered pervious land areas. Pervious and impervious land areas for urban areas were calculated based on land-use and land-cover classification in the spatial analysis (U.S. Geological Survey, 1990), impervious area percentages described in Wanielista and Yousef (1993, p. 506), and information provided by the RCID (K. Kolbo, Reedy Creek Improvement District, oral commun., 1999). Percentages of pervious and impervious land area for indicated land-use types within modeled sub-watersheds of the Reedy Creek watershed for 1990 are shown in table 5.

The watershed was divided into land segments for simulation purposes based on the location of streamflow gaging stations (table 4). A land segment is a parcel of land with distinctive but fairly uniform meteorological, physical (soil and slope), and hydrologic traits and is assumed to produce a homogeneous hydrologic and water-quality response for a given land-use type. Individual land segments with similar characteristics belong to the same land-segment type.

**Table 5.** Percentages of modeled pervious and impervious land areas based on geographic coverages from 1990 for land use types in sub-watersheds used in the Hydrological Simulation Program-Fortran model of the Reedy Creek watershed, Florida [When the sum of percentages is less than 100 percent, the remaining area is covered by open water; RIBS, rapid infiltration basins]

Sub-watershed	Pervious land area (percent)						Impervious land area (percent)
	Agriculture	Forest	Rangeland	Urban	Wetland	RIBS	
Whittenhorse Creek	27.5	2.4	19.0	1.3	43.6	0.4	0.6
Davenport Creek	45.5	2.8	16.0	3.6	26.7	0.0	1.5
Reedy Creek near Vineland	20.3	5.5	21.5	5.3	34.4	0.2	3.6
Bonnet Creek near Vineland <sup>1</sup>	2.2	10.8	14.2	9.8	40.1	0.0	13.2
Reedy Creek near Loughman <sup>1</sup>	19.9	6.0	20.0	5.4	37.3	0.1	4.1

<sup>1</sup>Does not include land areas in the Cypress Creek Basin.



**Figure 6.** Land use in the Reedy Creek watershed, Florida, used in the 1990-95 hydrologic and water-quality simulations.

Each land-segment type is assigned its own process-related parameters. Each land segment contains one or more of the six land-use types defined within the watershed. The segmentation of the land surface generally is based on the spatial variability in precipitation and differences in the physical characteristics of the watershed. Land segmentation for this study was based on topography, land use, depth to water table, and the relative altitudes of land surface and the Floridan aquifer system potentiometric surface (recharge and discharge areas). The Reedy Creek watershed was subdivided into five major land segments (fig. 7, table 6).

**Table 6.** Description of channel reaches and associated land segments assigned for routing of runoff through the Reedy Creek watershed, Florida, in the Hydrological Simulation Program-Fortran model

[mi, miles; --, not applicable; see fig. 8 for reach number, see fig. 7 for land segments]

Reach number	Reach description	Reach length (mi)	Drains to reach	Associated land segment
2	Bay Lake and Seven Seas Lagoon	1.00	3, 10	1
3	Upper L-405 Canal	5.56	6	1
4	C-4 Canal	2.13	6	1
5	L-403, EPCOT	3.36	6	1
6	Lower L-405 Canal	2.50	7	1
7	Reedy Creek near Vineland	2.01	8	1
8	Reedy Creek above I-4	2.52	15	1
9	Lake Mabel and South Lake	2.00	12	1
10	L-105 Canal	1.77	12	1
11	L-103 Canal and Lake Buena Vista	2.92	13	1
12	L-107 Canal and Upper C-1 Canal	6.75	13	1
13	Bonnet Creek near Vineland	2.37	14	1
14	Lower C-1 Canal	4.51	15	1
15	Reedy Creek at S-40	2.84	16	1
16	Reedy Creek near Loughman	--	--	1
21	Cypress Creek	--	11	2
31	Upper East Reedy Creek	1.0 <sup>1</sup>	3	3
41	Upper West Reedy Creek	1.0 <sup>1</sup>	4	3
51	Whittenhorse Creek	2.37	4	4
61	Davenport Creek	4.64	15	5

<sup>1</sup>Reach drains wetland with no clearly defined channel; reach represented as 1 mile for modeling purposes.

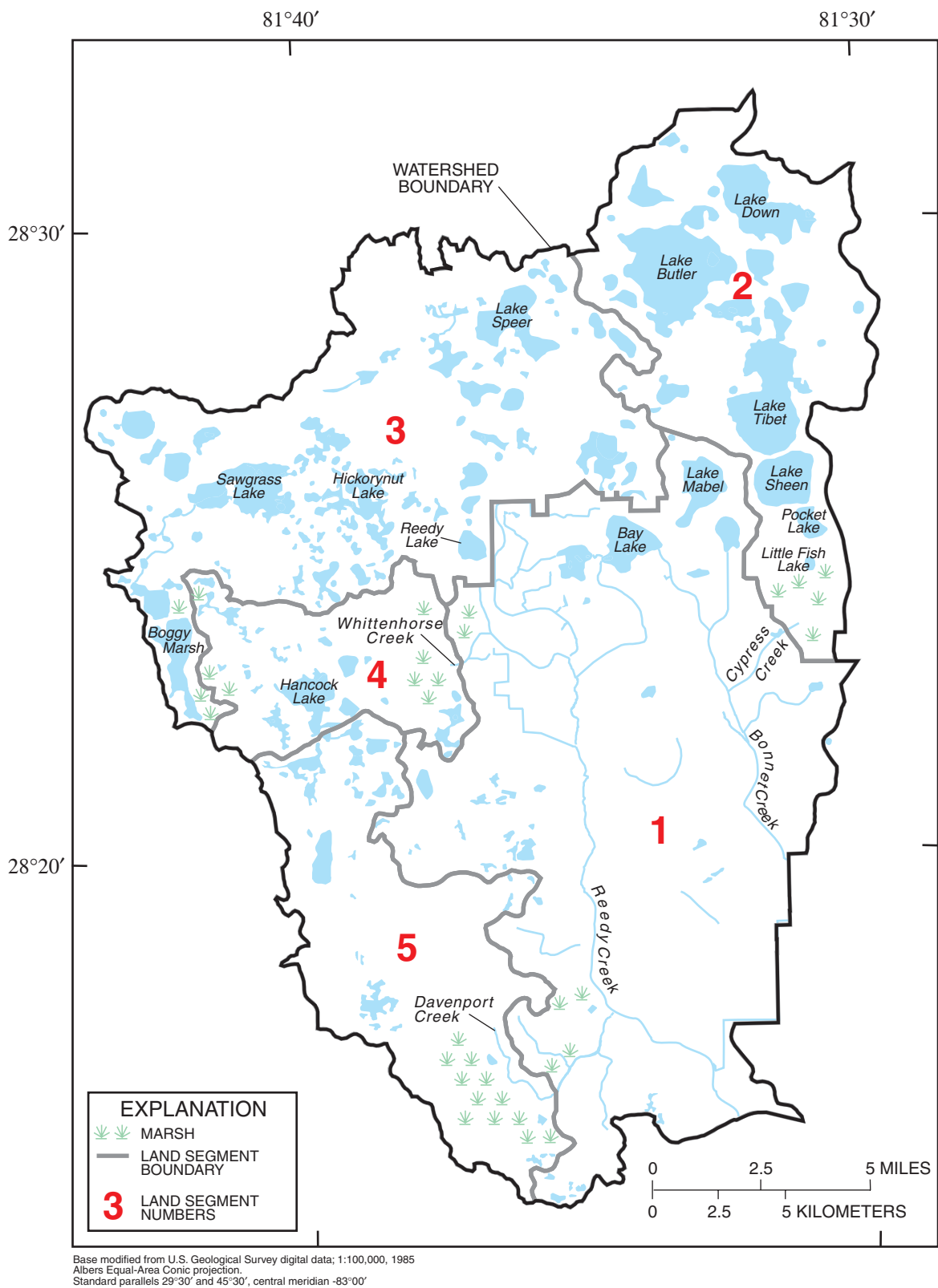
The HSPF model performs a simple routing of streamflow along channels of a drainage network to the outlet of a drainage basin. Use of the routing capability requires that a linked network of stream channels, lakes, ponds, and wetlands is divided into

segments called channel reaches. A channel reach has relatively uniform morphologic and hydraulic properties, and drains or connects sub-watersheds. Segmentation of channel reaches is somewhat generalized in the Reedy Creek watershed and is not intended to represent every culvert, ditch, pond, and channel in the drainage network.

Characterization of the stream channel system was based on measured channel cross-section data and topographic information. Cross-section data were derived from USGS streamflow records and from input files of the UNET hydraulic model (R. L. Barkau, written commun., 1992) of the RCID (M. Elsabagh, Reedy Creek Improvement District, oral commun., 1997). Accurate characterization of the stream channel is needed to provide a sound basis for routing streamflow and water-quality constituents through the channel system so that the model will approximate the observed hydrologic and water-quality data as closely as possible.

Segmentation of the stream channel reaches was based on the location of man-made structures, channel slope, and changes in the channel from natural to altered conditions (or the opposite, altered conditions to natural channel conditions). A total of 20 stream channel reaches was used to represent the movement of runoff and its constituents through stream channels and their tributaries (fig. 8, table 6). The length of the reaches varied from 1.0 to 6.8 mi. Stream reaches 31 and 41 drain low wetland areas with no clearly defined channel; the length of each reach was represented as 1 mi for modeling purposes. Each lake in the Reedy Creek watershed was not explicitly modeled. Lake and wetland areas directly linked with the stream channel network were accounted by reach-reservoir interactions in the model. Reaches 2-16 are associated with land segment 1 (RCID internal area), reach 21 (Cypress Creek) is associated with land segment 2, reaches 31 and 41 (Upper East and Upper West Reedy Creek, respectively) are associated with land segment 3, reach 51 (Whittenhorse Creek) is associated with land segment 4, and reach 61 (Davenport Creek) is associated with land segment 5 (table 6).

The HSPF source code includes 17 parameters for simulating hydrology of the rainfall-runoff process for pervious land surfaces (PERLND) and four parameters for impervious land surfaces (IMPLND) (table 1). Water quality of surface runoff was simulated in the pervious and impervious parts of the HSPF model



**Figure 7.** Distribution of land segments in the Reedy Creek watershed, Florida (land segment numbers from table 6).

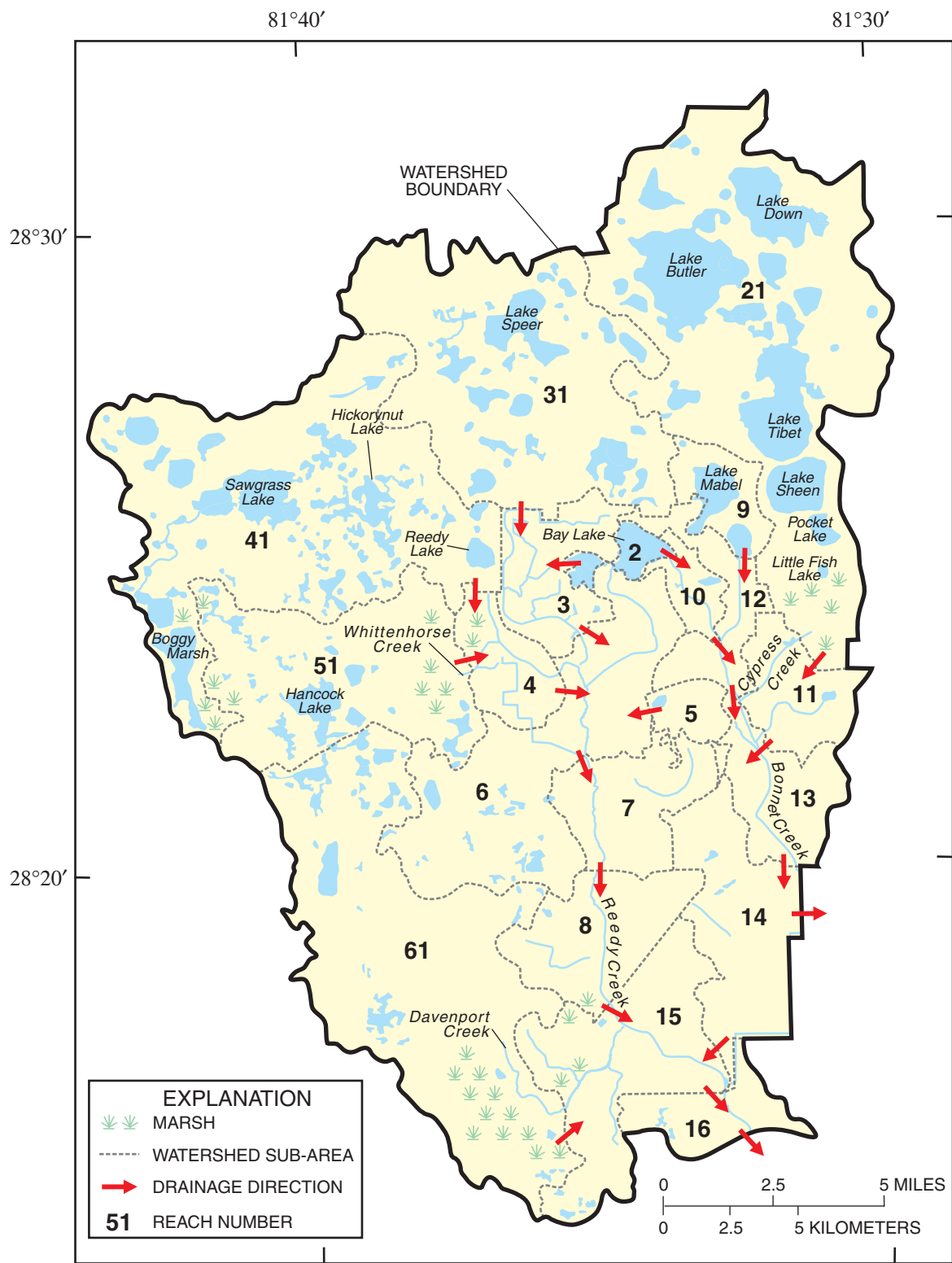


Figure 8. Surface-water reach network used in the Reedy Creek watershed, Florida (reach number from table 6).

by build-up and wash-off of constituents from the land surface. Water quality of the interflow and ground-water flow was simulated in the pervious parts of the HSPF model by contribution of a constant constituent loading for each land-use type. Nutrient cycling in-stream reaches was simulated using three water-quality subroutines in HSPF: 1) primary DO and BOD balances; 2) primary inorganic nitrogen and phosphorus balances; and 3) plankton populations (Bicknell and others, 1993). Parameters used in water-quality subroutines for simulation of nutrient cycling in-stream reaches for the Reedy Creek watershed model are listed in appendix A. Values for hydrologic parameters initially were estimated from values used in a modeling study in South Florida (AQUA TERRA Consultants and Linsley, Kraeger Associates, 1997). Water-quality parameter values initially were estimated from model input files from previous water-quality studies (U.S. Environmental Protection Agency, 2001), ground- and surface-water constituent concentration values and reactions reported by German (1986 and 1990), Hampson (1993), and Sumner and Bradner (1996), and files of the USGS in Altamonte Springs, Florida. The HSPF user control input (UCI) file used to simulate hydrology and water quality for the Reedy Creek watershed is listed in appendix D.

The Cypress Creek (fig. 2) watershed lacked sufficient rainfall data, continuous lake-stage data, and bathymetric data needed for simulation using HSPF. The closest rainfall site that could be used in the model to simulate runoff in the Cypress Creek watershed was about 1.5 mi southwest of the southern part of the watershed. Spatial variability of rainfall across the Cypress Creek watershed can cause varying lake levels among the large and numerous hydraulically interconnected lakes within the watershed. These lake level differences can result in flow reversals in the canals connecting the lakes. Wind also can affect lake levels and movement of water through the canals. Channel roughness and associated resistance to flow also can affect water movement from Pocket and Little Fish Lakes into the swamp upstream of the Cypress Creek gaging station. Adequate hydrologic modeling of the Cypress Creek watershed using HSPF would require data that were not available during the study period. After many attempts to simulate discharge from Cypress Creek with HSPF, it was determined that the best approach to modeling the entire Reedy Creek watershed was to use the observed flow and periodic

water-quality data from the USGS gaging station at Cypress Creek near Vineland as a point source for use in the hydrologic and water-quality parts of the HSPF model. Land areas within the Cypress Creek drainage were excluded from the model, and daily discharge values were input as a point source of inflow to the stream reach downstream from the USGS gaging station at Cypress Creek near Vineland.

## Hydrologic Model Calibration

Because of the complexity of the stream system within the RCID (hydraulic structures, retention ponds) and the anticipated difficulty of modeling the system, an approach of calibrating the model parameters for a subset of the gaged watersheds and confirming the usefulness of the parameters by simulating the remainder of the gaged sites was selected for this study. The use of calibrated parameter sets for regional (for example, countywide) floodplain and stormwater management on ungaged watersheds or at ungaged sites on gaged watersheds has frequently been applied since Lumb and James (1976) proposed this approach for stormwater management in DeKalb County, Georgia. This approach was commonly applied for floodplain management in northeastern Illinois (Price, 1994; Duncker and others, 1995), and also has been applied successfully in Louisville, Kentucky (Jarrett and others, 1998) and in southwestern Minnesota (Jones and Winterstein, 2000). Therefore, the calibration of HSPF model parameters at gaged sites and confirmation of the usefulness of those parameters at other gaged locations in the Reedy Creek watershed using the calibrated parameters is consistent with standard applications of the HSPF model throughout the country.

This calibration and confirmation approach was selected rather than the more common approach of calibrating a model for a given watershed and time period and then verifying the model for the same watershed for a different time period (that is, the calibration and verification approach) because of the limited availability of complete time series of meteorologic data, complex hydraulic relations within the RCID, and changes in land use during the study period (1990-95). For the calibration of HSPF, it is generally recommended that the "period of comparison should be as long as the data permit, preferably 5 years or more" (Linsley and others, 1975, p. 347). When this study began (1996), 6 years of extensive

rainfall and runoff data were available, only slightly more than the recommended minimum.

Complex hydraulics and changing land use in the Reedy Creek watershed also were limiting conditions. Flow patterns within the RCID property are extremely complex because of the many gated structures, canals, and wetlands. Thus, hydraulic effects of these structures and features could complicate the true rainfall-runoff response and its proper parameterization. By focusing the calibration effort on gaged watersheds draining into the RCID (that is, Cypress Creek, Davenport Creek, and Whittenhorse Creek), it was expected that a more reliable calibration of the rainfall-runoff response could be obtained. Also, the Reedy Creek watershed was undergoing development and it was uncertain whether 1990 land-use data (the most recent available data) could be used reliably in the simulation of runoff in the late 1990s. For these reasons, the parameter calibration and confirmation process was used.

The hydrologic part of the watershed model was calibrated through numerous iterative model runs, and model output were compared to observed data. Two sub-watersheds, Whittenhorse Creek and Davenport Creek, which are tributaries of Reedy Creek, were selected for calibration because these sub-watersheds have land-use types similar to those in the sub-watersheds elsewhere within the RCID, with the exception of urban areas (fig. 6). HSPEXP was used to assist in calibration of the Davenport Creek and Whittenhorse

Creek sub-watersheds. The default fit criteria used by HSPEXP (Lumb and others, 1994, p. 56) were modified to aid in obtaining better agreement between simulated and observed values (table 7). Simulated and observed water balances were compared for overall (the entire period from January 1990 through December 1995), annual, monthly, and storm-runoff event time periods. Model parameters were adjusted iteratively until the best-fit model was obtained.

Model parameters were adjusted for the calibration sub-watersheds, Whittenhorse Creek and Davenport Creek, to match overall (1990-95), annual, and monthly runoff volumes, and then to obtain agreement between the observed and simulated storm runoff volumes and runoff-duration curves of daily runoff. Graphical and statistical methods were used to assess the quality of model fit. Statistics can provide a measure of model improvement, and trends and biases can be detected graphically. The model was calibrated using an hourly computational time step and data were output at a daily time step for a 6-year period, January 1990 to December 1995.

The percent error between simulated and observed values was used to calibrate the overall, annual, and monthly water balances. Donigan and others (1984) state that for HSPF simulations, the annual or monthly fit is very good when the error is less than 10 percent, good when the error is 10 to 15 percent, and fair when the error is 15 to 25 percent.

**Table 7.** Hydrological Simulation Program-Fortran EXPert system (HSPEXP) default fit-quality criteria, fit-quality criteria used for calibration and confirmation of the Hydrological Simulation Program-Fortran (HSPF) rainfall-runoff hydrologic simulation, and calibration and confirmation sites simulated in the Reedy Creek watershed, Florida

[Criteria and error difference between simulated and observed values are in percent difference between simulated and observed values, with the exception of the error in low-flow recession, which is expressed as the absolute value of the difference between simulated and observed values]

Statistics	Criteria		Error difference between simulated and observed values				
	Default	Modeled	Whittenhorse Creek	Davenport Creek	Reedy Creek near Vineland	Bonnet Creek	Reedy Creek near Loughman
Error in total volume	10.0	10.0	-2.8	1.6	-12.2	-29.2	7.4
Error in low-flow recession	0.03	0.03	-0.02	-0.03	-0.02	-0.03	0.02
Error in 50 percent lowest flows	10.0	10.0	-3.3	12.6	-37.0	-59.6	-26.4
Error in 10 percent highest flows	15.0	15.0	1.9	-5.2	-3.0	-26.6	11.3
Error in storm volumes	20.0	15.0	7.6	20.8	-2.4	-8.5	138.3
Seasonal volume error	30.0	10.0	6.9	35.5	19.0	16.1	17.9
Summer storm volume error	50.0	15.0	-16.1	-14.5	24.8	-14.8	111.8

The quality of fit of the monthly streamflow values also was evaluated using the three statistics: 1) correlation coefficient between simulated and observed discharge; 2) coefficient of model-fit efficiency between simulated and observed flow; and 3) number of months where the percent error was less than a specific value (10 and 25 percent). The correlation coefficient,  $C$ , is calculated as:

$$C = \frac{\sum_{i=1}^N (Qo_i - Qo) \times (Qs_i - Qs)}{\left[ \sum_{i=1}^N (Qo_i - Qo)^2 \times \sum_{i=1}^N (Qs_i - Qs)^2 \right]^{0.5}}, \quad (1)$$

where

- $Qo_i$  is the observed runoff volume for month  $i$ ,
- $Qo$  is the observed average monthly runoff volume,
- $Qs_i$  is the simulated runoff volume for month  $i$ ,
- $Qs$  is the simulated average monthly runoff volume, and
- $N$  is the number of months in the calibration period.

The coefficient of model-fit efficiency,  $E$  (Nash and Sutcliffe, 1970), is calculated as:

$$E = \frac{\sum_{i=1}^N (Qo_i - Qo)^2 - \frac{(\sum_{i=1}^N (Qo_i - Qs_i))^2}{N}}{\sum_{i=1}^N (Qo_i - Qo)^2} \quad (2)$$

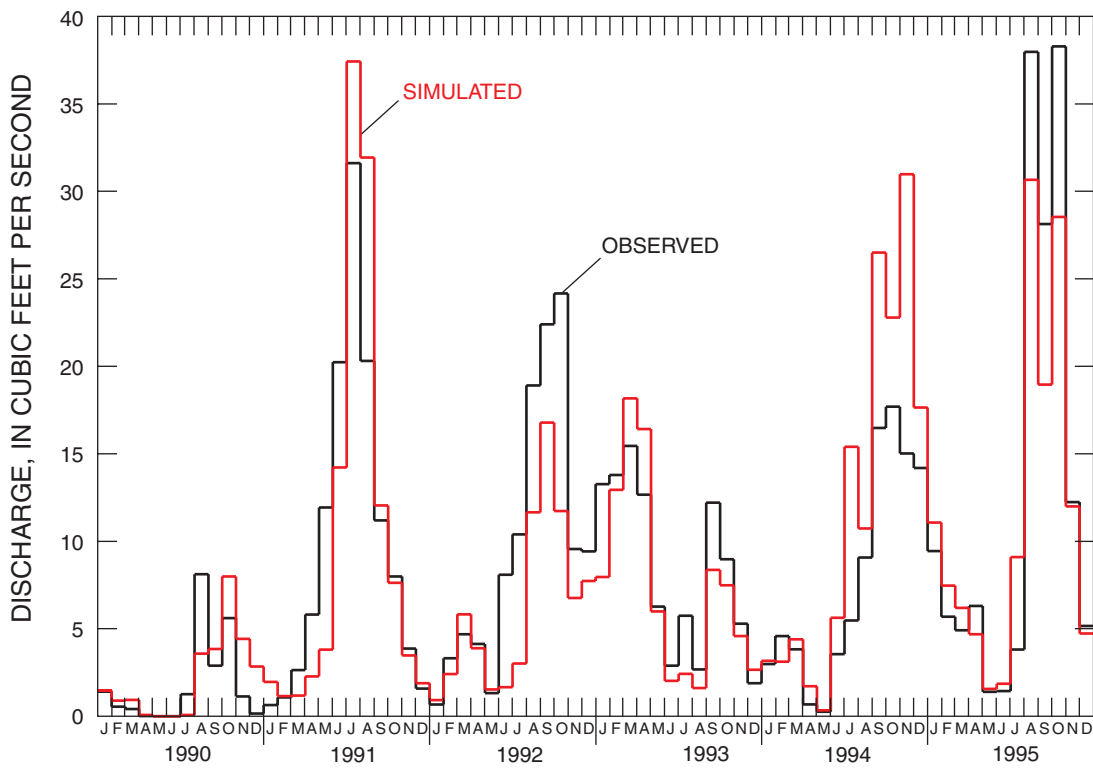
Studies cited by Duncker and others (1995) had coefficient of model-fit efficiencies varying from 0.80 to 0.98 for basins ranging in size from 0.88 to 1,342 mi<sup>2</sup> and model periods of 4 to 8 years. For the purposes of this study, the model fit was considered excellent if the coefficient of model-fit efficiency was greater than 0.97, good when greater than 0.9, and fair when greater than 0.8.

Daily flows were evaluated graphically by comparing the observed and simulated daily runoff-duration curves and time series. General agreement between the simulated and observed runoff-duration curves indicates adequate calibration over the range of simulated flow conditions. Inadequate calibration is indicated by significant departures between simulated and observed runoff-duration curves. The model calibration obtained “best-fit” simulations for Whittenhorse Creek (land segment 4) and Davenport Creek (land segment 5). Each land segment was calibrated separately, and calibration parameters for pervious and impervious land areas are presented in appendix B.

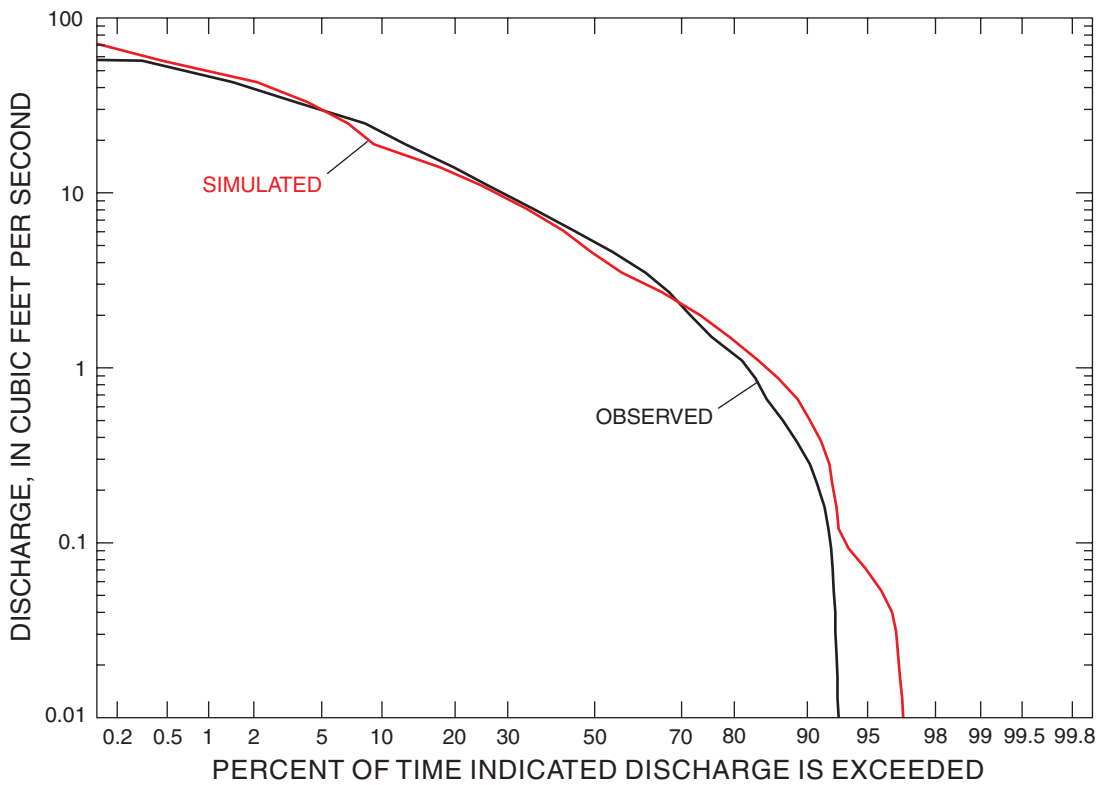
Simulated flows for Whittenhorse Creek agreed with observed flows for six of the seven fit-quality criteria specified in HSPEXP for calibration of HSPF (table 7). The default criterion for the error in summer storm volume is 50 percent and the calibration result yielded an error of -16.1 percent, less than 1 percent difference from the more stringent criterion (15 percent). Further, the criteria used in this study are more stringent than the default criteria listed in the user’s manual for HSPEXP (Lumb and others, 1994, p. 56) (table 7). According to the criteria of Donigan and others (1984), the overall water balance for the Whittenhorse Creek calibration was very good, and the annual water balances ranged from very good to poor over the simulation period. Observed and simulated monthly mean time series plots show the fit of the hydrologic calibration for Whittenhorse Creek (fig. 9). Duration curves of observed and simulated daily mean discharge at Whittenhorse Creek indicate good agreement for values above a discharge of about 1.0 ft<sup>3</sup>/s (fig. 10).

Simulated flows for Davenport Creek agreed with observed flows for four of the seven fit-quality criteria specified in HSPEXP for this study: error in total volume, error in low-flow recession, error in 10 percent highest flows, and error in summer storm volumes (table 7). The error in 50 percent lowest flows was 12.6 percent, and the HSPEXP criterion use in this study was 10 percent. The error in 50 percent lowest flows was considered close enough to the HSPEXP criterion to be marginally acceptable. Adjustment of parameter values affecting the 50 percent lowest flows had adverse affects on other criteria specified in HSPEXP. The default criterion for the error in storm volumes is 20 percent, and the calibration result





**Figure 9.** Simulated and observed monthly mean discharge values at Whittenhorse Creek near Vineland, Florida.



**Figure 10.** Discharge duration curves for simulated and observed daily mean values at Whittenhorse Creek near Vineland, Florida.

yielded an error of 20.8 percent. The simulated storm volumes matched the observed values close to the HSPEXP default criterion, but not the more stringent criterion set for this study (15 percent). The obtained result was close enough to the default HSPEXP criterion for error in storm volumes that it was considered acceptable. The seasonal volume error (35.5 percent) was larger than the HSPEXP default criterion of 30 percent; however, the fixed specification for HSPEXP of the seasons as June-August and December-February does not always match seasonal trends in the study area. This criterion may be given reduced weight or omitted from the judgment regarding the acceptability of the model fit for sub-areas within the Reedy Creek watershed. According to the criteria of Donigian and others (1984), the overall water balance for the Davenport Creek calibration was very good, and the annual water balances ranged from very good to fair over the simulation period. A plot of observed and simulated monthly mean discharge (fig. 11) shows the fit of the Davenport Creek calibration. Duration curves of observed and simulated daily mean discharge at Davenport Creek indicate an acceptable fit for discharges that were exceeded 90 percent of the time over the simulated period, that is, for discharges greater than 3 ft<sup>3</sup>/s (fig. 12).

Hydrologic model calibration statistics for Whittenhorse and Davenport Creeks over the 72-month simulation period, January 1990 to December 1995, are listed in table 8. The correlation coefficients, coefficients of model-fit efficiency, and other statistics of monthly flows for Whittenhorse Creek and Davenport Creek are not as good as those obtained in other studies summarized in Duncker and Melching (1998) because the quality and distribution

of rainfall data available for the Reedy Creek watershed are not as good as the data in those studies. Specifically, watersheds where high coefficients of model-fit efficiency were reported typically had several rainfall gages in or very close to the watershed and were located in parts of the country having less spatial variability in rainfall than the Reedy Creek watershed. The coefficients of model-fit efficiency for monthly flows obtained for Whittenhorse Creek and Davenport Creek are similar to those obtained in simulations of the Minnesota River basin in Minnesota (correlation coefficient between 0.877 and 0.927; coefficient of model-fit efficiency between 0.702 and 0.851) (S.E. Kroening, U.S. Geological Survey, oral comm., 2001). Given the lack of available rainfall data, the hydrologic calibration of the Whittenhorse Creek and Davenport Creek sub-watersheds was considered acceptable.

## Hydrologic Model Confirmation

Confirmation that the model parameter set results in an acceptable simulation of runoff for hydrologically similar watersheds provides a means of evaluating the parameter set. An acceptable confirmation indicates that the calibrated parameter set may be suitable for simulation of runoff in similar parts of the Reedy Creek watershed. The parameter set developed from the calibration can be transferred to other land areas in the Reedy Creek watershed. The validity of the parameter set is indicated by the goodness-of-fit of the simulated flows to the observed flows at selected confirmation sites.

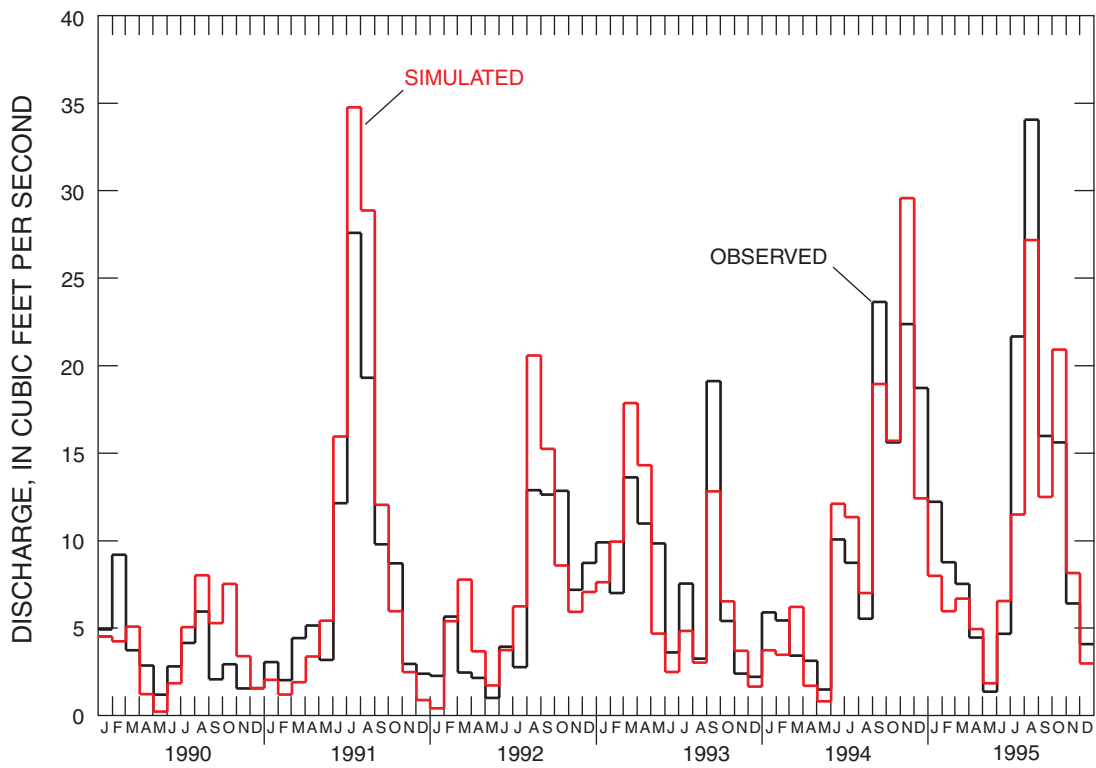
The hydrologic model was tested by applying the parameter sets developed for Whittenhorse Creek and Davenport Creek to other land segments within the Reedy Creek watershed, and by comparing the

**Table 8.** Hydrological Simulation Program-Fortran calibration and confirmation statistics for monthly flows simulated for five sites over a 6-year (72-month) period (1990-95) in the Reedy Creek watershed, Florida

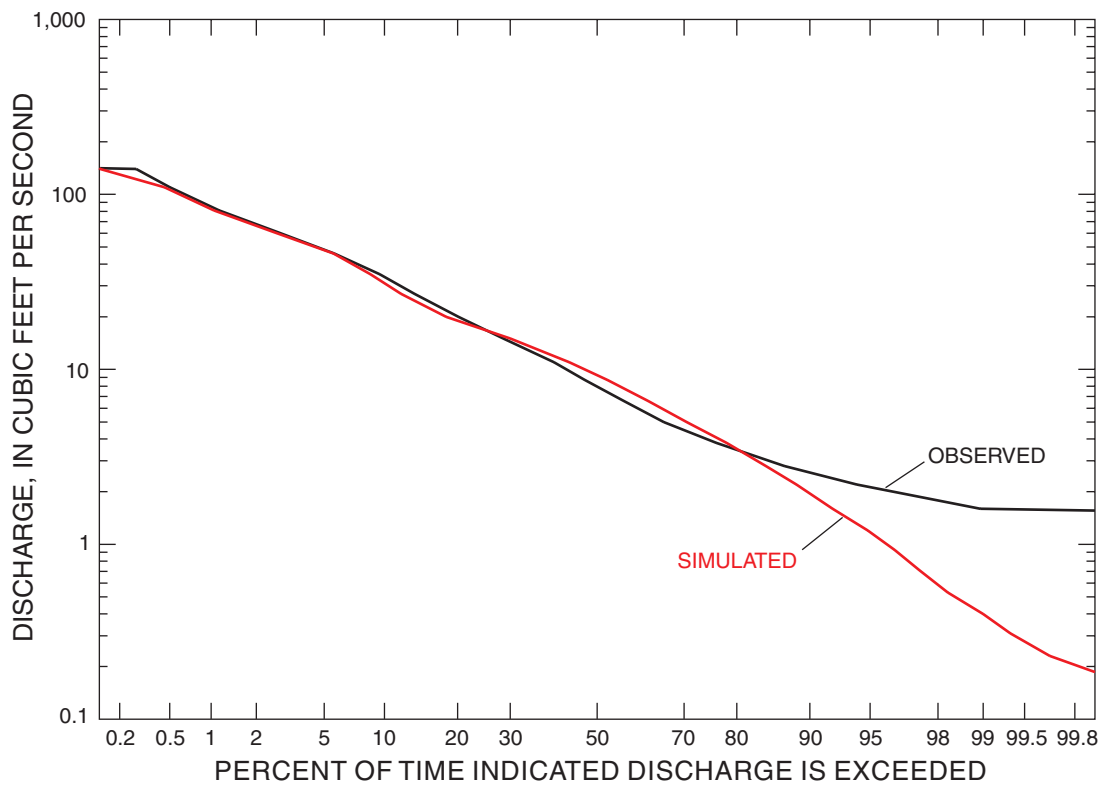
	Calibration		Confirmation		
	Whittenhorse Creek near Vineland	Davenport Creek near Loughman	Reedy Creek near Vineland	Bonnet Creek near Vineland	Reedy Creek near Loughman
Coefficient of model-fit efficiency	0.7166	0.7535	0.7846	0.6780	0.7741
Correlation coefficient	.8593	.8808	.9072	.9043	.8839
Number of months with a very good fit <sup>1</sup>	12	7	10	7	4
Number of months with a fair fit <sup>2</sup>	27	21	26	23	14

<sup>1</sup>Number of months when the difference between simulated and observed average monthly discharge was less than 10 percent.

<sup>2</sup>Number of months when the difference between simulated and observed average monthly discharge was less than 25 percent.



**Figure 11.** Observed and simulated monthly mean discharge values at Davenport Creek near Loughman, Florida.



**Figure 12.** Discharge duration curves for simulated and observed daily mean values at Davenport Creek near Loughman, Florida.

simulated results to observed data sets. Calibration sub-watersheds are directly associated with land segments within the modeled watershed; land segment 4 is synonymous with the Whittenhorse Creek calibration sub-watershed, and land segment 5 is synonymous with the Davenport Creek calibration sub-watershed. Similarities in characteristics among land segments, such as distribution of land-use types, topography, and hydrology determined whether parameters developed from the calibration step could be applied to another land segment. The model parameters developed from the Whittenhorse Creek calibration (land segment 4) were applied to land segment 3 (Upper East and Upper West Reedy Creeks); the model parameters developed for Davenport Creek (land segment 5) were applied to land segment 1 (internal RCID and southern part of the watershed) (appendix B and fig. 7).

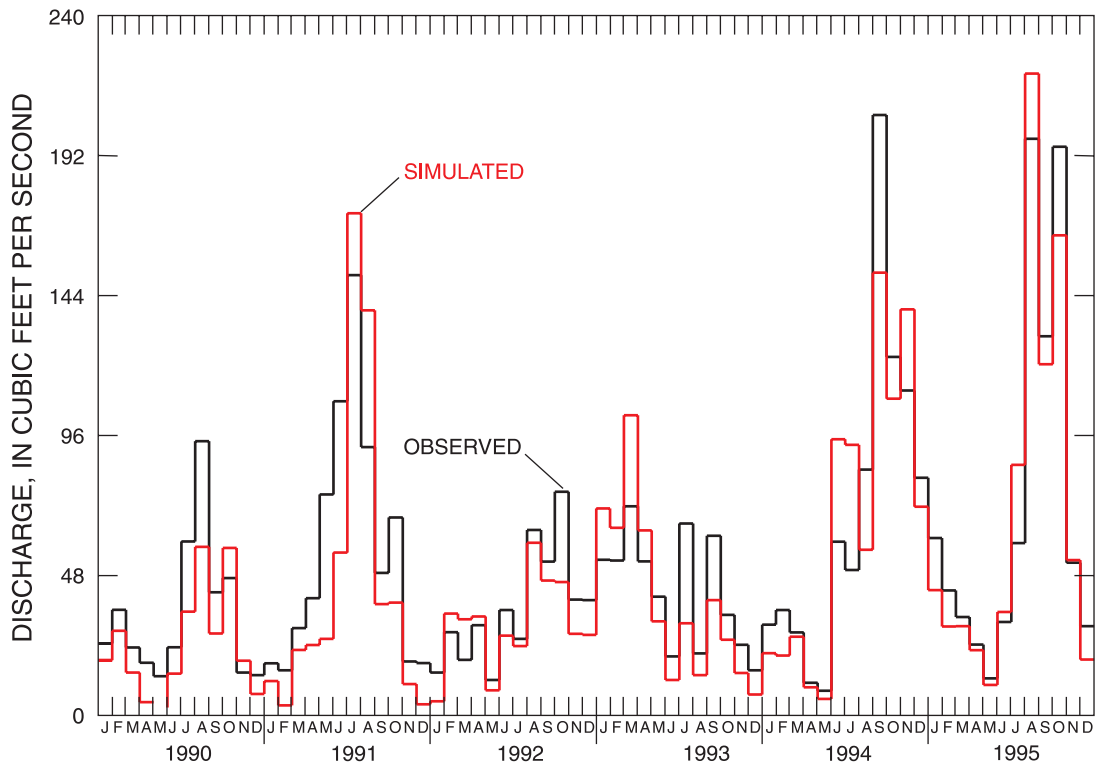
Simulated flows for Reedy Creek near Vineland agreed with the observed flows for three of the seven fit-quality criteria specified in HSPEXP for this study: error in low-flow recession, error in 10 percent highest flows, and error in storm volumes. If the default criteria listed in the user's manual for HSPEXP (Lumb and others, 1994, p. 56) were applied, five of the seven fit-quality criteria would be met, including errors in: low-flow recession, 10 percent highest flows, storm volumes, seasonal volumes, and summer storm volumes. The errors that exceed the HSPEXP criteria are related to simulation of the lowest flows: error in total volume and error in 50 percent lowest flows. The error in total volume was largely affected by the under simulation of flows below about 100 ft<sup>3</sup>/s. The overall water balance for the Reedy Creek near Vineland model confirmation was good, and the annual water balances ranged from good to poor over the simulation period using the criteria of Donigian and others (1984). Observed and simulated monthly mean time series plots show the fit of the hydrologic confirmation for Reedy Creek near Vineland (fig. 13). Duration curves of observed and simulated daily mean discharges confirm the errors noted in the simulation of the lowest flows as indicated by divergence of the curves above an exceedance of 50 percent (fig. 14). A slight divergence of the curves is also seen below an exceedance of about 1 percent.

The correlation coefficient and coefficient of model-fit efficiency and other statistics generated for monthly flows for Reedy Creek near Vineland (table 8) are not as good as those obtained in other

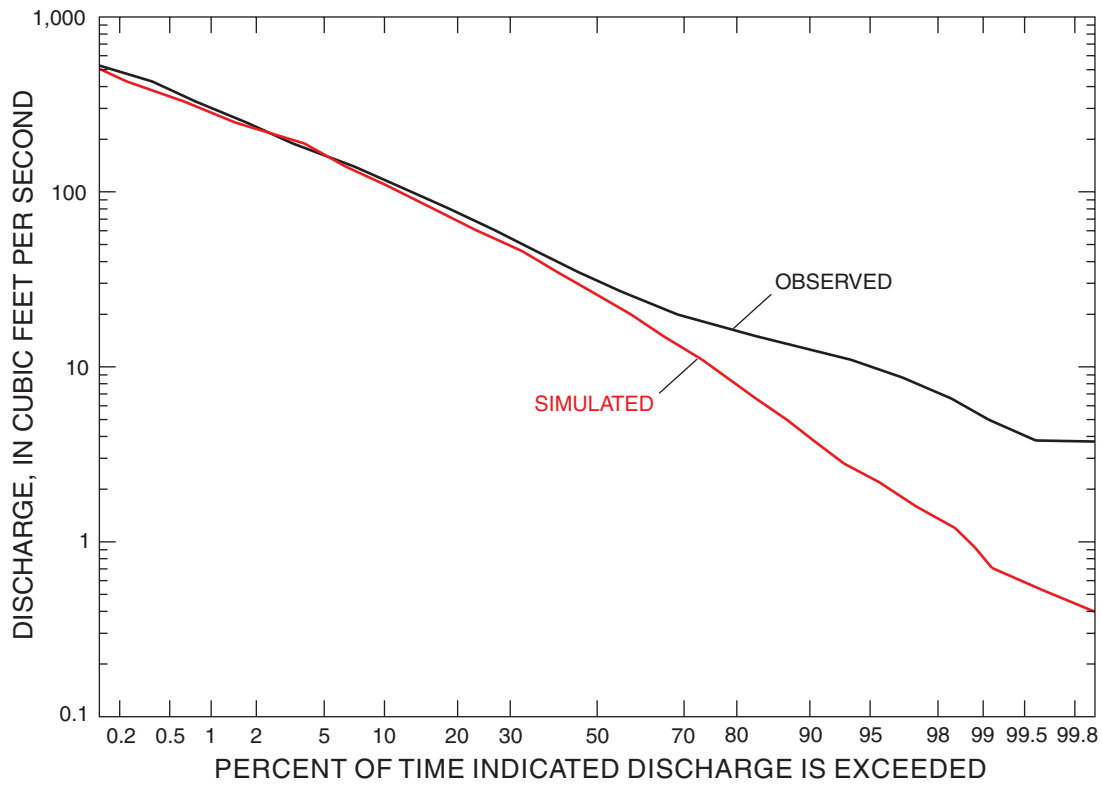
studies summarized in Duncker and Melching (1998). However, the coefficients of model-fit efficiency for monthly flows are better than those obtained for either calibration sub-watersheds, Whittenhorse Creek and Davenport Creek, and similar to those obtained in the Minnesota River basin in Minnesota (S.E. Kroening, U.S. Geological Survey, oral comm., 2001). The fact that better statistical fit coefficients were calculated for the confirmation site than for the calibration sites indicates that a sound conceptual model has been developed. Given the inadequate distribution of rainfall gaging stations throughout the watershed, the hydrologic confirmation for Reedy Creek at Vineland was considered acceptable.

Flows for Bonnet Creek near Vineland were substantially under simulated. The total simulated runoff volume was about 71 percent of the total observed runoff volume over the study period. Thus, the difference in total simulated runoff volume was about 29 percent. The overall water balance for the Bonnet Creek near Vineland model confirmation was poor, and annual water balances ranged from good to poor over the simulation period using the criteria of Donigian and others (1984). Plots of observed and simulated monthly mean discharges indicate under simulation of discharges during all years of the simulated period (fig. 15). Duration curves of daily mean discharge also indicate an under simulation of discharges throughout the range of discharge (fig. 16). Observed discharge data for the Cypress Creek near Vineland gaging station were input as a point source upstream from the Bonnet Creek near Vineland model confirmation site. Therefore, the error between simulated and observed discharge at the Bonnet Creek near Vineland site is attributed to the simulation of the intervening area between the Cypress Creek and Bonnet Creek gaging stations. Hydrologic model confirmation statistics for Bonnet Creek near Vineland over the 72-month simulation period, January 1990 to December 1995, are listed in table 8.

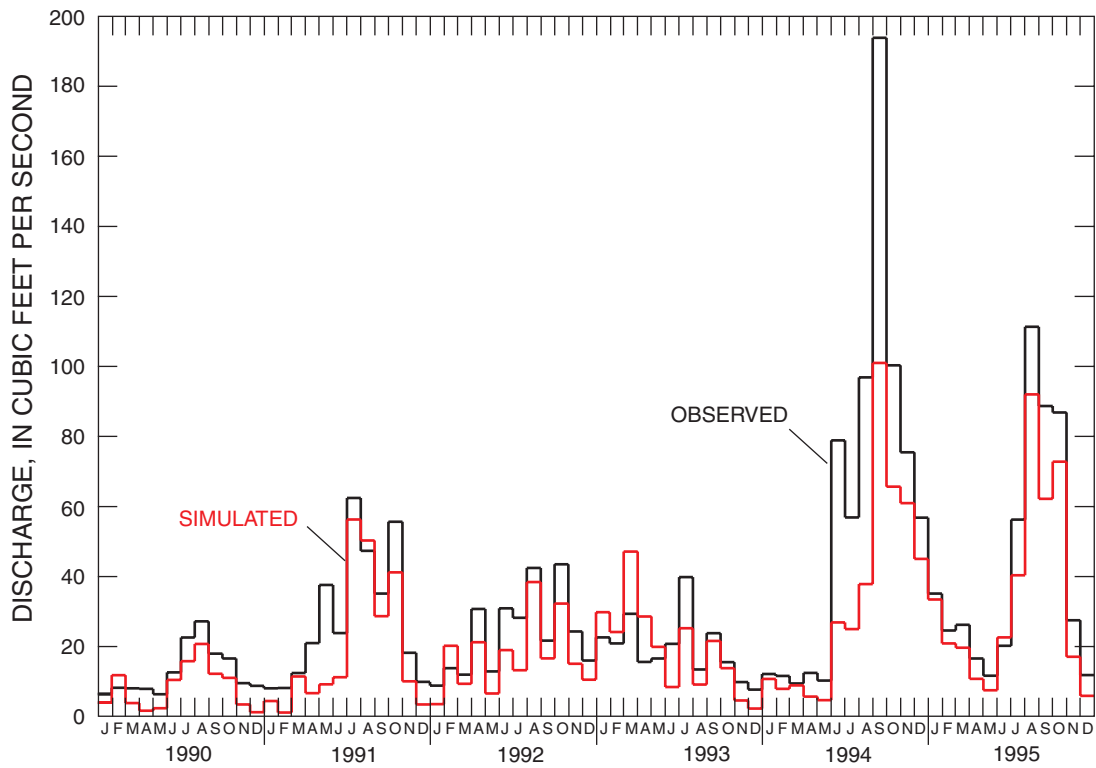
Part of the difficulty in simulating the area between the Cypress Creek and Bonnet Creek gaging stations was due to uncertainty in the size of the contributing drainage area. German (1986 and 1989) approximated the intervening drainage area between the Cypress Creek and Bonnet Creek gaging stations to be about 26 mi<sup>2</sup>; however, the annual water resources report (U.S. Geological Survey, 2000) indicates the area is 15.4 mi<sup>2</sup>. Additionally, the area between the Cypress Creek and Bonnet Creek gaging



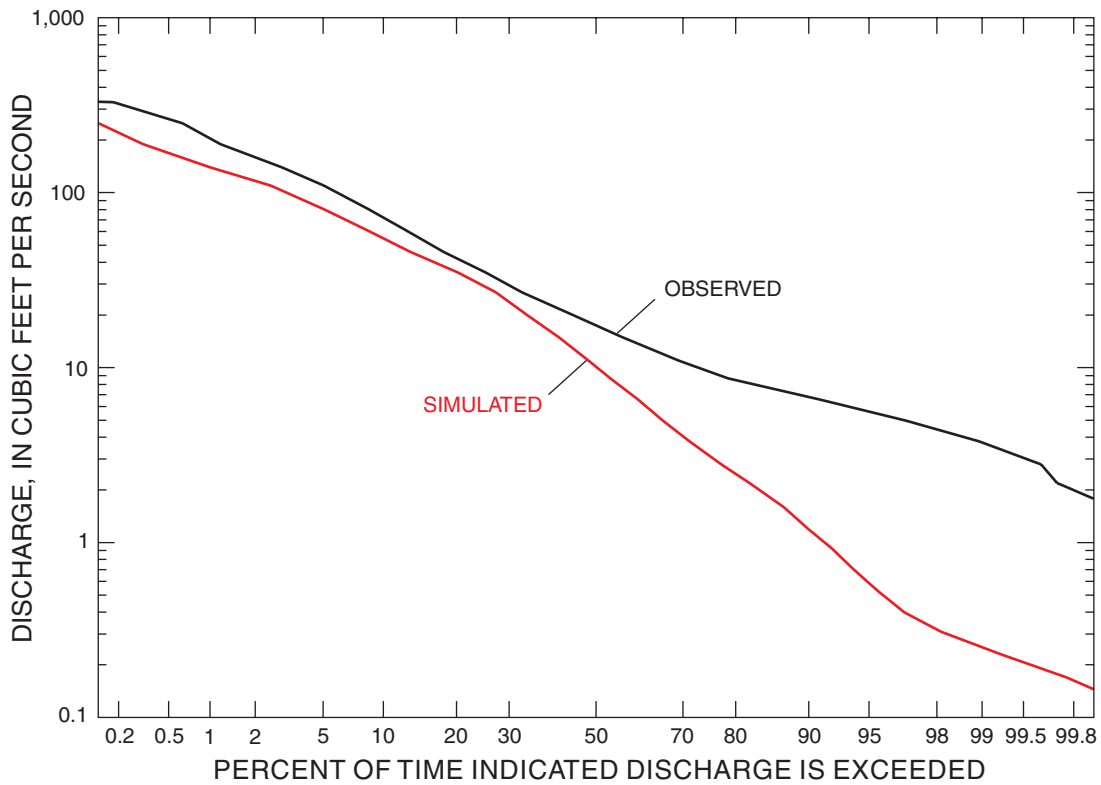
**Figure 13.** Observed and simulated monthly mean discharge values at Reedy Creek near Vineland, Florida.



**Figure 14.** Discharge duration curves for observed and simulated daily mean values at Reedy Creek near Vineland, Florida.



**Figure 15.** Observed and simulated monthly mean discharge values at Bonnet Creek near Vineland, Florida.



**Figure 16.** Discharge duration curves for observed and simulated daily mean values at Bonnet Creek near Vineland, Florida.

stations contains a substantial amount of impervious area. Streamflow records for Cypress and Bonnet Creeks near Vineland are rated as “fair” and “poor,” respectively (U.S. Geological Survey, 2000). Further, the hydraulic control at Bonnet Creek is a sheet-pile weir with sluice gate, located a short distance downstream from the gage. If the weir and gate are operated consistently, then the stage-discharge rating at the site should be stable. Examination of changes in the stage-discharge relation for the site, however, indicates substantial shifts that seem inconsistent for this type of control, further increasing the uncertainty regarding the data at this site.

Another source of error in simulating flow in the areas between the Cypress Creek and Bonnet Creek gaging stations may relate to discrepancies between surface-water and ground-water flow divides. The current model boundary reasonably defines the eastern surface-water drainage boundary; however, ground water may be a significant source of baseflow in parts of the Reedy Creek watershed (O’Reilly, 1998). It is possible that ground water is contributing an indeterminate amount of water to the lower Bonnet Creek drainage. Consideration of ground-water contribution to Bonnet Creek could improve the water balance simulation for Bonnet Creek near Vineland; however, a thorough evaluation of the ground-water contribution is beyond the scope of the current study.

On longer time scales (monthly or over the 72-month simulation period) the simulated monthly discharges from Reedy Creek near Loughman agreed well with observed data (fig. 17). Simulated flows for Reedy Creek near Loughman agreed with the observed flows for three of the seven fit-quality criteria specified in HSPEXP for this study: error in total volume, error in low-flow recession, and error in 10 percent highest flows. The water balance for the entire study period is matched within 8 percent, and the monthly flows achieved the second highest value of the coefficient of model-fit efficiency among all the sites in this study (table 8). On a shorter time scale (less than a month), however, storm volumes are greatly over simulated and low flows (less than 8 ft<sup>3</sup>/s) are greatly under simulated. Duration curves of observed and simulated daily mean discharge reflect the poor representation of the high and low distribution of daily discharges (fig. 18). A primary reason for the poor results at low flows is the diversion of an unknown amount of water from the RCID at the Bonnet Creek near Kissimmee site (fig. 2, map

number 23). The simulation results at Reedy Creek near Loughman likely can be improved once the quantity of the diversion is known. The difficulties in the simulation of the flow at Reedy Creek near Loughman also result from the under simulation of flow at Bonnet Creek near Vineland. Finally, the hydrologic flow routing applied in HSPF is poorly suited to the complex hydraulics in the large wetland conservation area between Highway 192 (Reedy Creek near Vineland and Bonnet Creek near Vineland) and the Reedy Creek near Loughman gaging station.

Results of the hydrologic modeling indicate that the regional confirmation approach worked well for flow simulation at Reedy Creek near Vineland. There were, however, a number of complications in simulating flows at Bonnet Creek near Vineland and Reedy Creek near Loughman; these complications support the original concerns about the complexities of simulating flows within the RCID boundary. The decision to calibrate the rainfall-runoff model parameters for the sub-watersheds draining to the RCID and confirm the usefulness of these parameters at gages within the RCID probably yielded better results than if model calibration had been done for the observed discharges at each streamflow gage.

Given the uncertainty in the rainfall data used to drive the HSPF model, the model yields acceptably reliable simulations of flow for Whittenhorse Creek, Davenport Creek, and Reedy Creek near Vineland. The simulation of flows at Bonnet Creek near Vineland is questionable primarily because of the uncertainty in the drainage area of Bonnet Creek near Vineland. The simulation of flows for Reedy Creek near Loughman also is questionable because of the uncertainty in the simulated Bonnet Creek near Vineland flows, the uncertain amount of diversion at Bonnet Creek near Kissimmee, and the difficulties of simulating complex flow in the large wetland conservation area between Highway 192 and the Reedy Creek near Loughman gaging station.

## Water-Quality Model Calibration

Selection of water-quality constituents for simulation was based primarily on the availability of water-quality data for sites throughout the Reedy Creek watershed (table 4). Dissolved oxygen, nitrogen, and phosphorus species were simulated because of the availability of observed continuous and periodic water-quality data. Representation of nutrient cycling

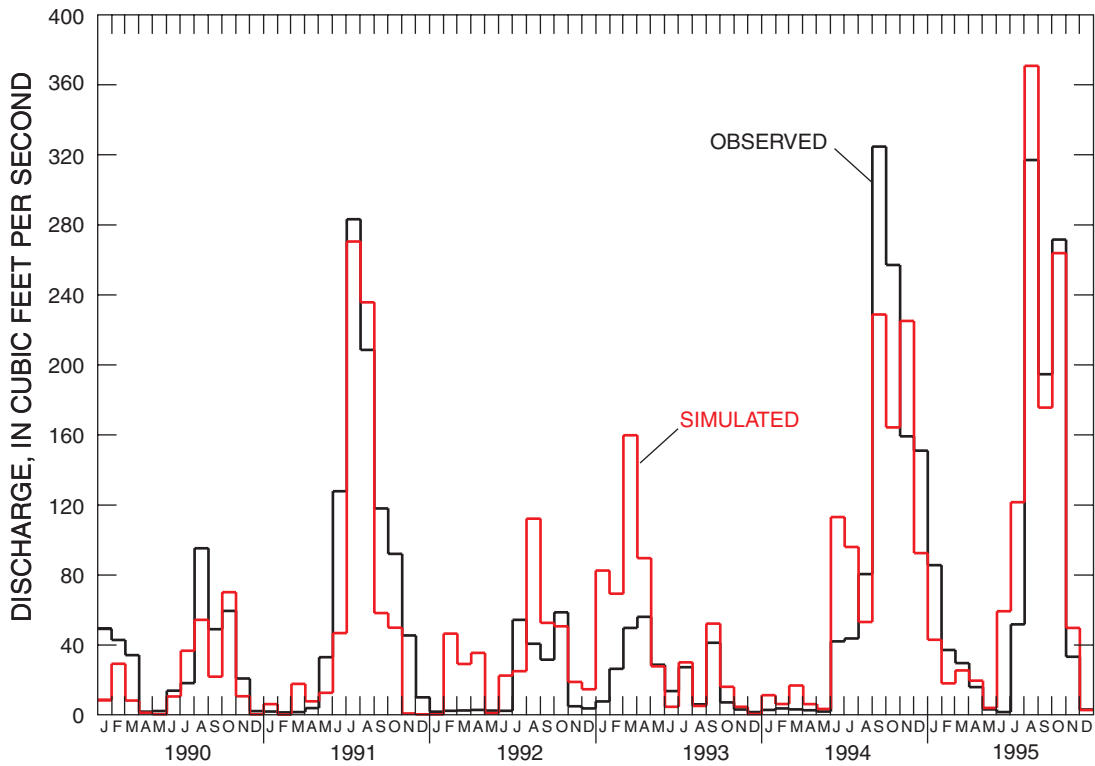


Figure 17. Observed and simulated monthly mean discharge values at Reedy Creek near Loughman, Florida.

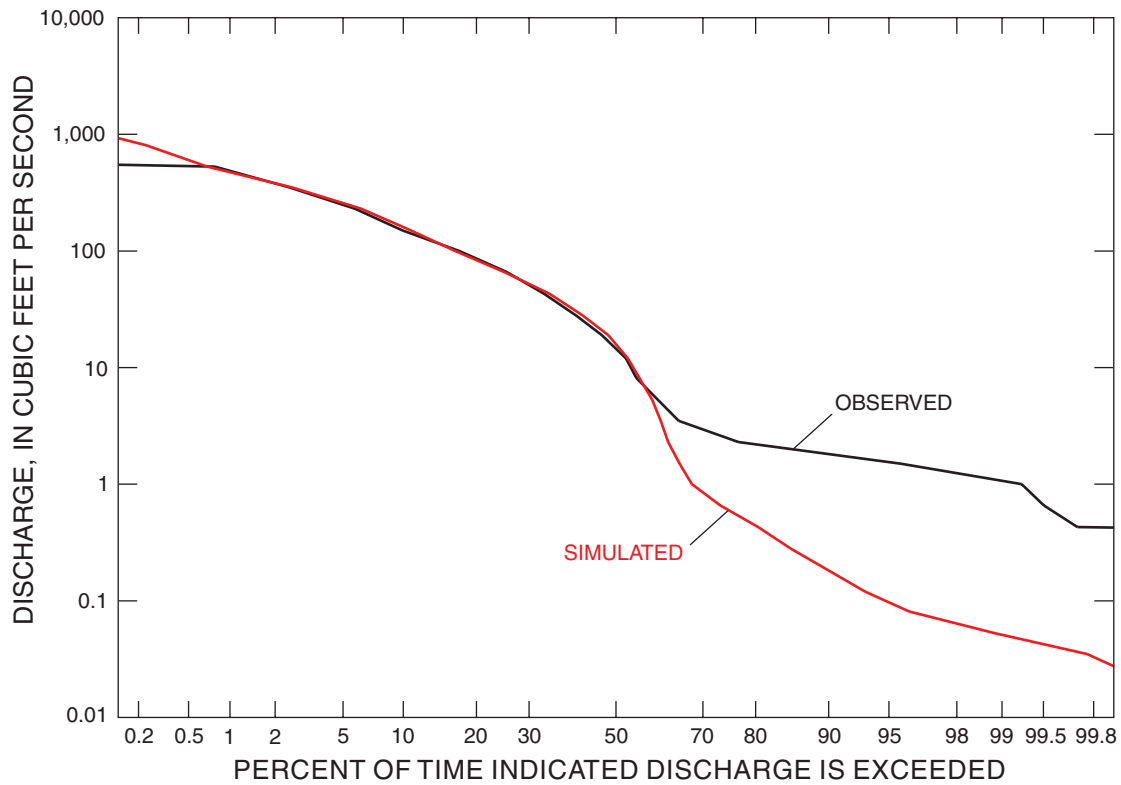


Figure 18. Discharge duration curves for Observed and simulated daily mean values at Reedy Creek near Loughman, Florida.



in HSPF also requires simulation of BOD and phytoplankton populations. In addition to precipitation and potential ET used in the hydrologic part of the model, continuous records of solar radiation, air and water temperature, wind speed, and atmospheric deposition of ammonia and nitrate nitrogen were used as input to the water-quality part of the model (tables 2 and 4, appendix D). Ground-water quality data from surficial aquifer system monitoring wells also were used to evaluate the water-quality part of the model.

Simulated water-quality constituent loadings from land areas within the Cypress Creek drainage were excluded from the water-quality part of the model. A discussion of difficulties in representing the Cypress Creek sub-watershed in the HSPF model was presented previously in this report. Daily constituent loadings of DO, BOD, ammonia nitrogen, nitrate nitrogen, and total phosphorus were input as a point source of inflow to the stream reach downstream from the Cypress Creek near Vineland gaging station. Mean monthly DO concentrations were computed from 57 periodic observations of DO concentration at the Cypress Creek near Vineland gaging station from 1989-96. The mean monthly DO concentrations were disaggregated using the mean monthly value for each day of the month to create a daily mean concentration time series for each day of the year. The daily time series of DO concentrations computed for a 1 year period were applied to each year of the simulation period (1990-95). Daily DO concentrations were combined with daily streamflow values to calculate daily constituent loadings. Linear interpolation was applied between periodic observations of constituent concentration for ammonia nitrogen, nitrate nitrogen, and total phosphorus to create a daily constituent concentration time series. Daily constituent concentrations of ammonia nitrogen, nitrate nitrogen, and total phosphorus were combined with the daily streamflow values to calculate daily constituent loadings. Time series of BOD loadings were estimated from 13 periodic observations of BOD concentration for 1994-96 from other locations in the Reedy Creek watershed. Based on these observations and empirical knowledge of the hydrologic and water-quality conditions at the Cypress Creek gaging station, a constant value was used to represent the BOD concentration for the simulation period. Daily values of streamflow were combined with the constant BOD concentration to obtain a time series of daily BOD loading.

The water-quality part of the model was calibrated in an iterative manner. Calibration of water-quality constituents was performed by visual comparison of observed and simulated constituent concentrations except for DO, which was calibrated using a statistical comparison. Parameters pertaining to DO were calibrated based on observed data for the site at Reedy Creek near Vineland (fig. 2, map number 29); parameters pertaining to other constituents were calibrated based on observed data for Whittenhorse Creek, Davenport Creek, Reedy Creek near Vineland, Bonnet Creek near Vineland, and Reedy Creek near Loughman.

The calibration and confirmation approach used in the hydrologic part of the watershed model was used as a starting point to calibrate the water-quality model. The sub-watersheds of Whittenhorse Creek and Davenport Creek were calibrated, and the water-quality model parameters sets for those sub-watersheds were distributed as in the hydrologic part of the model. The model fit for simulated and observed constituent concentrations was subsequently reviewed for hydrologic model confirmation sites: Reedy Creek near Vineland, Bonnet Creek near Vineland, and Reedy Creek near Loughman. Based on review of water-quality model fit at hydrologic model confirmation sites, it was determined that further calibration of the water-quality parameter set was needed to obtain an acceptable fit for observed and simulated constituent concentrations.

The poor water-quality model fit observed at hydrologic model confirmation sites likely can be attributed to the relatively small amount of periodically observed water-quality data, and the distribution of land-use types in the hydrologic model calibration and confirmation sub-watersheds. Water-quality parameter sets calibrated for Whittenhorse Creek and Davenport Creek represent the aggregated affects of the land-use types in those sub-watersheds. The percentage of the agriculture land-use type for the Davenport Creek sub-watershed is about twice that of other sub-watersheds (table 5). Land areas in the RCID contain greater percentages of the urban land-use type, which is not well represented in the Whittenhorse Creek and Davenport Creek sub-watersheds. Therefore, the aggregated affects of land-use types on water-quality reactions may be different for individual sub-watersheds.

Parameters developed from calibration of the model for various water-quality constituents for the Whittenhorse Creek and Davenport Creek

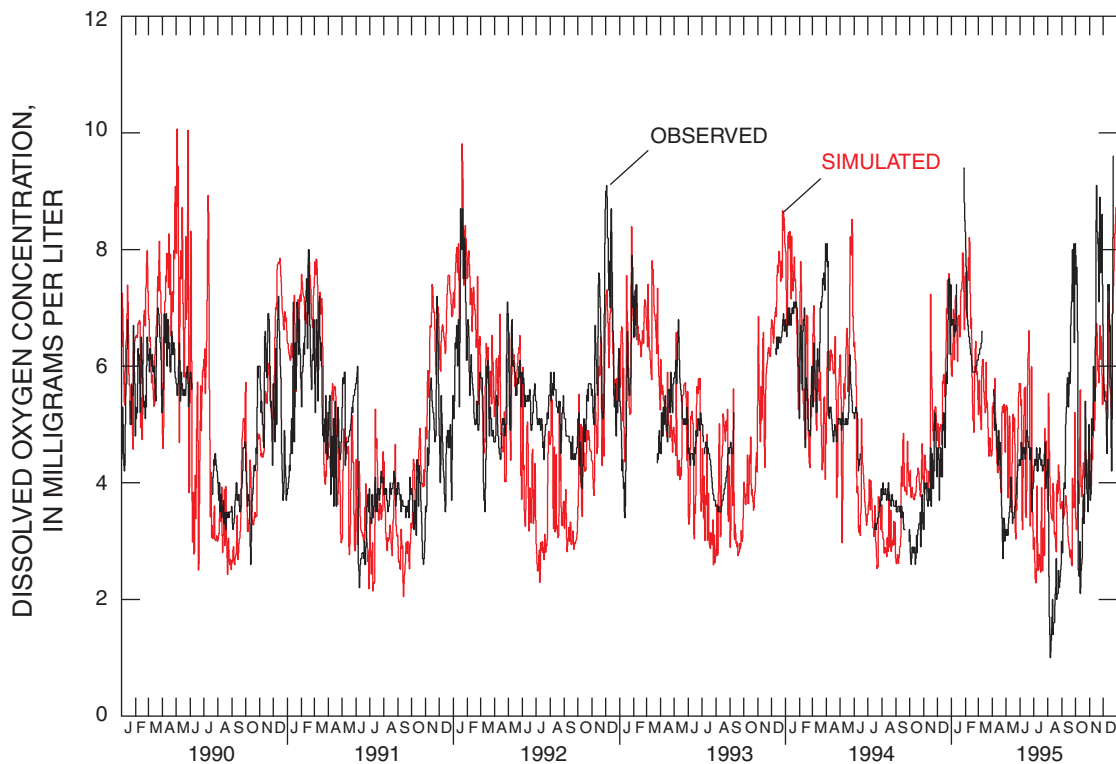
sub-watersheds were applied to other land and water areas in the watershed and subsequently adjusted to obtain the best possible agreement between observed and simulated concentration values at hydrologic model confirmation sites. Parameter values used to simulate build-up and wash-off and interflow and ground-water flow contribution from land areas, and water-quality processes in a stream reach for the Reedy Creek watershed are listed in appendix C.

It was not possible to calibrate constituent values on a daily time step, with the exception of DO (at the Reedy Creek near Vineland site), because the remainder of the available observed data were discrete, not continuous. Discrete water-quality data represent samples collected at a specific time on a given day and, thus, constituent concentrations at a fixed point in time. The value at this fixed point in time may or may not be representative of the average constituent concentration for the entire day. Simulated daily values are mean values of constituent concentration simulated on an hourly basis. Simulated average stream conditions for a day may not be representative of a constituent concentration at any given time during that day. Therefore, it is unlikely that the simulated daily mean and instantaneous observed concentration of a given constituent

will have the same value on any given day. Model fit was considered acceptable if the constituent concentration of simulated values fell within the range of observed values over the modeled period, and simulated values generally indicated similar long-term and monthly trends as those indicated by observed data.

Dissolved oxygen concentration was calibrated by adjusting model parameter values to obtain an acceptable fit between simulated and observed daily mean DO concentration at Reedy Creek near Vineland (fig. 2, map number 29). Simulated DO concentrations for Reedy Creek near Vineland indicated a tendency for the model to slightly overestimate the observed concentrations. The correlation coefficient between simulated and observed daily mean DO concentration values was 0.633. Overall simulated DO values followed the seasonal variation of observed values (fig. 19). Model parameters used to calibrate DO and applied to land-segments and channel reaches in the model are listed in appendix C.

Simulated time series of total phosphorus and phosphate phosphorus concentrations for Whittenhorse Creek generally over simulated the available observed concentrations (figs. 20 and 21, respectively). This over simulation indicated that processes



**Figure 19.** Simulated and observed daily mean dissolved oxygen concentration at Reedy Creek near Vineland, Florida.

in the large wetland area upstream from the site on Whittenhorse Creek may have been removing phosphorus entering the water from overland, subsurface, and upstream sources. Reach parameters in HSPF related to phosphorus uptake and settling were adjusted such that the observed concentrations matched as closely as possible to the simulated concentrations. Further adjustment of model parameters to improve the model fit adversely affected other modeled water-quality constituents. It was not possible to fully represent the wetlands processes without more specific knowledge of water-quality reactions, constituent concentrations, and constituent loadings from specific land-use types within the watershed.

Simulated time series of ammonia nitrogen concentrations for Whittenhorse Creek generally appeared to under simulate the available observed concentrations (fig. 22). The reach parameters in HSPF related to nitrogen uptake and settling were adjusted such that the observed ammonia nitrogen concentrations matched as closely as possible the observed data without adversely affecting other constituents. Simulated nitrate nitrogen concentrations more closely agreed with observed concentrations (fig. 23), and adjustment of parameters decreasing ammonia nitrogen decay could upset the nitrate balance. Undefined processes in the large wetland upstream from the site on Whittenhorse Creek likely are affecting chemical and biochemical reactions, which affect constituent concentrations in water samples at the gaging site.

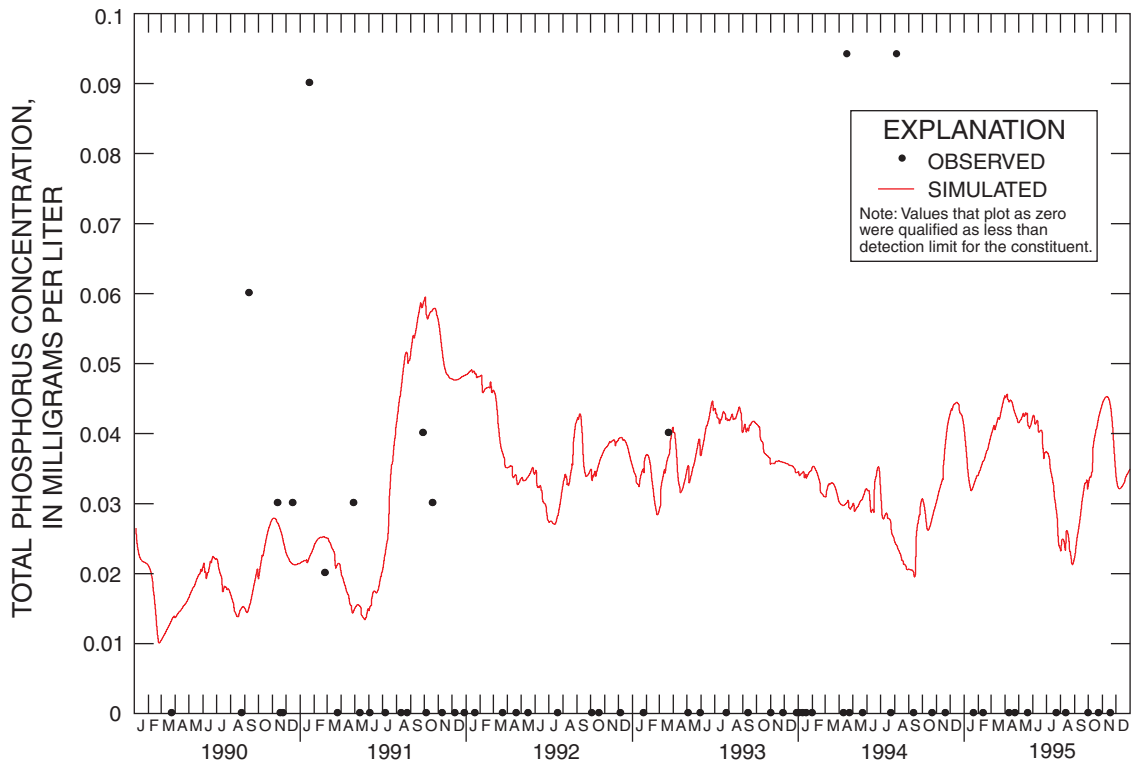
Simulated time series of total phosphorus and phosphate phosphorus concentrations for Davenport Creek generally agreed well with the available observed concentrations (figs. 24 and 25, respectively). Based on the similarity to results for water-quality calibrations for the Potomac River (Camacho and Blasenstein, 1992) and for Walnut Creek, Iowa (Donigian and others, 1993), the calibration of total phosphorus and phosphate phosphorus concentrations for Davenport Creek is considered acceptable.

Simulated time series of ammonia nitrogen concentrations for Davenport Creek generally agreed with the available observed concentrations (fig. 26). The amount of observed periodic ammonia nitrogen concentration data is small for Davenport Creek and the effect of some over-simulated concentrations at times of low observed concentrations may cause some concern regarding the quality of the ammonia nitrogen simulation. However, simulated time series of nitrate

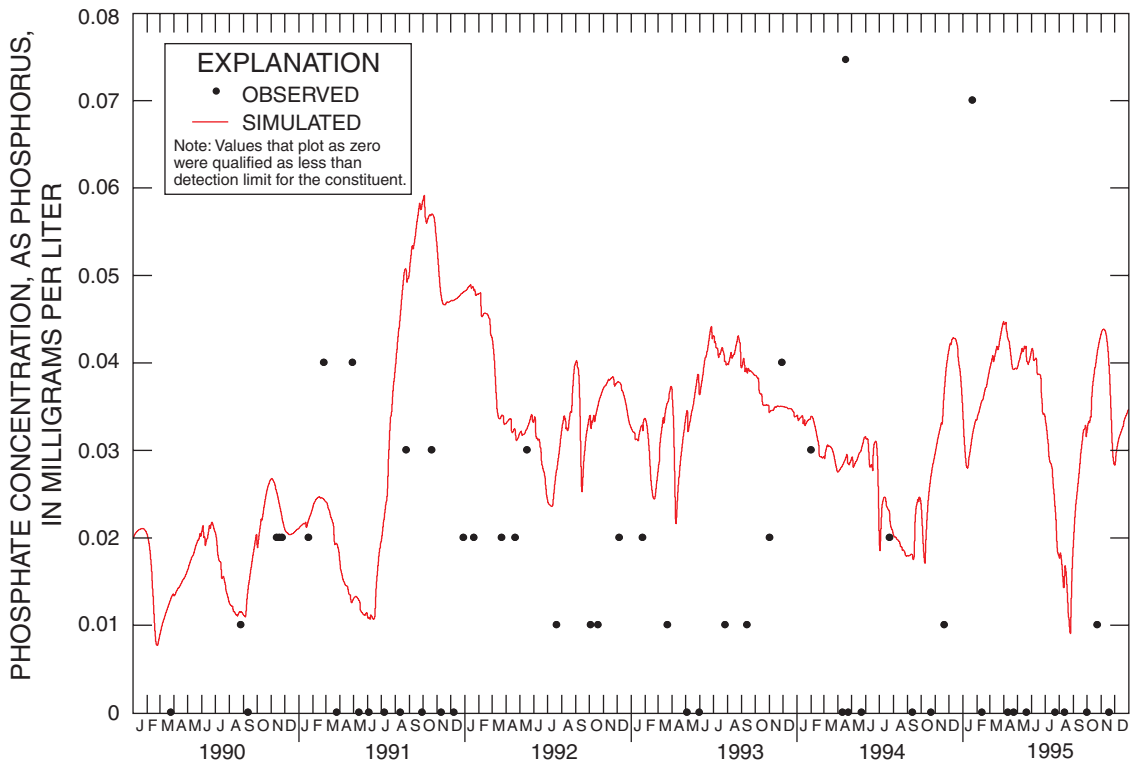
nitrogen concentrations agreed well with the available observed concentrations (fig. 27). Adjustment of model parameters to reduce the possibility of over simulating ammonia nitrogen concentrations could result in reduced quality of the nitrate nitrogen simulation. Therefore, the ammonia nitrogen and nitrate nitrogen simulations are considered acceptable for Davenport Creek.

Simulated time series of total phosphorus concentrations for Reedy Creek near Vineland greatly under simulated observed concentrations from 1990-91, and slightly under simulated the observed concentrations from 1992-95 (fig. 28). Simulated time series of phosphate phosphorus concentrations for Reedy Creek near Vineland greatly under simulated observed concentrations from 1990-91, and slightly under simulated the observed concentrations from 1992-95 (fig. 29).

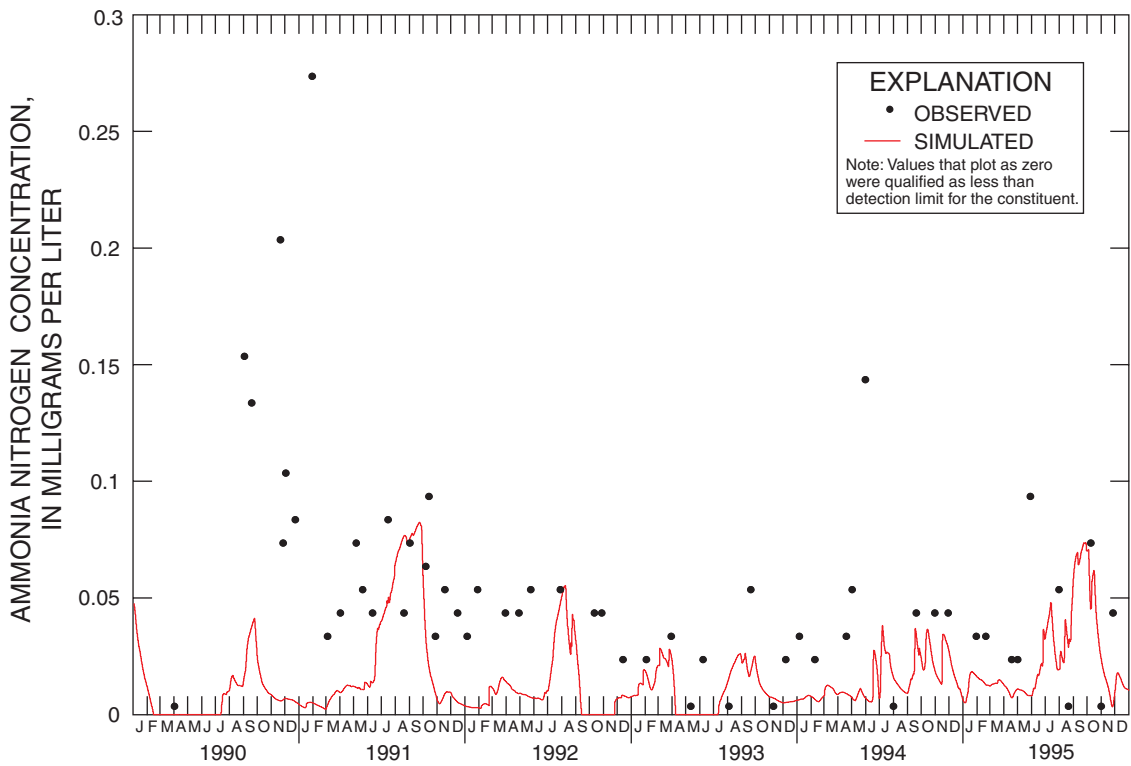
Simulated time series of ammonia nitrogen concentrations for Reedy Creek near Vineland agreed well with the observed concentrations (fig. 30). Conversely, the simulated time series of observed nitrate nitrogen concentrations greatly under simulated the observed nitrate nitrogen concentrations from 1990-91, and slightly under simulated the observed nitrate nitrogen concentrations from 1992-95 (fig. 31). Simulated concentrations of total phosphorus, phosphate, and nitrate nitrogen substantially less than observed concentrations during 1990-91 may be the result of increases in constituent concentrations in surface runoff, interflow, and ground water in the form of treated wastewater disposed into wetland areas draining to the stream channel upstream from the Reedy Creek near Vineland gaging station. Prior to 1992, the RCID discharged treated wastewater to wetland areas adjacent to Reedy Creek north of the gaging station at Reedy Creek near Vineland (fig. 2, map number 29). Reclaimed wastewater was pumped to wetland areas adjacent to Reedy Creek and aerated to elevate DO concentrations before the water was allowed to drain into Reedy Creek through surface runoff and shallow ground-water infiltration (T. McKim, Reedy Creek Improvement District, oral comm., 2000). Modeling the effects of disposing treated wastewater into wetland areas was not possible due to a lack of observed data relating to disposal rates, constituent concentrations in the treated wastewater, and specific information related to disposal location and methods.



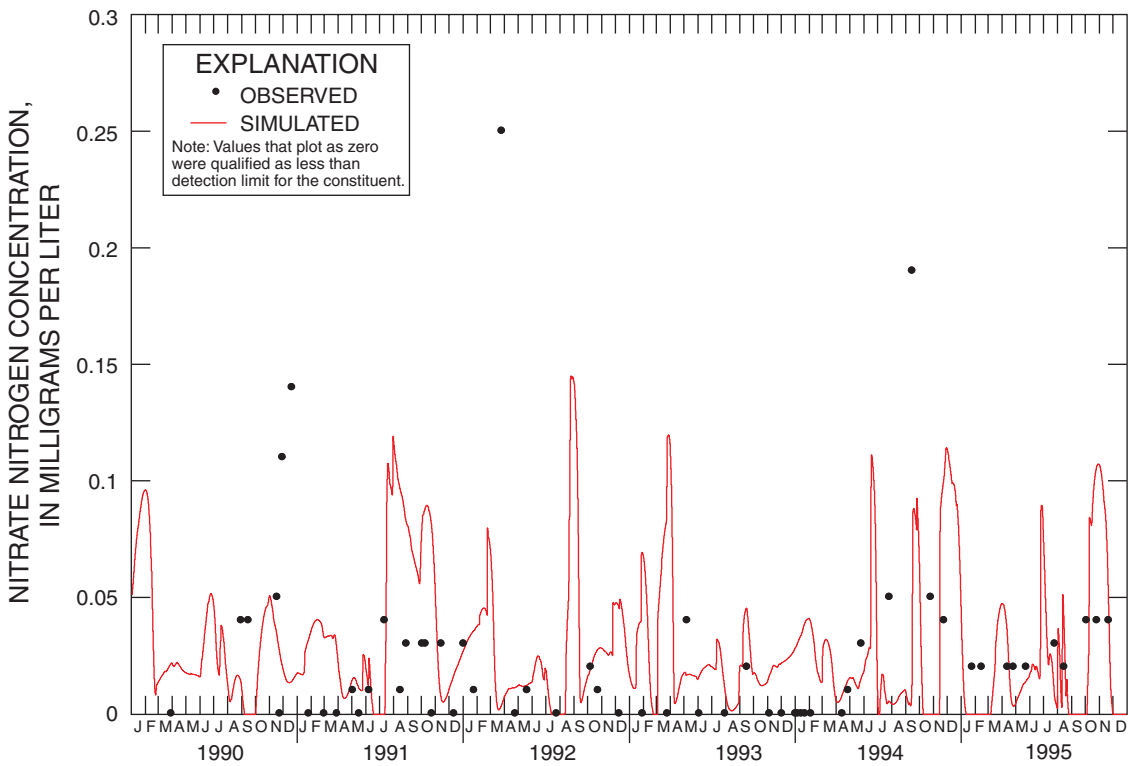
**Figure 20.** Simulated daily mean and observed periodic total phosphorus concentration values for Whittenhorse Creek near Vineland, Florida.



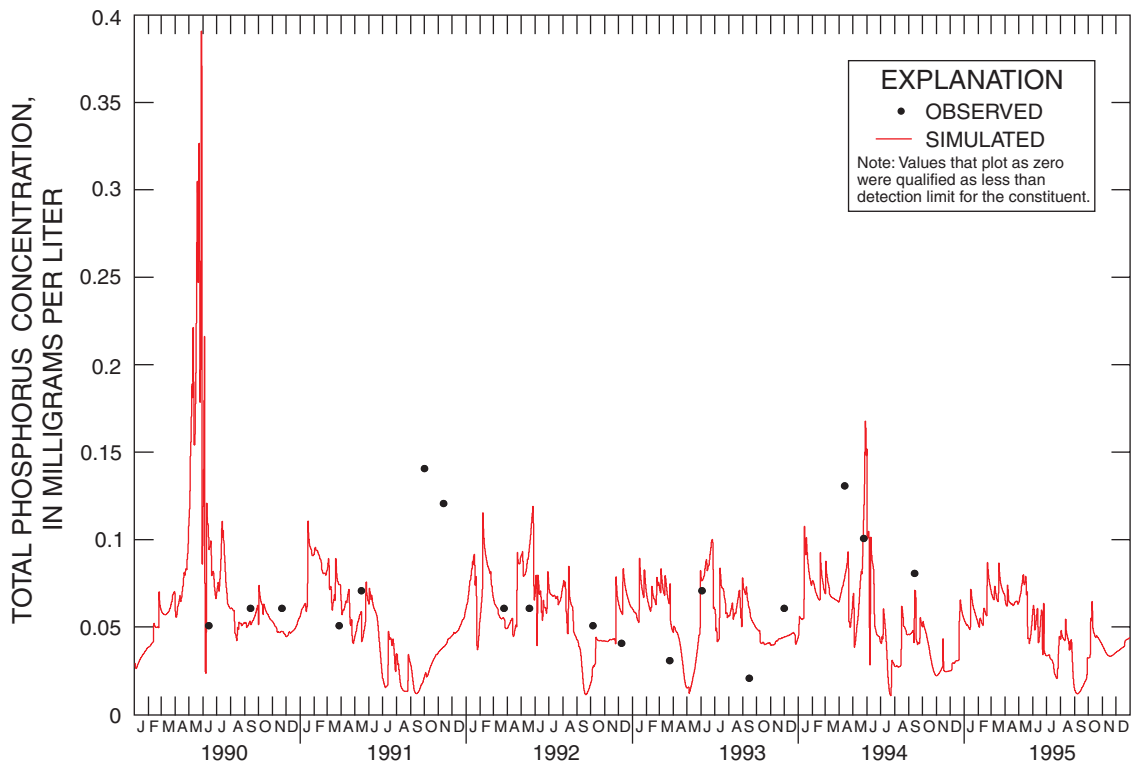
**Figure 21.** Simulated daily mean and observed periodic phosphate concentration values for Whittenhorse Creek near Vineland, Florida.



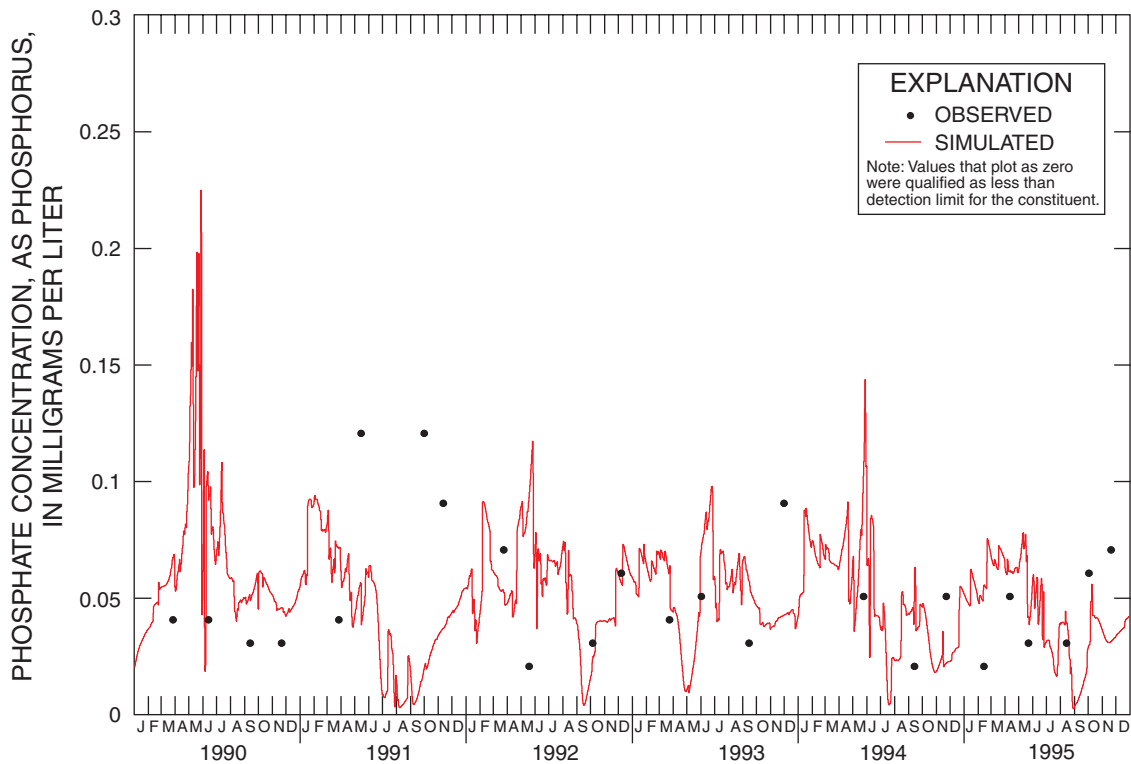
**Figure 22.** Simulated daily mean and observed periodic ammonia nitrogen concentration values for Whittenhorse Creek near Vineland, Florida.



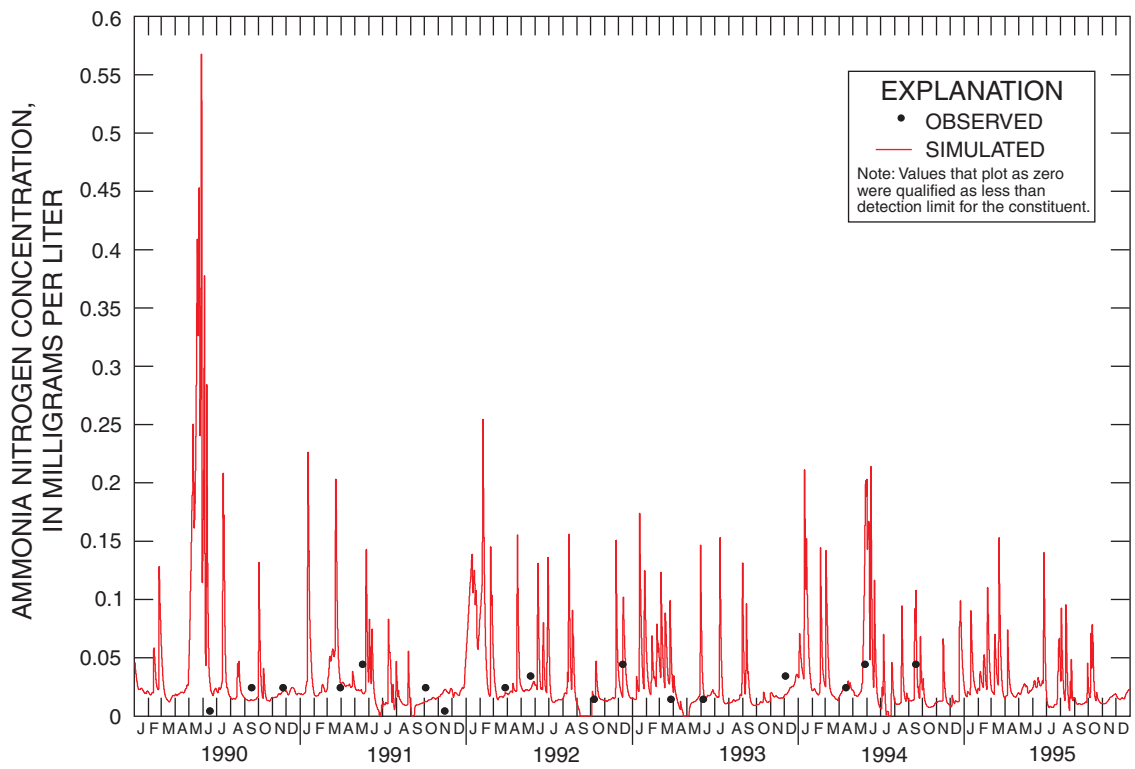
**Figure 23.** Simulated daily mean and observed periodic nitrate nitrogen concentration values for Whittenhorse Creek near Vineland, Florida.



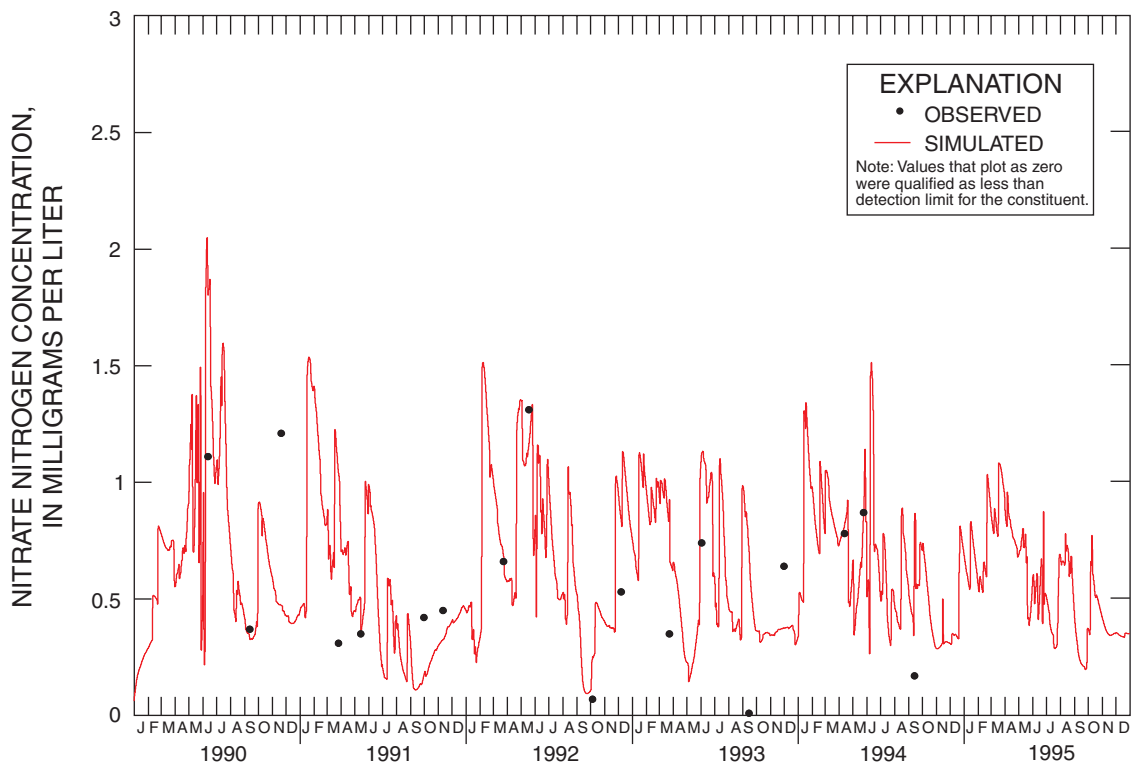
**Figure 24.** Simulated daily mean and observed periodic total phosphorus concentration values for Davenport Creek near Loughman, Florida.



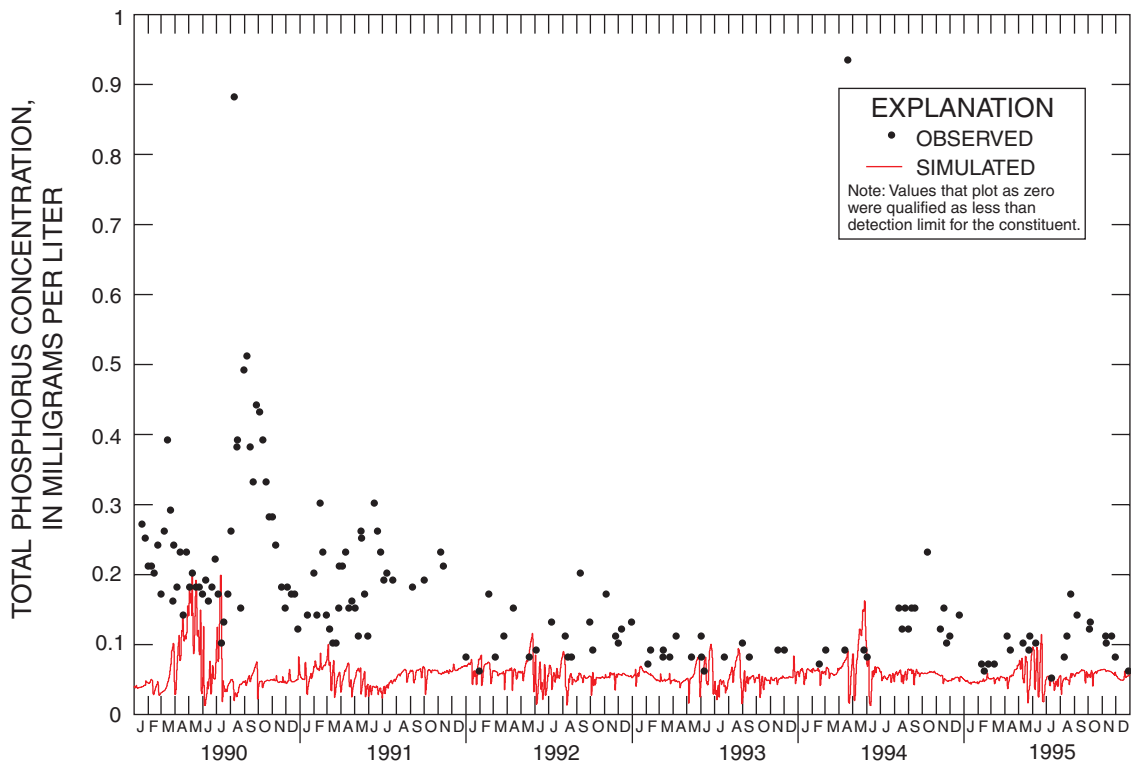
**Figure 25.** Simulated daily mean and observed periodic phosphate concentration values for Davenport Creek near Loughman, Florida.



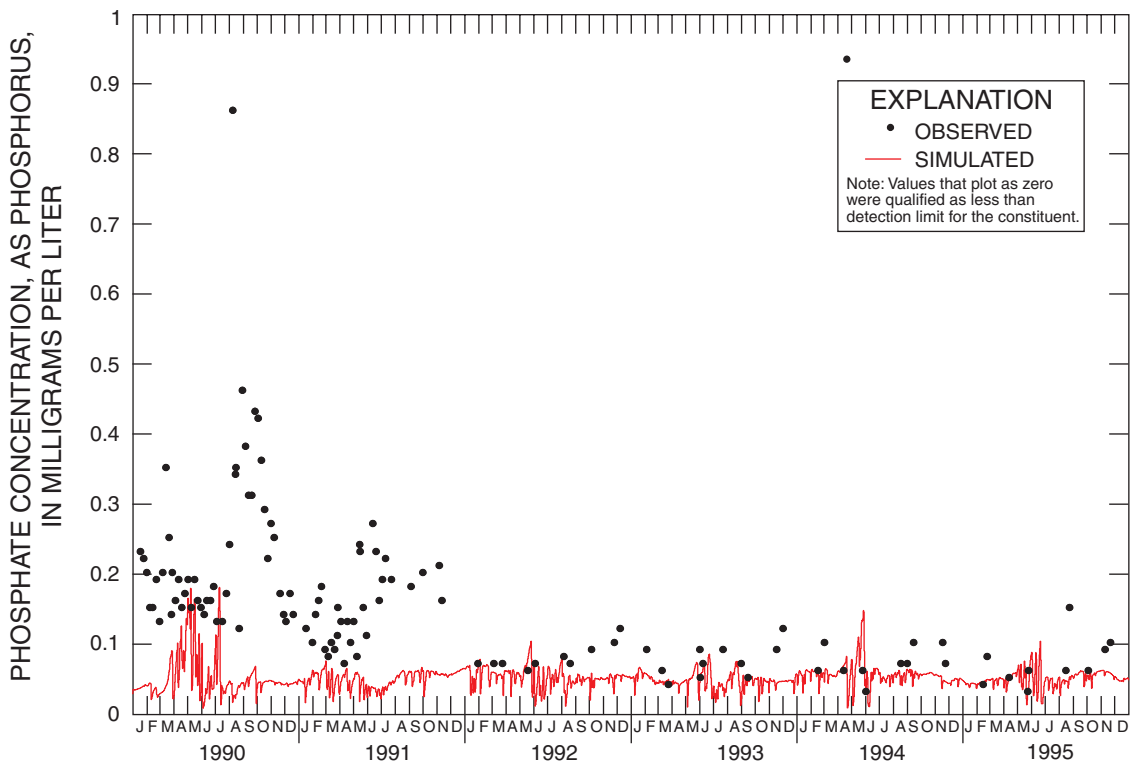
**Figure 26.** Simulated daily mean and observed periodic ammonia nitrogen concentration values for Davenport Creek near Loughman, Florida.



**Figure 27.** Simulated daily mean and observed periodic nitrate nitrogen concentration values for Davenport Creek near Loughman, Florida.

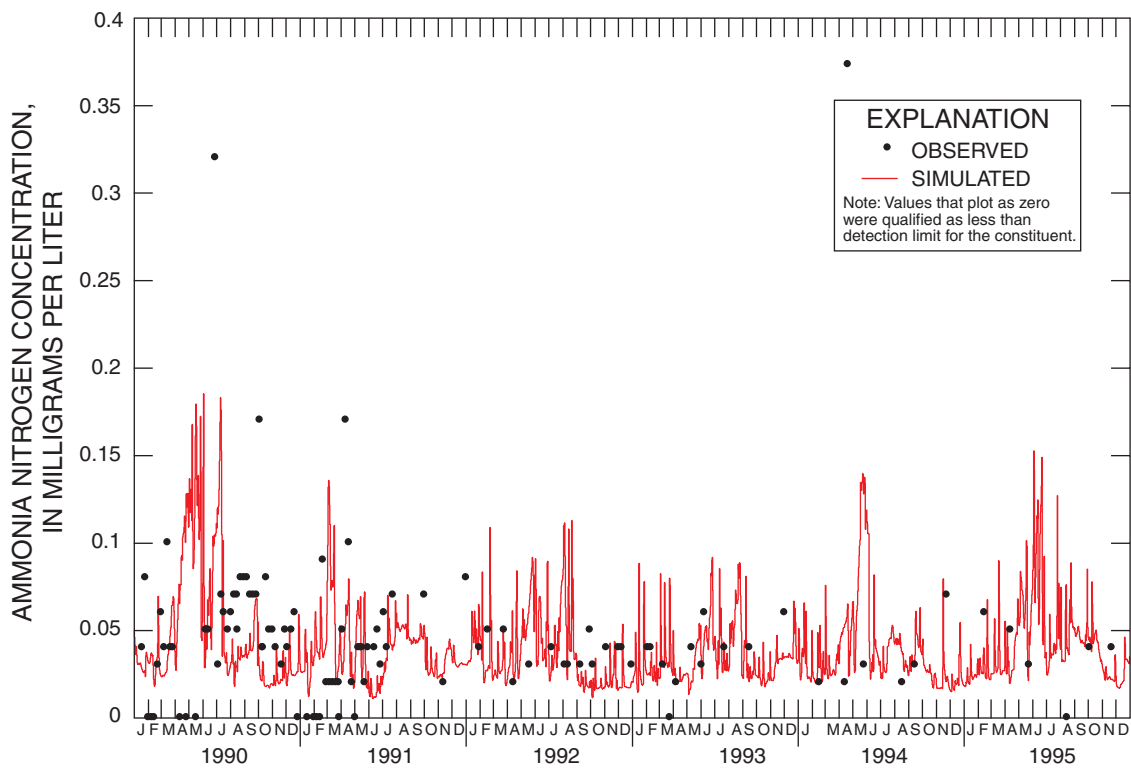


**Figure 28.** Simulated daily mean and observed periodic total phosphorus concentration values for Reedy Creek near Vineland, Florida.

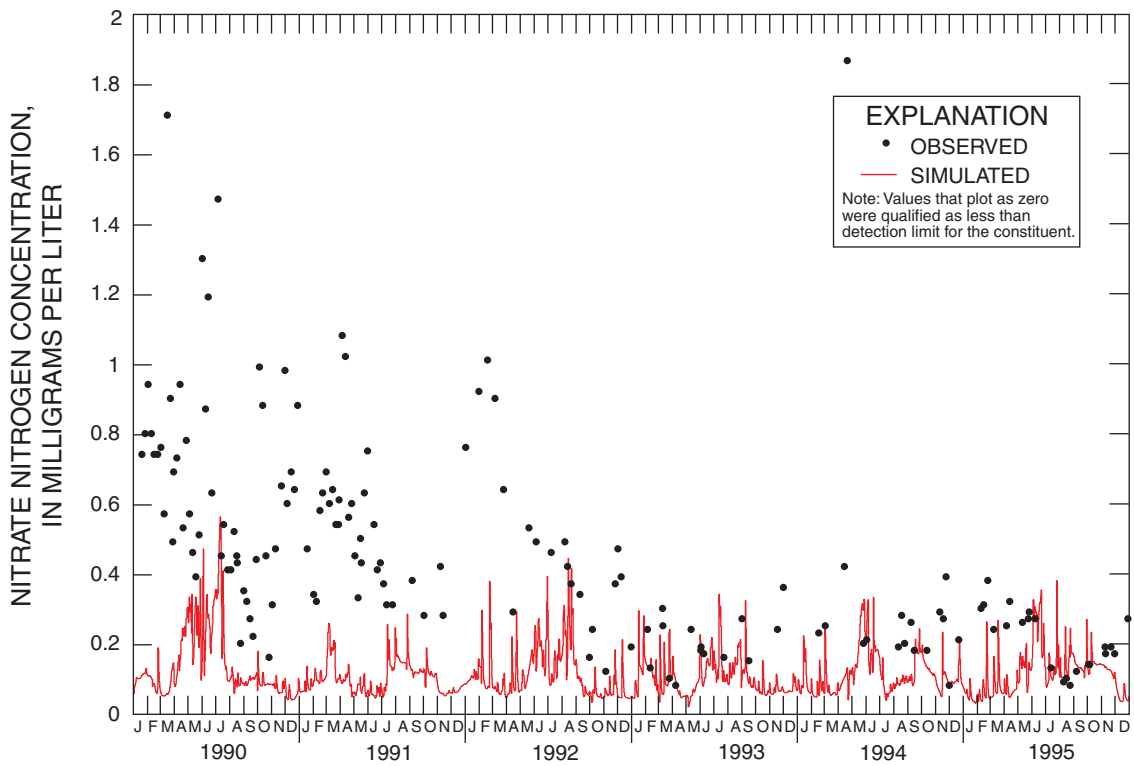


**Figure 29.** Simulated daily mean and observed periodic phosphate concentration values for Reedy Creek near Vineland, Florida.

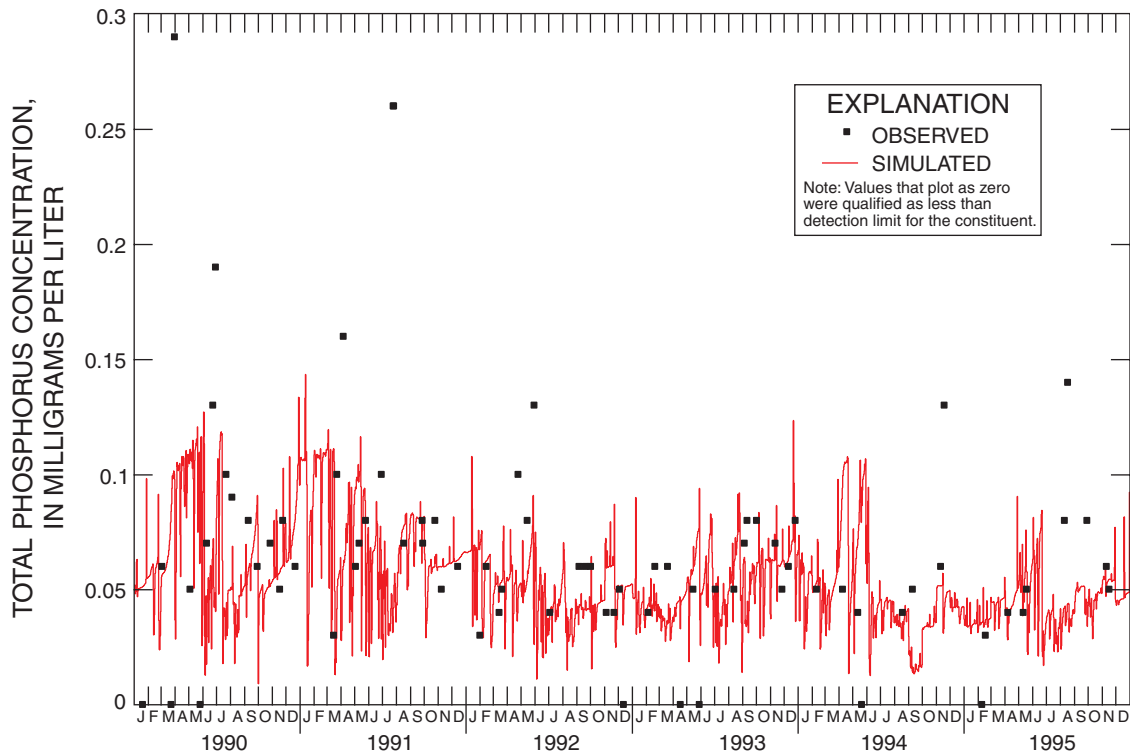




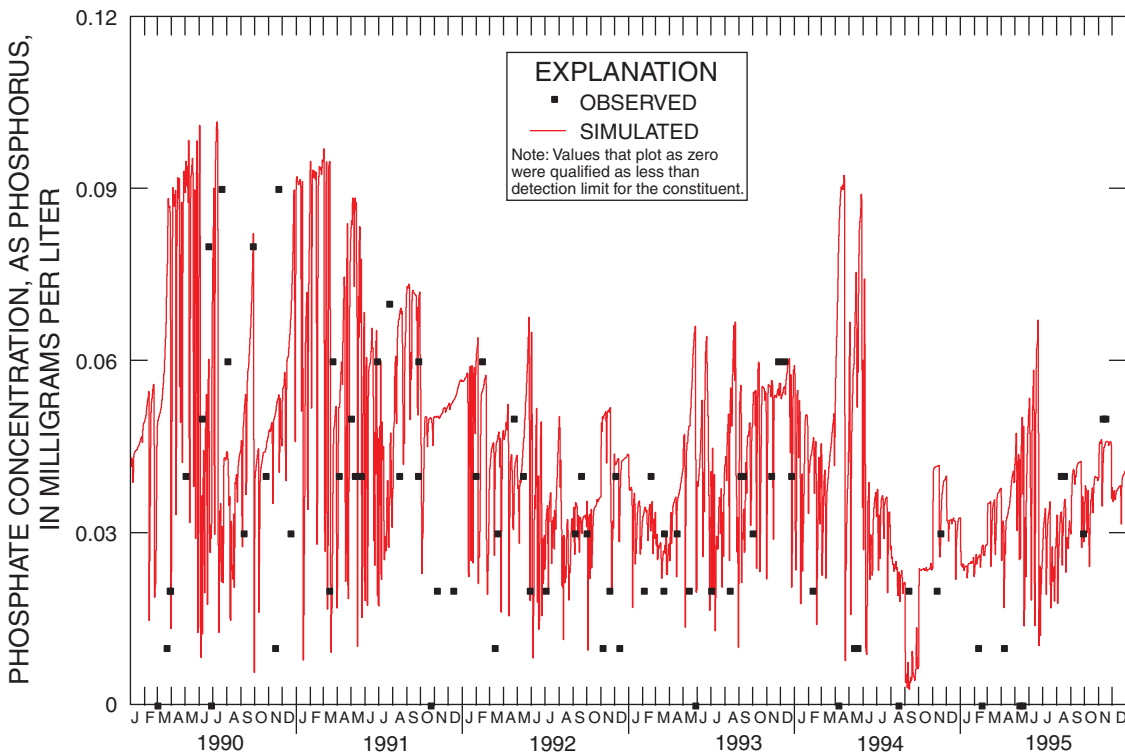
**Figure 30.** Simulated daily mean and observed periodic ammonia nitrogen concentration values for Reedy Creek near Vineland, Florida.



**Figure 31.** Simulated daily mean and observed periodic nitrate nitrogen concentration values for Reedy Creek near Vineland, Florida.



**Figure 32.** Simulated daily mean and observed periodic total phosphorus concentration values for Bonnet Creek near Vineland, Florida.



**Figure 33.** Simulated daily mean and observed periodic phosphate concentration values for Bonnet Creek near Vineland, Florida.

Simulated time series of total phosphorus for Bonnet Creek near Vineland agreed well with observed concentrations, and simulated phosphate phosphorus concentrations slightly over simulated observed concentrations (figs. 32 and 33, respectively). This result is similar to water-quality calibrations for the Potomac River (Camacho and Blasenstein, 1992) and for Walnut Creek, Iowa (Donigian and others, 1993).

Simulated time series of ammonia nitrogen concentrations for Bonnet Creek near Vineland agreed well with the observed concentrations, and simulated time series of nitrate nitrogen concentrations slightly over simulated the observed concentrations (figs. 34 and 35, respectively). Undefined water-quality processes in urban land-use areas upstream from the Bonnet Creek near Vineland gaging station may be affecting chemical and biochemical reactions, which affect constituent concentrations in water samples at the gaging site. It was not possible to fully represent the urban land-use types without more specific knowledge of water-quality reactions, constituent concentrations, and constituent loadings from specific land-use types within the watershed. The difficulties in representing the Bonnet Creek drainage between the Cypress Creek and Bonnet Creek gaging stations were previously discussed in the hydrologic model confirmation section of this report. Additional evaluation of the hydrologic and water-quality processes in this part of the watershed is beyond the scope of the current study.

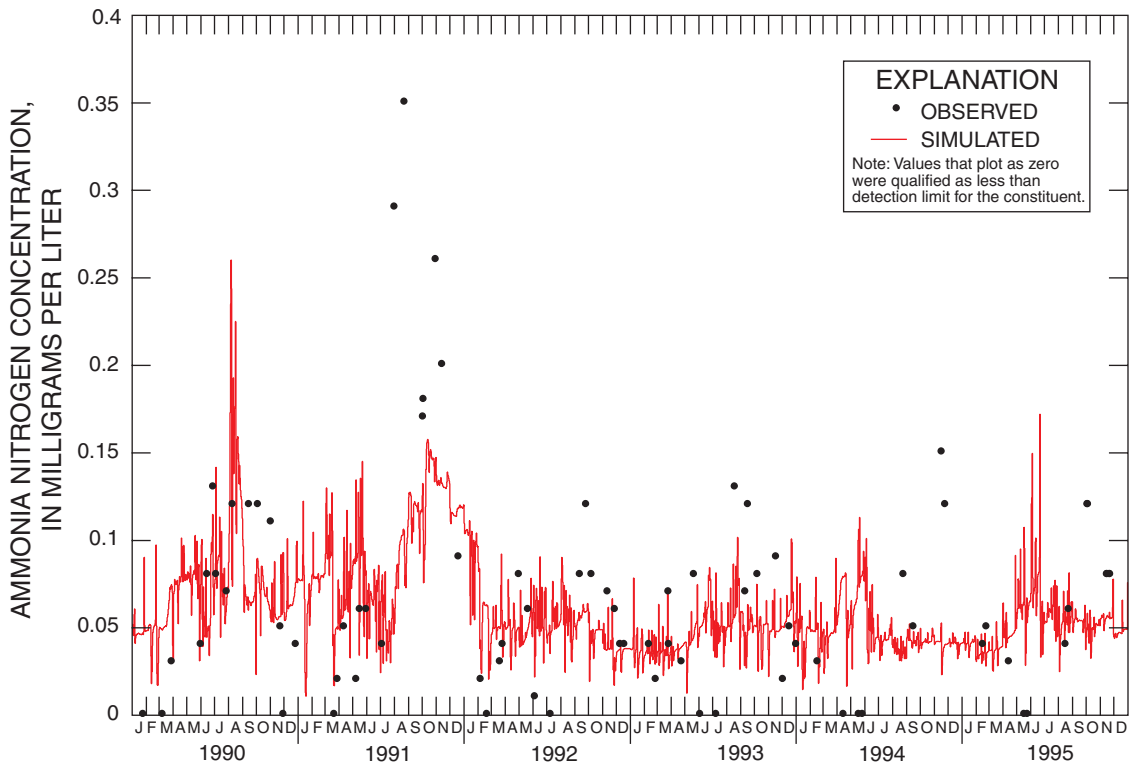
Simulated time series of total phosphorus and phosphate phosphorus concentrations for Reedy Creek near Loughman slightly under simulated the available observed concentrations (figs. 36 and 37, respectively). Simulation of total phosphorus and phosphate phosphorus concentrations that were significantly less than observed concentrations during 1990-91 may have resulted from increases in constituent concentrations in surface runoff, interflow, and ground water from the discharge of treated wastewater into wetland areas draining to the stream channel upstream from the Reedy Creek near Vineland gaging station, as previously discussed.

Simulated time series of ammonia nitrogen concentrations for Reedy Creek near Loughman agreed well with observed concentrations (fig. 38). The general agreement between simulated, continuous values and observed, discrete values was similar to water-quality calibrations for the Potomac River (Camacho and Blasenstein, 1992) and for Walnut Creek, Iowa (Donigian and others, 1993). Simulated time series of

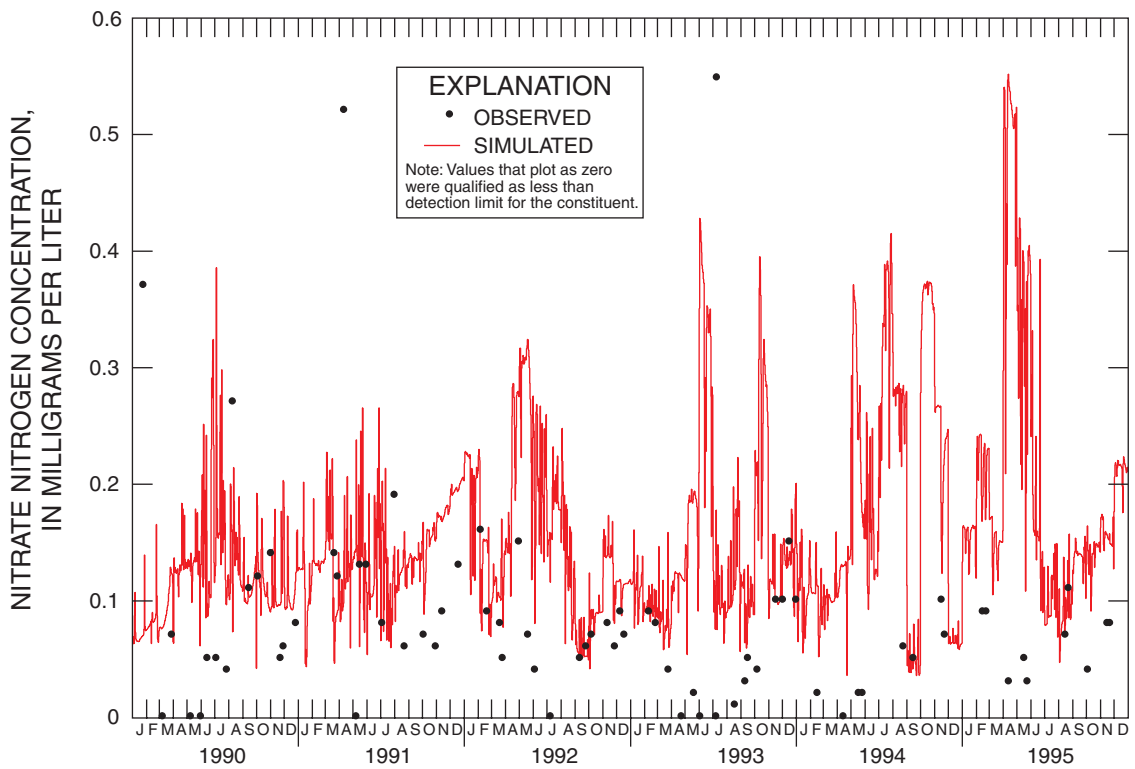
nitrate nitrogen concentrations slightly over simulated observed concentrations (fig. 39).

The unknown amount and quality of water diverted from the Reedy Creek watershed at the Bonnet Creek near Kissimmee gaging station (fig. 2, map number 23) and undefined processes in the large wetland area upstream of the Reedy Creek at S-40 near Loughman gaging station (fig. 2, map number 32) may be affecting chemical and biochemical reactions, which affect constituent concentrations in water samples at the Reedy Creek near Loughman gaging station (fig. 2, map number 33). German (1989) reported that most of the processes affecting water quality in the Reedy Creek watershed south of Highway 192 probably occur in the wetland areas (fig. 6). Total nitrogen and phosphorus loads were reduced between Reedy Creek near Vineland and Reedy Creek at S-40 near Loughman by about 33 percent by water-quality reactions in the lower Reedy Creek wetland area (German, 1989). Wetland processes are not fully represented within the model because of insufficient data on water-quality reactions, constituent concentrations, and constituent loadings in the wetland areas of the Reedy Creek watershed. The simulation results at Reedy Creek near Loughman likely could be improved by further data collection and in-depth analysis of wetland processes, and by quantification of the volume and quality of water diverted from the watershed downstream from the Bonnet Creek near Vineland gaging site.

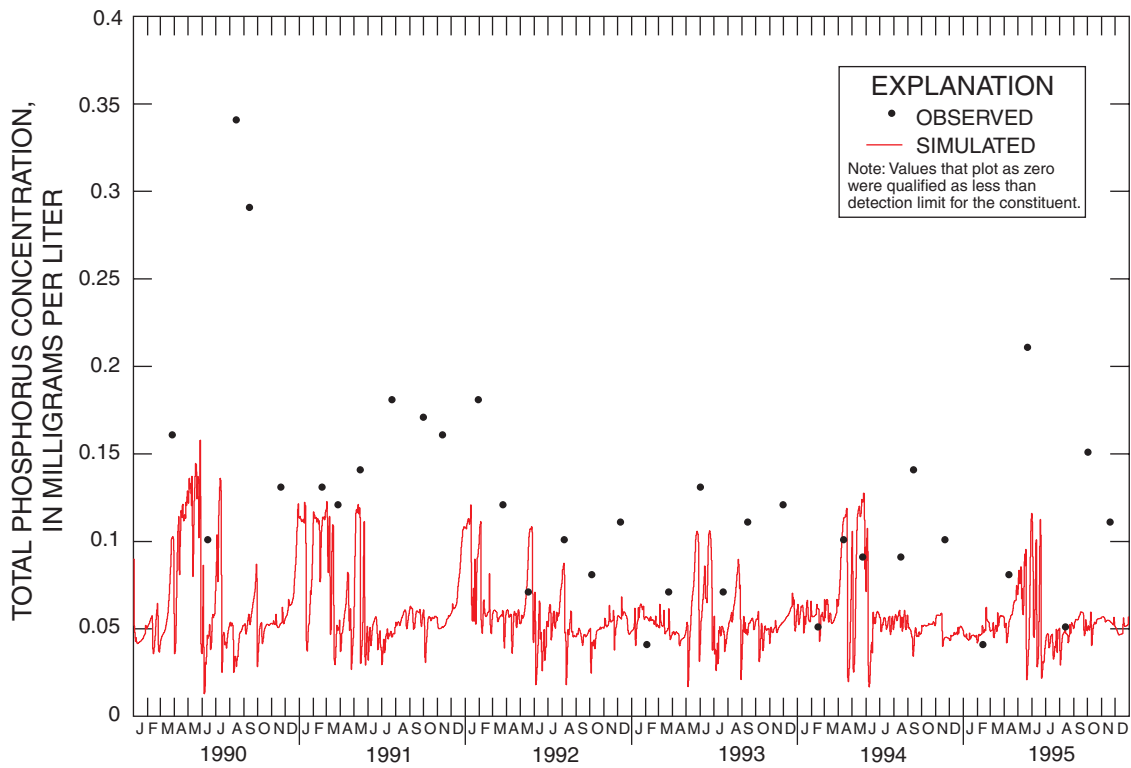
The water-quality calibration was further evaluated by validation of model-parameter values specified for the interflow and ground-water zone concentrations used to obtain a suitable fit between observed and simulated constituent concentrations. Dissolved phosphorus concentrations in ground water from the surficial aquifer system in both Orange County and the Reedy Creek watershed ranged from less than the reporting limit (0.02 milligrams per liter (mg/L)) to 0.07 mg/L, and dissolved orthophosphorus concentrations ranged from less than the reporting limit (0.01 mg/L) to 0.06 mg/L (J. Adamski, U.S. Geological Survey, oral comm., 1999). These values are in reasonable agreement with the concentrations specified in HSPF for the interflow and ground-water zone concentrations (appendix C), and generally support the model calibration for total phosphorus.



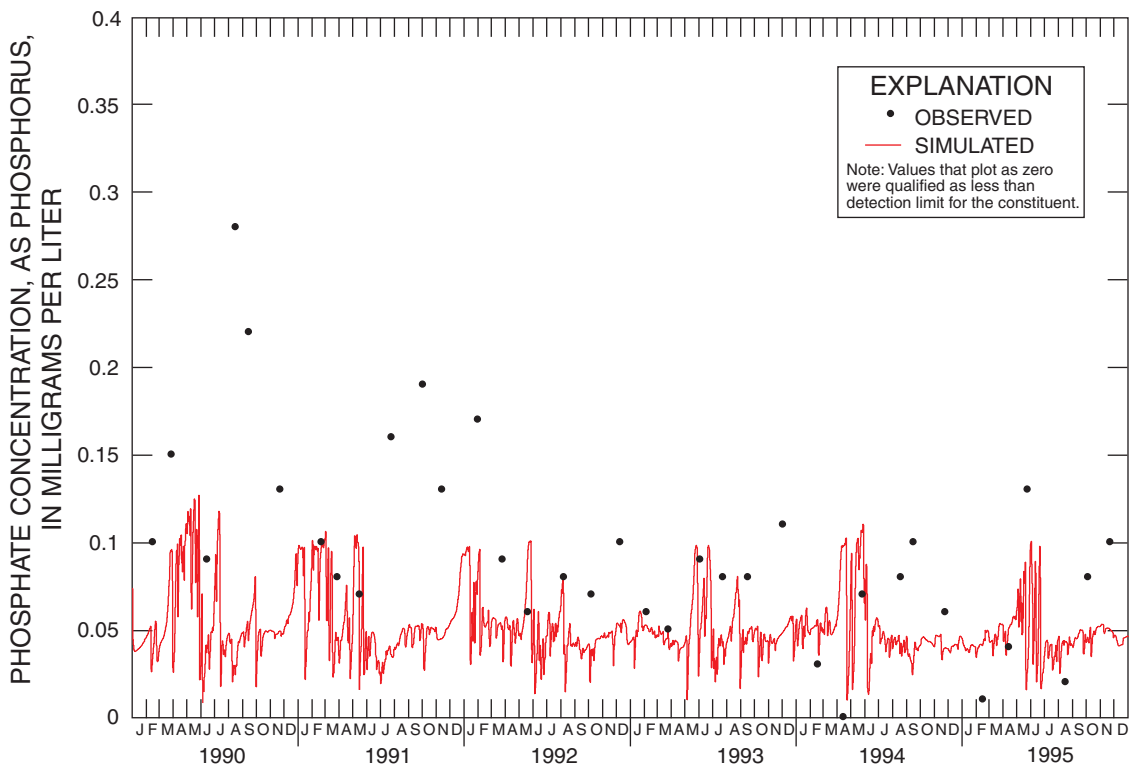
**Figure 34.** Simulated daily mean and observed periodic ammonia nitrogen concentration values for Bonnet Creek near Vineland, Florida.



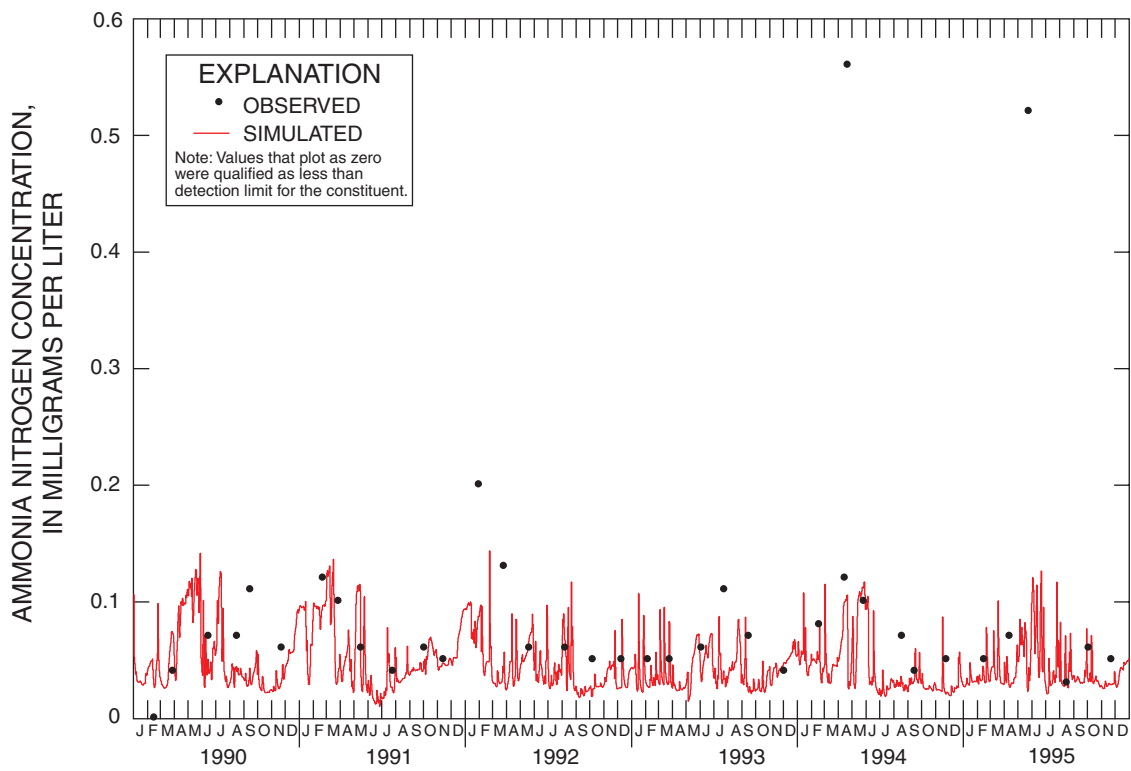
**Figure 35.** Simulated daily mean and observed periodic nitrate nitrogen concentration values for Bonnet Creek near Vineland, Florida.



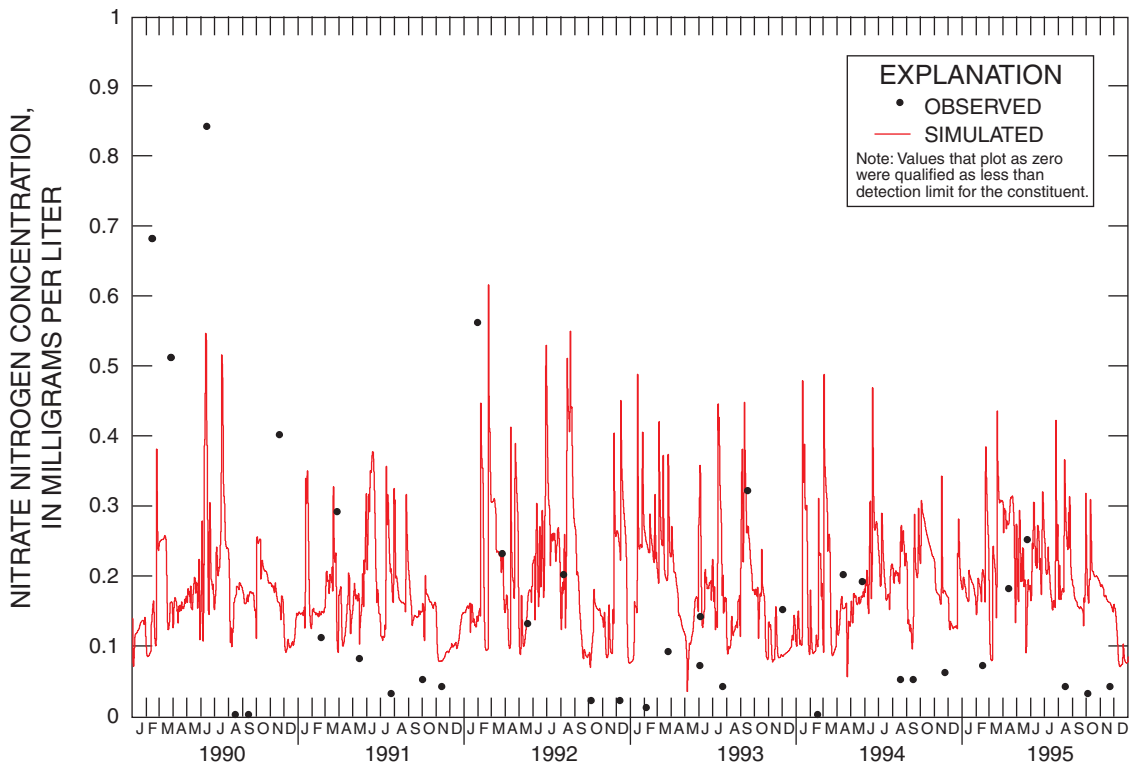
**Figure 36.** Simulated daily mean and observed periodic total phosphorus concentration values for Reedy Creek near Loughman, Florida.



**Figure 37.** Simulated daily mean and observed periodic phosphate concentration values for Reedy Creek near Loughman, Florida.



**Figure 38.** Simulated daily mean and observed periodic ammonia nitrogen concentration values for Reedy Creek near Loughman, Florida.



**Figure 39.** Simulated daily mean and observed periodic nitrate nitrogen concentration values for Reedy Creek near Loughman, Florida.

The samples from the surficial aquifer system also were analyzed for ammonia nitrogen and nitrate nitrogen. Ammonia nitrogen concentrations ranged from less than the reporting limit (0.01 mg/L) to 0.7 mg/L in Orange County, and less than the reporting limit to 0.44 mg/L in the Reedy Creek watershed. For these sites, nitrite plus nitrate nitrogen (mainly nitrate nitrogen) concentrations ranged from less than the reporting limit (0.02 mg/L) to 6.3 mg/L. Concentrations of nitrite plus nitrate nitrogen greater than the reporting limit were measured in the Reedy Creek watershed. Comparison of the observed instream and ground-water concentrations of ammonia nitrogen and nitrate nitrogen and the values for interflow and ground-water zone concentrations specified in HSPF, supports the calibration for ammonia nitrogen and nitrate nitrogen concentrations in the Reedy Creek watershed.

## **FUTURE LAND-USE SCENARIO SIMULATION**

Simulation of a future land-use scenario for the Reedy Creek watershed was based on the hydrologic and water-quality simulations previously discussed in this report, projected future land use within the RCID, and existing land use for areas external to the RCID but within the Reedy Creek watershed. The time series input for the 6-year model simulation period remained unchanged, and all other input to the model (that is, parameters) remained the same except for land use. The user control input file for this scenario is given in appendix E. Errors associated with the calibration and confirmation processes of the existing land use also are present in the future land-use scenario. Therefore, relative changes observed between existing and future land use can be considered unbiased by errors associated with the calibration and confirmation process.

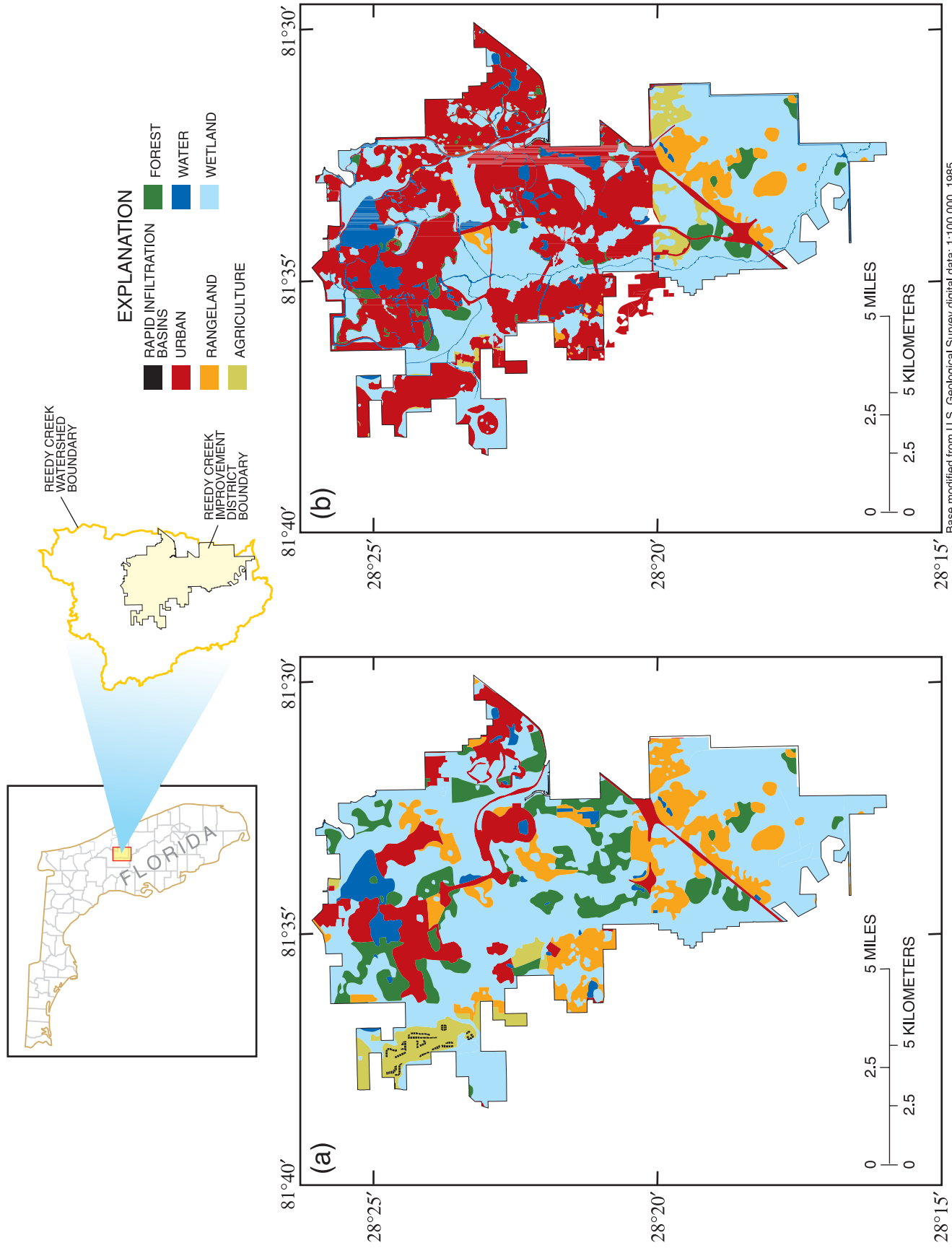
### **Scenario Development**

Runoff and water quality for a future land-use scenario were simulated based only on projected land use within the RCID, assuming that characteristics of land-use types remained unchanged and no additional best management practices (BMPs) were implemented. Projected future land-use data for areas outside the RCID generally are not readily available. Therefore, in the future land-use scenario only planned land development in the RCID could be

evaluated as a means to illustrate the effects of land development on water quality in Reedy Creek. If a true representation of possible future water quality in the Reedy Creek watershed is desired, estimates of future land development in the watershed outside of the RCID should be included. Future land-use data, including spatial distribution of land cover in the RCID, which represents 25.5 percent of the total land area of the Reedy Creek watershed, were obtained, based on the RCID City of Lake Buena Vista and City of Bay Lake Comprehensive Plan 2008 (Reedy Creek Improvement District, 1999).

Land-cover attributes from the RCID future land-use spatial data were correlated with the USGS land-use and land-cover classification system for use with remote sensor data (U.S. Geological Survey, 1990). Future land-use data provided by the RCID were adjusted, based on land-cover type, to conform to the six land-use types that characterize the Reedy Creek watershed: agriculture, rangeland, forest, wetlands, RIBS, and urban area (fig. 40). The RCID classification of future land-use types did not closely match the six land-use types used in the existing land-use watershed simulation. Difficulties in reclassification of the RCID land-use types to conform to the six existing land-use types may lead to improper classification of some land areas in the future land-use scenario. Land areas improperly classified were most likely classified as other land-use types with similar characteristics and have relatively little influence on the overall outcome of the future land-use simulation. Existing land-use data (fig. 6), representing the distribution of land use in the Reedy Creek watershed as it existed at the start of the modeling period (January 1990) for areas external to the RCID, were combined with the adjusted RCID future land-use data to produce a future land-use scenario spatial data set for the entire Reedy Creek watershed. Land-use types represented in the existing land use, that were changed to other land-use types in the future land-use scenario, accounted for approximately 20 percent of the total watershed area.

Percentages of modeled pervious and impervious land area for indicated land-use types of modeled sub-watersheds of the Reedy Creek watershed are listed in table 9. Percentages listed for the Bonnet Creek near Vineland and Reedy Creek near Loughman watersheds do not include land areas in the Cypress Creek sub-watershed because the Cypress Creek drainage was input as a point source and not modeled explicitly.



**Figure 40.** Land use in the Reedy Creek Improvement District, Florida, (a) existing 1990 and (b) future 2008.



**Table 9.** Modeled percentages of pervious and impervious land areas based on geographic coverages from existing (1990) and future (2008) land use in the Reedy Creek Improvement District

[When the sum of percentages is less than 100 percent, the remaining area is covered by open water; RIBS, rapid infiltration basins]

	Pervious land area (percent)						Impervious land area (percent)
	Agriculture	Forest	Range-land	Urban	Wetland	RIBS	
Whittenhorse Creek existing land use	27.5	2.4	19.0	1.3	43.6	0.4	0.6
Whittenhorse Creek future land use	25.7	2.2	17.9	2.1	41.1	.0	5.5
Davenport Creek existing land use	45.5	2.8	16.0	3.6	26.7	.0	1.5
Davenport Creek future land use	45.5	2.8	16.0	3.6	26.7	.0	1.5
Reedy Creek near Vineland existing land use	20.3	5.5	21.5	5.3	34.4	.2	3.6
Reedy Creek near Vineland future land use	18.8	2.3	18.0	5.0	29.6	.0	16.3
Bonnet Creek near Vineland <sup>1</sup> existing land use	2.2	10.8	14.2	9.8	40.1	.0	13.2
Bonnet Creek near Vineland <sup>1</sup> future land use	2.1	4.3	11.8	7.5	27.1	.0	35.6
Reedy Creek near Loughman <sup>1</sup> existing land use	19.9	6.0	20.0	5.4	37.3	.1	4.1
Reedy Creek near Loughman <sup>1</sup> future land use	19.9	2.9	16.6	5.1	32.6	.0	15.0

<sup>1</sup>Does not include land areas in the Cypress Creek sub-watershed.

Overall, the percentage of modeled forest and urban-impervious land-use types changed the most between existing and future land use: for areas upstream from the Reedy Creek near Loughman gaging station, there was a 50 percent reduction in the amount of forest area, and a 300 percent increase in the impervious land areas indicated (table 9). Drainage areas upstream from the Bonnet Creek near Vineland gaging station had the greatest differences in modeled pervious and impervious land areas between existing and future land use.

No change in land area for the Davenport Creek sub-watershed is indicated because all of the land areas in this sub-watershed are outside of the RCID; land use distribution is the same for the existing and future land use. As indicated in table 9, RIBS are a small percentage of the existing land use and are not represented as a land-use type in the future land-use scenario. Based on the RCID future land-use data, areas indicated as RIBS in the existing land use were changed to other land-use types in the future land-use scenario (fig. 40). Wastewater disposed to the RIBS land-use type in the RCID likely will be diverted for use as irrigation water, and the net effect on water quality in the watershed should be similar to that presented in this report. The greatest change in the future land-use scenario for all sub-watersheds was an increase in the impervious land use.

## Hydrology

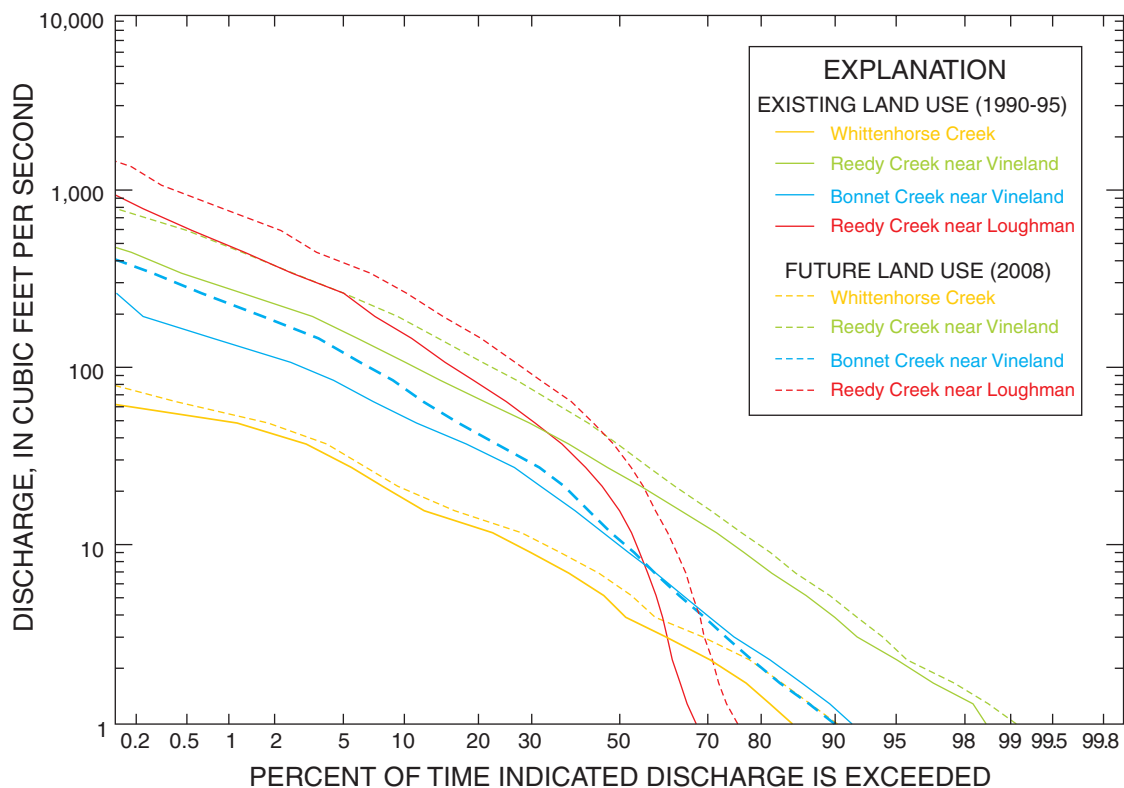
Annual mean discharge summaries at four sites indicated increased runoff in the future land-use scenario (table 10). Davenport Creek was not included in the comparison because no changes in land areas are projected between existing and future land use, and therefore, discharge would not change. Annual mean discharge increased at three of the four sites by about 30 percent or greater. These three sites also had the greatest change in impervious area between existing and future land use (table 9). Increases in the total runoff in each sub-watershed and in the entire Reedy Creek watershed, as simulated in the future land-use scenario, can likely be attributed to the overall increase in impervious areas.

Duration curves of daily mean discharge for existing and future land use also indicated an increase in total runoff from the Reedy Creek watershed for the future land-use scenario (fig. 41). An increase in overland flow and decrease in infiltration attributed to increases in impervious areas are indicated by increases in discharge duration. Three of the four duration curves (fig. 41) indicate an increase in discharges for all exceedance percentages in the future land-use scenario. This likely is the result of storage characteristics of the sub-watersheds. Storage of stormwater affects the flow distribution by

**Table 10.** Annual mean discharge summary for 6-year simulations using existing (1990) and future (2008) land use for the Reedy Creek watershed, Florida

[Discharge values are in cubic feet per second]

	Annual mean discharge						6-year mean discharge
	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	
Whittenhorse Creek existing land use	2.19	10.0	6.17	7.50	11.9	11.4	8.20
future land use	3.37	11.7	7.71	8.88	13.4	12.8	9.64
Reedy Creek near Vineland existing land use	24.2	46.0	31.1	39.8	66.7	70.1	46.3
future land use	46.5	74.7	62.5	69.5	95.1	98.3	74.4
Bonnet Creek near Vineland existing land use	8.19	19.7	17.1	19.5	33.4	33.9	22.0
future land use	14.7	28.0	26.4	28.4	41.7	41.8	30.2
Reedy Creek near Loughman existing land use	21.0	59.6	33.9	45.0	84.6	96.9	56.8
future land use	51.9	100.5	79.6	87.9	126.0	138.2	97.4



**Figure 41.** Daily mean discharge duration curves of simulated values for existing (1990) and future (2008) land use of the Reedy Creek watershed, Florida.

increasing flows throughout the range of flows. The future land-use scenario duration curve for Bonnet Creek indicates increases in discharge greater than about 8 ft<sup>3</sup>/s and decreases in discharge less than about 8 ft<sup>3</sup>/s. This is consistent with the changes in land-use percentage between the existing and future land use. The Bonnet Creek sub-watershed had the greatest decrease in percentage of pervious area, and thus, the greatest increase in percentage of impervious area. The resulting increase in impervious area will increase the amount of surface runoff, which is greater during storm events at a higher discharge range of the duration curve. The larger reduction in infiltration in Bonnet Creek relative to other sub-watersheds results in substantially reduced baseflow.

## Water Quality

A rank-sum test (Mann, 1945; and Wilcoxon, 1945) was used to test whether the two watershed simulations (existing and future land use) produce populations of constituent concentrations that are identical (null hypothesis). The comparison between simulated mean constituent concentrations over the 6-year simulation period for existing and future land use indicated a difference in the mean value of a constituent for 14 of 20 possible site-constituent combinations (five sites and four constituents at each site) (table 11). The p-value associated with the mean constituent concentrations for existing and future land use is a measure of the likelihood that the mean constituent concentration values are the same (Ott, 1992, p. 230-233). A p-value of 0.000 indicates that there is no likelihood that values are the same; a p-value of 1.000 indicates that the values are identical. Six of the 20 site-constituent combinations had a significant difference at the 0.1 percent level (p-value less than 0.001), and eight of the 20 site-constituent combinations had a significant difference at the 1.0 percent level (p-value less than 0.01). For these site-constituent combinations this means that the null hypothesis can be rejected with a 99.9 and 99 percent confidence, respectively. Total phosphorus and phosphate phosphorus have the greatest tendency to reject the null hypothesis for the Reedy Creek near Vineland and Reedy Creek near Loughman sites. Ammonia nitrogen also had a statistically significant difference in concentration at Reedy Creek near Loughman. The difference between existing and

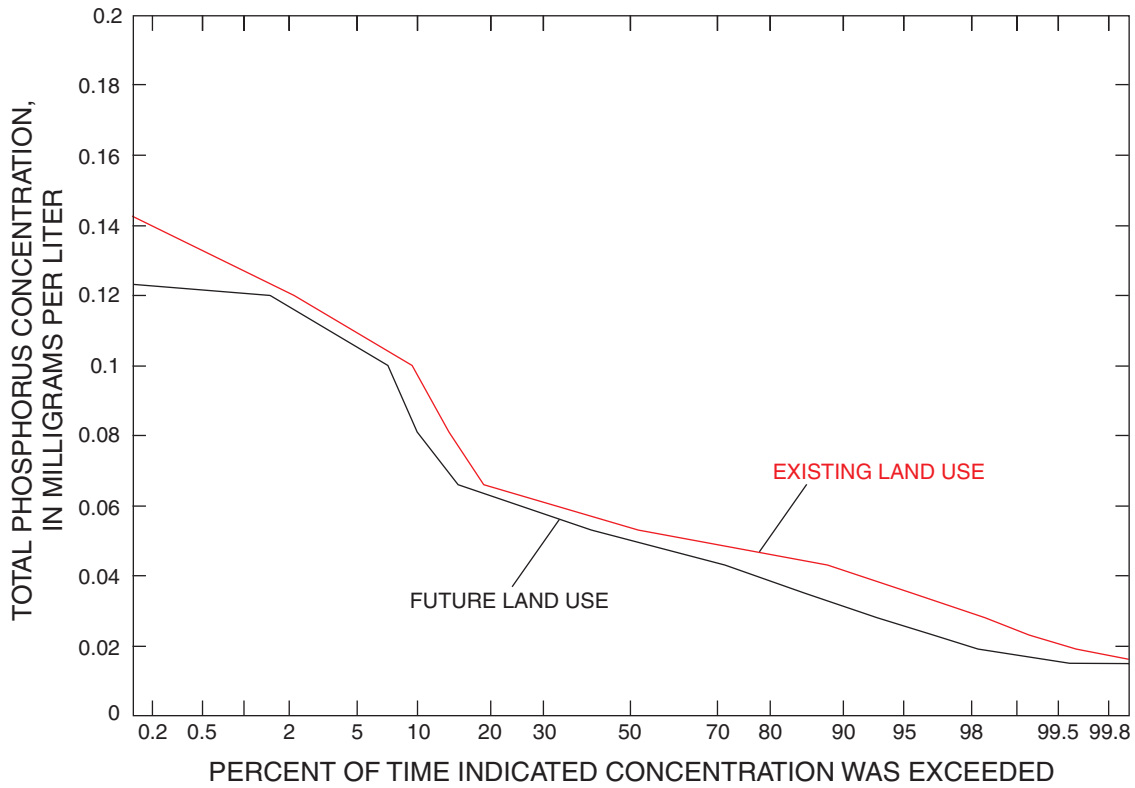
future land use mean concentration values for all site-constituent combinations was less than 0.01 mg/L.

Simulation results for Reedy Creek near Loughman illustrate the effect land-use changes within the RCID have on simulated water-quality constituents at the outflow point of the study area. Changes in land use were based only on changes within the RCID boundaries, which represent about 25.5 percent of the total Reedy Creek watershed, and assuming that land characteristics remained unchanged and no additional BMPs were implemented. Duration curves of daily mean total phosphorus and phosphate phosphorus concentrations indicated a slight decrease in constituent concentration for the future land-use scenario throughout the range of values at Reedy Creek near Loughman (figs. 42 and 43, respectively). Duration curves of daily mean ammonia nitrogen and nitrate nitrogen concentrations indicated a slight decrease in constituent concentration for values having a likelihood of exceedance less than 15 percent and no change above an exceedance of about 20 percent (figs. 44 and 45, respectively).

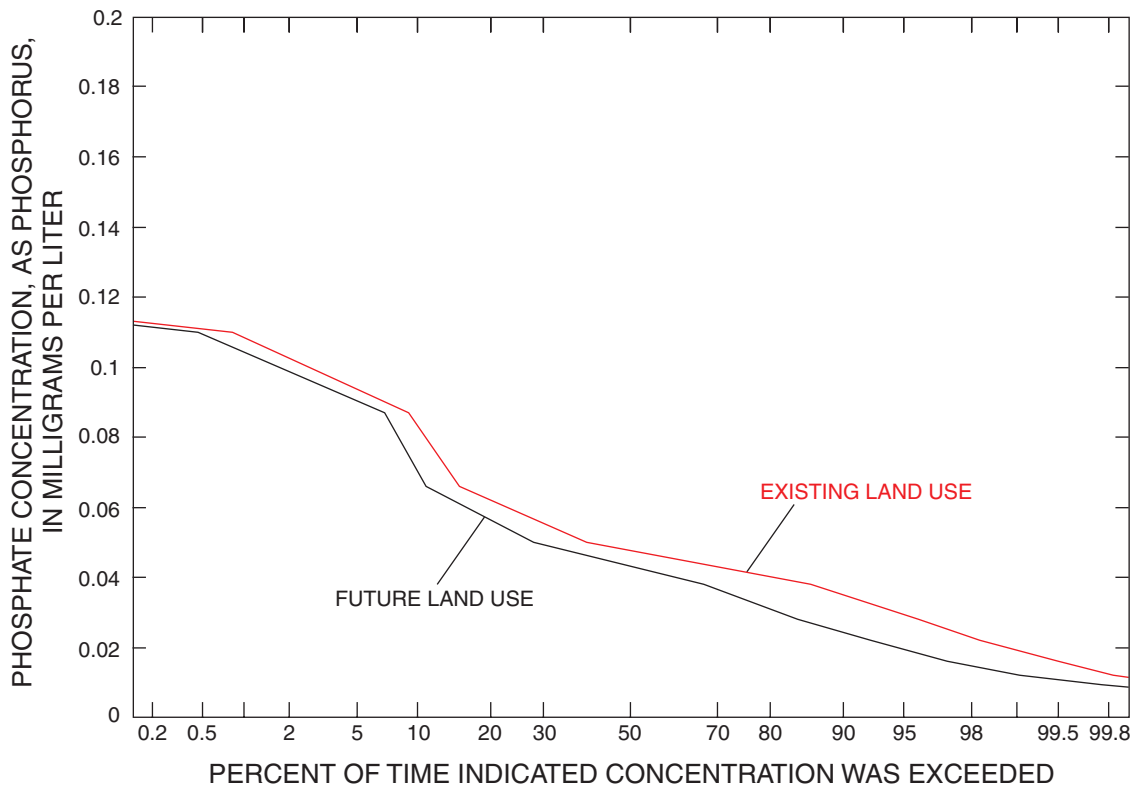
**Table 11.** Mean constituent concentrations for 6-year simulations using existing (1990) and future (2008) land use in the Reedy Creek watershed, Florida

[p-value is the probability that mean concentration values for existing and for future land use are equal; all constituent concentration values are in milligrams per liter]

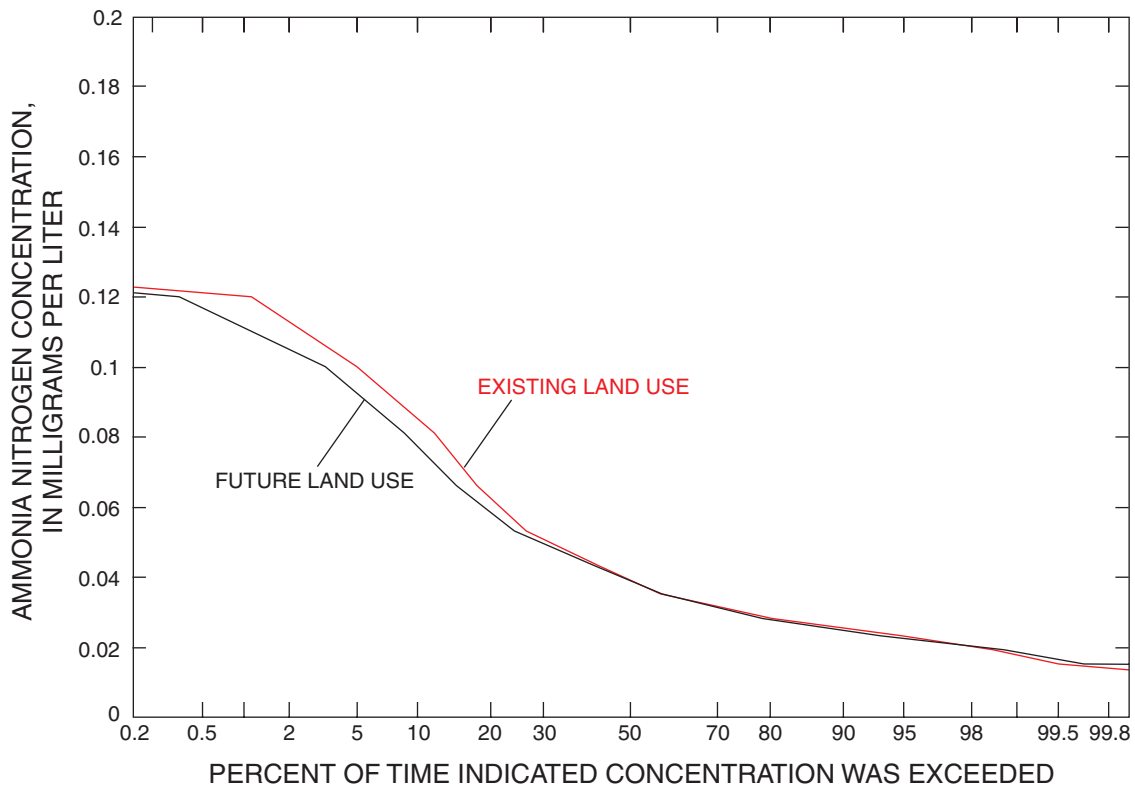
	Total phosphorus	Phosphate	Ammonia nitrogen	Nitrate nitrogen
Whittenhorse Creek				
existing land use	0.034	0.031	0.016	0.029
future land use	.033	.031	.017	.028
p-value	.0531	.1725	.0013	.0890
Davenport Creek				
existing land use	.056	.051	.034	.618
future land use	.056	.051	.034	.620
p-value	.8743	.8524	.9354	.8776
Reedy Creek near Vineland				
existing land use	.057	.051	.041	.117
future land use	.051	.044	.041	.118
p-value	.0000	.0000	.5848	.8904
Bonnet Creek near Vineland				
existing land use	.055	.043	.061	.160
future land use	.056	.043	.065	.170
p-value	.0479	.6185	.0000	.0000
Reedy Creek near Loughman				
existing land use	.059	.052	.046	.188
future land use	.053	.045	.045	.185
p-value	.0000	.0000	.0059	.1464



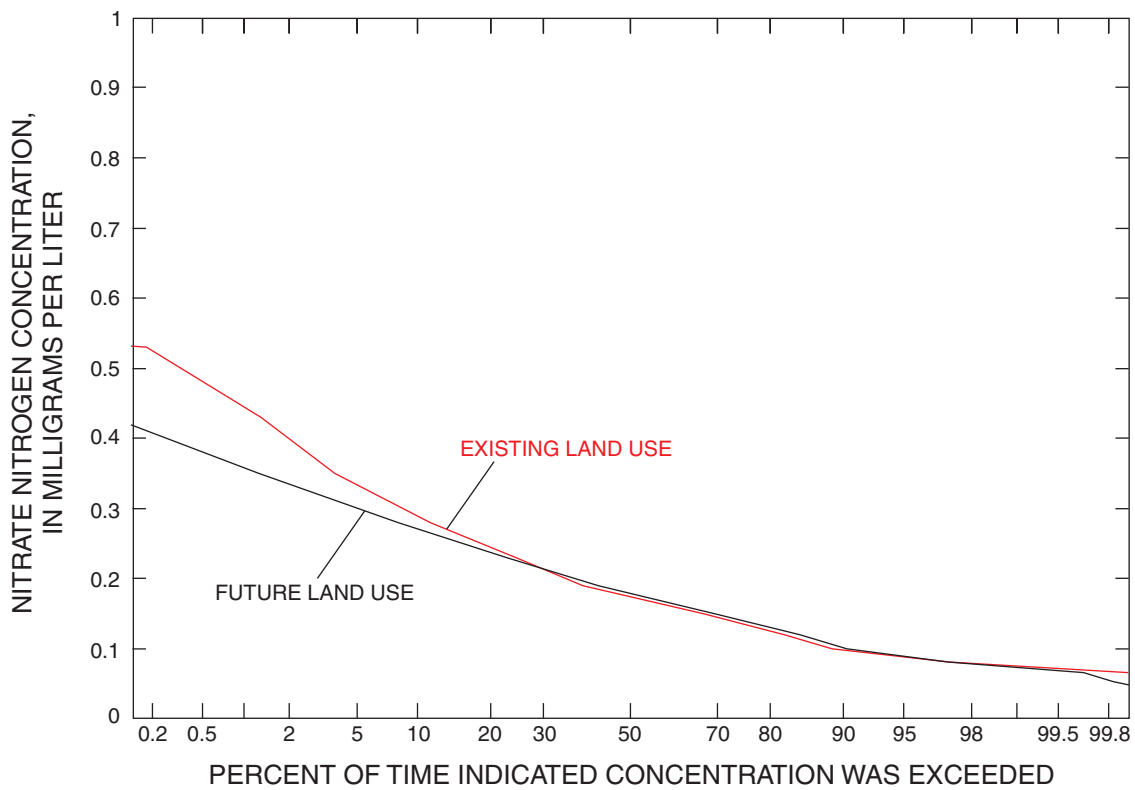
**Figure 42.** Duration curves of simulated daily mean total phosphorus concentration for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



**Figure 43.** Duration curves of simulated daily mean phosphate concentration for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



**Figure 44.** Duration curves of simulated daily mean ammonia nitrogen concentration for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



**Figure 45.** Duration curves of simulated daily mean nitrate nitrogen concentration for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.

Results were similar at Whittenhorse Creek, Reedy Creek, and Bonnet Creek near Vineland. Changes in the mean constituent concentrations are shown in table 11. Slight decreases in mean constituent concentrations and percent exceedance over the simulated period likely are due to dilution of stream-water resulting from increased discharges in the future land-use scenario. The relatively small changes in constituent concentrations between existing and future land use are reasonable relative to urban runoff quality observations made in the Nationwide Urban Runoff Project (NURP) as summarized by Novotny and Olem (1994, p. 491-493). The NURP project involved collecting intensive storm-runoff water-quality samples from 28 cities across the United States. Analysis of these data indicated that although land use has an overall effect on mean constituent concentrations, storm-to-storm variabilities eclipse these effects, thus rendering land-use categories useless in predicting urban runoff quality at unmonitored sites or in explaining site to site differences where monitoring data are available. Even though substantial land-use changes were simulated in the RCID, based on existing and projected future land use, it is not surprising that minimal changes in simulated concentrations result, given the weak relation between constituent concentrations in storm runoff and land use found in the NURP data. Therefore, comparison of constituent loads between current and future land-use

conditions is a more reasonable approach to evaluate potential changes in water quality.

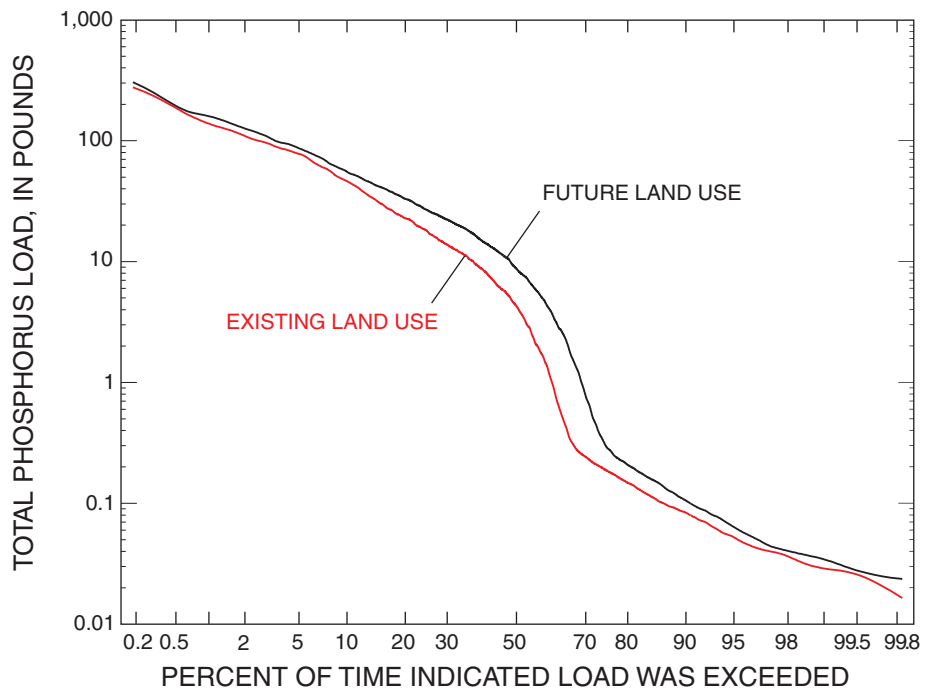
## Water-Quality Loads

Constituent loadings are a function of both discharge and constituent concentration. In general, water-quality constituent concentrations are not correlated to discharge, and discharge is the primary factor in the determination of constituent loading. The ability of the model to simulate both discharge and concentration allows the calculation and comparison of amounts or loads of a constituent transported past a given point. Maximum daily and total annual constituent loads were calculated using simulated daily mean values of discharge and constituent concentration for Reedy Creek near Loughman (table 12). Constituent loads of total phosphorus, ammonia nitrogen, and nitrate nitrogen for Reedy Creek near Loughman calculated by German (1989) are similar in magnitude to total annual constituent loads calculated by using existing land use for the 6-year period. This is further confirmation that the Reedy Creek watershed model is a reasonable representation of water-quality processes within the watershed. The simulated maximum daily load increased for all constituents for future land use, as compared to existing land use. The maximum daily nitrate nitrogen load increased about 15 percent, which was the greatest increase of all daily constituent loads.

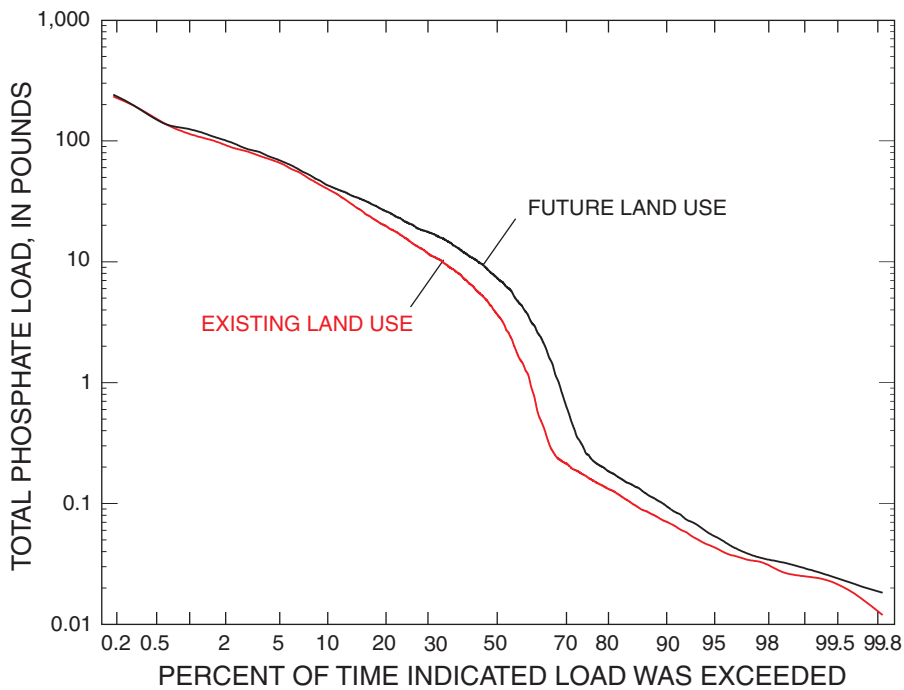
**Table 12.** Constituent load summary for Reedy Creek near Loughman, Florida, for 6-year (72-month) simulations using existing (1990) and future (2008) land use in the Reedy Creek watershed

[Load values are in pounds]

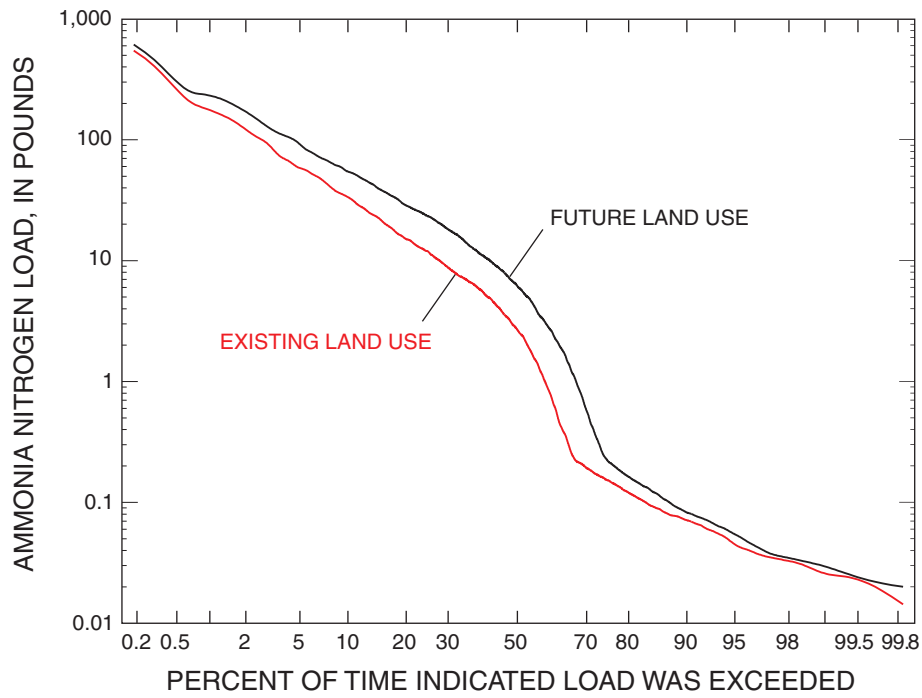
	Maximum daily load	Annual total load						6-year total load
		Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	
Total phosphorus as P								
existing land use	303	1,750	5,780	3,240	4,410	8,220	8,970	32,400
future land use	336	3,160	7,510	5,500	6,420	10,200	10,400	43,200
Phosphate, PO <sub>4</sub> as P								
existing land use	262	1,560	4,730	2,850	3,920	7,010	7,890	28,000
future land use	278	2,440	5,730	4,380	5,210	8,240	8,660	34,700
Ammonia, NH <sub>3</sub> as N								
existing land use	680	1,620	4,660	3,040	3,800	5,800	8,430	27,400
future land use	719	3,760	7,340	6,260	6,530	8,700	11,600	44,100
Nitrate, NO <sub>3</sub> as N								
existing land use	1,760	9,320	26,000	20,000	22,800	38,300	42,200	159,000
future land use	2,020	17,800	36,600	33,400	32,600	49,800	53,400	224,000



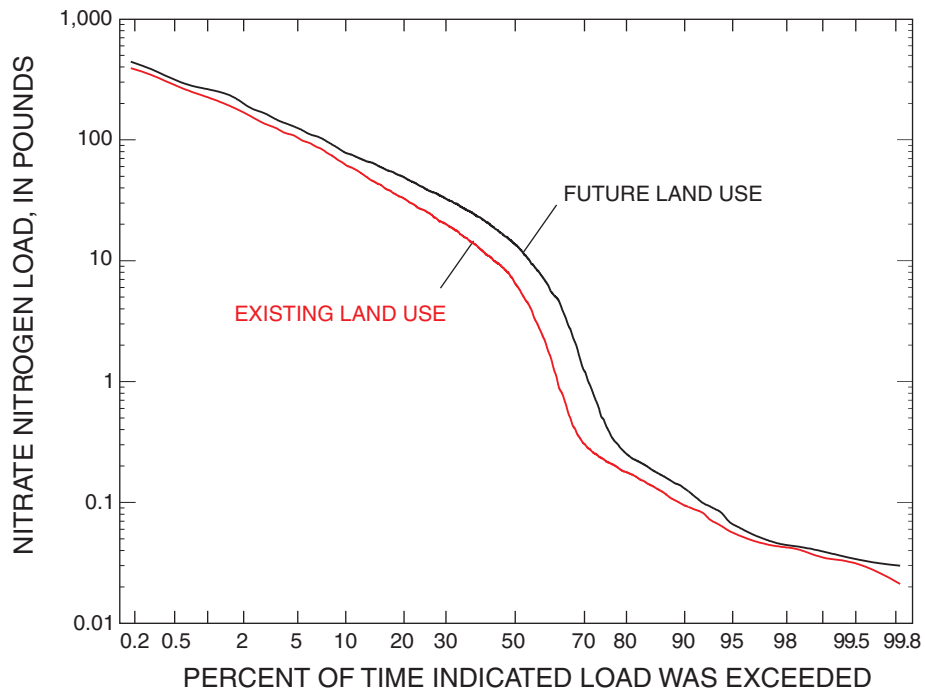
**Figure 46.** Duration curves of simulated daily total phosphorus load for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



**Figure 47.** Duration curves of simulated daily phosphate load for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



**Figure 48.** Duration curves of simulated daily ammonia nitrogen load for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



**Figure 49.** Duration curves of simulated daily nitrate nitrogen load for existing (1990) and future (2008) land use for Reedy Creek near Loughman, Florida.



On average, the maximum daily load increased 10 percent for all constituents. Similar to maximum daily loads, total annual loading of total phosphorus, phosphate phosphorus, ammonia nitrogen, and nitrate nitrogen increased for the future land-use scenario. Total annual ammonia nitrogen loading increased by about 61 percent, the greatest percentage increase of the four constituents. The smallest percentage increase of the four constituents was for total annual phosphate phosphorus loading (about 24 percent). The increases in daily and annual loads simulated for future land use are the result of increases in runoff. However, the implementation of additional BMPs potentially could mitigate some of these load increases.

Duration curves of daily total phosphorus, phosphate phosphorus, ammonia nitrogen, and nitrate nitrogen load indicated an increase in the likelihood of exceeding a given load throughout the range of daily constituent loads at Reedy Creek near Loughman (figs. 46-49). Duration curves of constituent loadings represent the percent of time a daily load is exceeded. All the duration curves indicate a slope change below a load of approximately 0.25 pounds per day (lb/day) for total phosphorus, phosphate phosphorus, and ammonia nitrogen, and 0.45 lb/day for nitrate nitrogen. The slope change corresponds to an exceedance for the existing and future land-use simulations of about 68 and 77 percent, respectively, corresponding to a daily mean discharge of about 1.0 ft<sup>3</sup>/s for Reedy Creek near Loughman (fig. 41). Simulated daily mean discharges less than about 1.0 ft<sup>3</sup>/s for Reedy Creek near Loughman differ significantly from observed discharges (fig. 18). Given the poor model fit of daily mean discharges less than 1.0 ft<sup>3</sup>/s, load exceedance for existing and future land use above 68 and 77 percent, respectively, should be considered outside of the model's range of accurate prediction.

The simulation of loads of ammonia nitrogen, nitrate nitrogen, total phosphorus, and phosphate phosphorus also is acceptably reliable for Whittenhorse Creek, Davenport Creek, and Reedy Creek near Vineland. This conclusion is made on the basis of the acceptable hydrologic simulation and the reasonable match between observed and simulated constituent concentrations at these points. Reasonable matches between observed and simulated constituent concentrations also were obtained for Bonnet Creek near Vineland and Reedy Creek near Loughman. The loads, however, are questionable because of the questionable hydrologic simulations at these locations. The changes

in simulated loads at Bonnet Creek near Vineland and Reedy Creek near Loughman as a result of projected changes in the watershed still may be useful for water-quality planning and management because the bias in the simulation of current conditions also is present in the simulation of scenarios reflecting changed land use. Therefore, the bias in each simulation will be cancelled in the comparison, and the resulting differences may be a reasonable estimate of expected changes in runoff and water quality.

In general, water-quality constituent concentrations are not correlated to discharge, and discharge is the primary factor used to determine constituent loading. Changes in land use within the RCID to a more impervious land-use type resulted in increased runoff across the study area. Because future land use outside of the RCID is difficult to predict, and because areas within the Reedy Creek watershed but external to RCID drain through the RCID, it is important to monitor changes in areas external to the RCID. Monitoring would include mapping changes in the land use of sub-watersheds draining to Reedy Creek, and monitoring the quantity and quality of waters external to the RCID draining to Reedy Creek and into the RCID.

## SUMMARY

Hydrologic and water-quality data have been collected within the 177-mi<sup>2</sup> Reedy Creek, Florida, watershed, beginning as early as 1939, but the data had not been used to evaluate the relations among land use, hydrology, and water quality. A model of the Reedy Creek watershed was developed and applied to the period from January 1990 to December 1995 to provide a computational foundation for evaluating the effects of future changes in land use on hydrology and water quality in the watershed.

The Hydrological Simulation Program-Fortran (HSPF) model was used to simulate hydrology and water quality of runoff for pervious land areas, impervious land areas, and stream reaches. Six land-use types were used to characterize the hydrology and water quality of pervious and impervious land areas in the Reedy Creek watershed: agriculture, rangeland, forest, wetlands, rapid infiltration basins (RIBS), and urban areas. Hydrologic routing and water-quality reactions were simulated to characterize hydrologic and water-quality processes and the movement of runoff and its constituents through the main stream channels and their tributaries.

Compilation of meteorologic, hydrologic, and water-quality time series data, and topographic, hydrologic, and land-use spatial data were part of the simulation plan and database development for the model. The Reedy Creek watershed was subdivided into five separate land areas representing different land characteristics and drainage features, and the stream channel system was divided into reaches based on measured channel cross-section data and topographic information. A total of 19 stream channel reaches were used to represent the movement of runoff, water-quality reactions, and constituent movement through the main stream channels and their tributaries.

Because of the complexity of the stream system within the Reedy Creek Improvement District (RCID) (hydraulic structures, retention ponds) and the anticipated difficulty of modeling the system, an approach of calibrating the model parameters for a subset of the gaged watersheds and confirming the usefulness of the parameters by simulating the remainder of the gaged sites was selected for this study. Two sub-watersheds (Whittenhorse Creek and Davenport Creek) were selected for calibration because both have similar land use to watersheds within the RCID (with the exception of urban areas).

The overall water balance for the Whittenhorse Creek calibration was very good, and the annual water balances ranged from very good to poor over the simulation period, based on the criteria of Donigan and others (1984). For Davenport Creek, the overall water balance was very good and the annual water balances ranged from very good to fair over the simulation period. Duration curves of observed and simulated daily mean discharge indicate good agreement for values at Whittenhorse Creek and an acceptable fit at Davenport Creek. Given the lack of available rainfall data for these sub-watersheds, the hydrologic calibrations of the Whittenhorse Creek and Davenport Creek sub-watersheds were considered acceptable.

The hydrologic model was tested by applying the parameter sets developed for Whittenhorse Creek and Davenport Creek to other land segments within the Reedy Creek watershed, and by comparing the simulated results to observed data sets for Reedy Creek near Vineland, Bonnet Creek near Vineland, and Reedy Creek near Loughman. The hydrologic model confirmation for Reedy Creek near Vineland (correlation coefficient, 0.91, and coefficient of model-fit efficiency, 0.78, for monthly flows) was acceptable. Flows for Bonnet Creek near Vineland were substan-

tially under simulated. The total simulated runoff volume was about 71 percent of the total observed runoff volume over the study period. Thus, the difference in total simulated runoff volume was about 29 percent. Consideration of the ground-water contribution to Bonnet Creek could improve the water balance simulation for Bonnet Creek near Vineland; however, a thorough evaluation of the ground-water contribution is beyond the scope of the current study. On longer time scales (monthly or over the 72-month simulation period), the simulated discharges for Reedy Creek near Loughman agreed well with observed data (correlation coefficient, 0.88, and coefficient of model-fit efficiency, 0.77, for monthly flows). On a shorter time scale (less than a month), however, storm volumes were greatly over simulated and low flows (less than 8 cubic feet per second) were greatly under simulated. A primary reason for the poor results at low flows is the diversion of an unknown amount of water from the RCID at the Bonnet Creek near Kissimmee site.

Selection of water-quality constituents for simulation was based primarily on the availability of water-quality data for sites throughout the Reedy Creek watershed. Dissolved oxygen (DO), nitrogen, and phosphorus species were simulated because of the availability of observed continuous and periodic water-quality data. Representation of nutrient cycling in HSPF also required simulation of biochemical oxygen demand (BOD) and phytoplankton populations. Daily constituent loadings of DO, BOD, ammonia nitrogen, nitrate nitrogen, and total phosphorus were estimated from periodically observed constituent concentrations and input as a point source of inflow to the stream reach downstream from the Cypress Creek near Vineland gaging station.

The water-quality part of the model was calibrated in an iterative manner. Calibration of water-quality constituents was performed by visual comparison of observed and simulated constituent concentrations except for DO, which was calibrated using a statistical comparison. Parameters pertaining to DO were calibrated based on observed data for the site at Reedy Creek near Vineland; parameters pertaining to other constituents were calibrated based on observed data for Whittenhorse Creek, Davenport Creek, Reedy Creek near Vineland, Bonnet Creek near Vineland, and Reedy Creek near Loughman. The correlation coefficient for simulated and observed daily mean DO concentration values at Reedy Creek near Vineland was 0.633. Simulated time series of total phosphorus,

phosphate, ammonia nitrogen, and nitrate nitrogen had acceptable agreement with periodic observed values for the Whittenhorse Creek and Davenport Creek calibration sites.

Agreement between simulated and observed constituent concentrations varied at sites in the watershed. At Reedy Creek near Vineland, simulated concentrations of total phosphorus, phosphate, and nitrate nitrogen concentrations substantially under estimated observed concentrations during 1990-91. This may be the result of increases in constituent concentrations in surface runoff, interflow, and ground water in the form of treated wastewater disposed into wetland areas draining to the stream channel upstream from the site. Simulated water-quality constituent concentrations for the Reedy Creek near Loughman site have a moderately acceptable agreement with observed constituent concentrations. The unknown amount and quality of water diverted from the Reedy Creek watershed at the Bonnet Creek near Kissimmee gaging station and undefined processes in the large wetland area upstream of the Reedy Creek at S-40 near Loughman gaging station may be affecting chemical and biochemical reactions, which affect constituent concentrations in water samples at the Reedy Creek near Loughman gaging station.

Simulation of a future land-use scenario for the Reedy Creek watershed was based on the hydrologic and water-quality simulations, projected future land use within the RCID, and existing land use for areas external to the RCID but within the Reedy Creek watershed. Future land-use data provided by the RCID were adjusted, based on land-cover type, to conform to the six land-use types that characterize the Reedy Creek watershed: agriculture, rangeland, forest, wetlands, RIBS, and urban areas. The percentage of forest and urban-impervious land use showed the most change between existing and future land use; forest decreased by 50 percent and urban-impervious area increased by 300 percent.

A comparison of daily mean discharge summaries indicated an increase in runoff at sites where a change in land use occurred. Increases in total runoff from each sub-watershed and the entire Reedy Creek watershed, as simulated in the future land-use scenario, likely can be attributed to an overall increase in impervious areas.

The simulated maximum daily load increased for all water-quality constituents for the future land-use scenario. The maximum daily nitrate nitrogen load

increased about 15 percent, which was the greatest increase of all daily constituent loads. On average, the maximum daily load increased 10 percent. Duration curves of daily total phosphorus, phosphate, ammonia nitrogen, and nitrate nitrogen load indicated an increase in the likelihood of exceeding a given load throughout the range of daily constituent loads at Reedy Creek near Loughman. The increases in daily and annual loads simulated for future land use are the result of increases in runoff. However, the implementation of additional BMPs potentially could mitigate some of these load increases.

Because future land use outside the RCID is difficult to predict, and because areas within the Reedy Creek watershed but external to RCID drain through the RCID, it is important to monitor changes in areas external to the RCID. Monitoring would include mapping changes in the land use of sub-watersheds draining to Reedy Creek, and monitoring the quantity and quality of waters external to the RCID draining to Reedy Creek and into the RCID.

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## Appendix A

**Appendix A.** Hydrological Simulation Program-Fortran (HSPF) subroutines and parameters used to simulate water-quality processes in a reach or mixed reservoir for the Reedy Creek watershed, Florida

[OXRX, subroutine for simulation of primary processes which determines dissolved oxygen concentration; NUTRX, subroutine for simulation of inorganic nitrogen and phosphorus balances; PLANK, subroutine for simulation of plankton populations and associated reactions; BOD, biochemical oxygen demand; DO, dissolved oxygen]

Abbreviation	Explanation	Water-quality subroutine
KBOD20	Unit BOD decay rate at 20 degrees Celsius	OXRX
TCBOD	Temperature correction coefficient for BOD decay	OXRX
KODSET	Rate of BOD settling	OXRX
SUPSAT	Maximum allowable DO supersaturation	OXRX
BENOD	Benthic oxygen demand at 20 degrees Celsius	OXRX
TCBEN	Temperature correction coefficient for benthic oxygen demand	OXRX
EXPOD	Exponential factor in the DO term of the benthic oxygen demand equation	OXRX
BRBOD (1)	Benthic release rate of BOD under aerobic conditions	OXRX
BRBOD (2)	Benthic release rate of BOD under anaerobic conditions	OXRX
EXPREL	Exponent in the DO term of the benthic BOD release equation	OXRX
TCGINV	Temperature correction coefficient for surface gas invasion	OXRX
REAK	Empirical constant in the equation used to calculate the reaeration coefficient	OXRX
EXPRED	Exponent of the depth	OXRX
EXPREV	Exponent of velocity in the reaeration coefficient equation	OXRX
BRTAM (1)	Benthic release rates of ammonia under aerobic conditions	NUTRX
BRTAM (2)	Benthic release rates of ammonia under anaerobic conditions	NUTRX
BRPO4 (1)	Benthic release rates of ortho-phosphorus under aerobic conditions	NUTRX
BRPO4 (2)	Benthic release rates of ortho-phosphorus under anaerobic conditions	NUTRX
ANAER	Concentration of DO below which anaerobic conditions are assumed to exist	NUTRX
KTAM20	Nitrification rate of ammonia at 20 degrees Celsius	NUTRX
KNO220	Nitrification rate of nitrite at 20 degrees Celsius	NUTRX
KNO320	Nitrate denitrification rate at 20 degrees Celsius	NUTRX
TCNIT	Temperature correction coefficient for nitrification	NUTRX
TCDEN	Temperature correction coefficient for denitrification	NUTRX
DENOXT	Dissolved oxygen concentration threshold for denitrification	NUTRX
EXPNVG	Exponent in the gas layer mass transfer coefficient equation for ammonia volatilization	NUTRX
EXPNVL	Exponent in the gas liquid layer mass transfer coefficient equation for ammonia volatilization	NUTRX
RATCLP	Ratio of chlorophyll-A content of biomass to phosphorus content	PLANK
NONREF	Non-refractory fraction of algae and zooplankton biomass	PLANK
LITSED	Multiplication factor for total sediment concentration used to determine sediment contribution to light extinction	PLANK
ALNRP	Fraction of nitrogen requirements for phytoplankton growth that is satisfied by nitrate	PLANK
EXTB	Base extinction coefficient for light	PLANK
MALGR	Maximum unit algal growth rate	PLANK
CMMLT	Michaelis-Menton constant for light limited growth	PLANK
CMMN	Nitrate Michaelis-Menton constant for nitrogen-limited growth	PLANK
CMMNP	Nitrate Michaelis-Menton constant for phosphorus-limited growth	PLANK
CMMP	Phosphate Michaelis-Menton constant for phosphorus-limited growth	PLANK
TALGRH	Temperature above which algal growth ceases	PLANK
TALGRL	Temperature below which algal growth ceases	PLANK
TALGRM	Temperature below which algal growth is retarded	PLANK
ALR20	Algal unit respiration rate at 20 degrees Celsius	PLANK
ALDH	High algal unit death rate	PLANK
ALDL	Low algal unit death rate	PLANK
OXALD	Increment to the phytoplankton unit death rate due to anaerobic conditions	PLANK
NALDH	Inorganic nitrogen concentration below which high algal death rate occurs	PLANK
PALDH	Inorganic phosphorus concentration below which high algal death rate occurs	PLANK
SEED	Minimum concentration of phytoplankton not subject to advection	PLANK
MXSTAY	Concentration of phytoplankton not subject to advection at very low flow	PLANK
OREF	Outflow at which the concentration of phytoplankton not subject to advection is midway between SEED and MXSTAY	PLANK
CLALDH	Chlorophyll-A concentration above which high algal death rate occurs	PLANK
PHYSET	Rate of phytoplankton settling	PLANK
REFSET	Rate of settling for dead refractory organics	PLANK



## Appendix B

**Appendix B1. Hydrological Simulation Program-Fortran parameter values for pervious land areas used to simulate hydrology for the Reedy Creek watershed, Florida**  
[in., inches; mm, millimeters; hr, hour; ft, feet; m, meters. Explanation of parameter abbreviations is given in table 1]

Land segment	Land-use type	LZSN (in.)	INFILT (in./hr)	LSUR (ft)	SLSUR (none)	KVARY (/in.)	AGWRC (/day)	INFEXP (none)	INFILD (none)	DEEPPR (none)	BASETP (none)	AGWETP (none)	CEPSC (in.)	UZSN (in.)	NSUR <sup>1</sup> (none)	INTFW (none)	IRC (day)
1	Agriculture	2.0	0.08	1,252.9	0.008	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.08	0.26	0.2	0.5	0.8
1	Forest	2.0	0.2	855.2	0.005	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.10	0.73	0.35	0.6	0.8
1	Rangeland	2.0	0.2	1,182.0	0.011	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.42	0.15	0.5	0.8
1	Urban	2.0	0.06	1,144.8	0.007	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.42	0.10	0.5	0.8
1	Wetland	1.5	0.2	943.8	0.004	0.0	0.97	2.0	2.0	0.4	0.0	0.1	0.20	0.46	0.35	0.7	0.8
1	RIBS	2.0	0.25	100.0	0.001	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.00	0.70	0.10	0.6	0.8
3	Agriculture	2.0	0.2	795.3	0.014	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.08	0.20	0.20	1.0	0.9
3	Forest	2.0	0.25	1,372.0	0.028	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.10	0.56	0.35	1.0	0.9
3	Rangeland	2.0	0.25	1,147.1	0.020	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.32	0.15	1.0	0.9
3	Urban	2.0	0.07	1,223.6	0.016	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.32	0.10	1.0	0.9
3	Wetland	1.5	0.25	690.7	0.004	0.0	0.97	2.0	2.0	0.4	0.0	0.1	0.20	0.35	0.35	1.0	0.9
3	RIBS	2.0	0.25	100.0	0.001	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.00	0.70	0.10	1.0	0.9
4	Agriculture	2.0	0.2	481.9	0.013	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.08	0.20	0.20	1.0	0.9
4	Forest	2.0	0.25	433.0	0.026	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.10	0.56	0.35	1.0	0.9
4	Rangeland	2.0	0.25	1,937.8	0.028	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.32	0.15	1.0	0.9
4	Urban	2.0	0.07	1,311.2	0.031	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.32	0.1	1.0	0.9
4	Wetland	1.5	0.25	510.7	0.004	0.0	0.97	2.0	2.0	0.4	0.0	0.1	0.20	0.35	0.35	1.0	0.9
4	RIBS	2.0	0.25	100.0	0.001	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.00	0.7	0.10	1.0	0.9
5	Agriculture	2.0	0.08	792.0	0.016	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.08	0.26	0.20	0.5	0.8
5	Forest	2.0	0.2	318.6	0.016	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.10	0.73	0.35	0.6	0.8
5	Rangeland	2.0	0.2	847.8	0.015	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.42	0.15	0.5	0.8
5	Urban	2.0	0.06	642.1	0.010	0.0	0.97	2.0	2.0	0.5	0.0	0.0	0.05	0.42	0.10	0.5	0.8
5	Wetland	1.5	0.2	662.2	0.005	0.0	0.97	2.0	2.0	0.4	0.0	0.1	0.20	0.46	0.35	0.7	0.8

<sup>1</sup>NSUR is Manning's n coefficient (dimensionless).

**Appendix B2.** Hydrological Simulation Program-Fortran monthly index values for density of deep-rooted vegetation for pervious land areas used to simulate hydrology for the Reedy Creek watershed, Florida

Land segment	Land-use type	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
1	Agriculture	0.1	0.2	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.1
1	Forest	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
1	Rangeland	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
1	Urban	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
1	Wetland	0.5	0.6	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.5
1	RIBS	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
3	Agriculture	0.1	0.2	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.1
3	Forest	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
3	Rangeland	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
3	Urban	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
3	Wetland	0.5	0.6	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.5
3	RIBS	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
4	Agriculture	0.1	0.2	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.1
4	Forest	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
4	Rangeland	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
4	Urban	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
4	Wetland	0.5	0.6	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.5
4	RIBS	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
5	Agriculture	0.1	0.2	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.1
5	Forest	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
5	Rangeland	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
5	Urban	0.2	0.3	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.2
5	Wetland	0.5	0.6	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.8	0.6	0.5

**Appendix B3.** Hydrological Simulation Program-Fortran parameter values for impervious land areas used to simulate hydrology for the Reedy Creek watershed, Florida [ft, feet; in., inches; explanation of parameter abbreviations is given in table 1]

Land segment	LSUR (ft)	SLSUR (none)	NSUR <sup>1</sup>	RETSC (in.)
1	200	0.01015	0.015	0.05
3	200	0.01015	0.015	0.05
4	200	0.01015	0.015	0.05
5	200	0.01015	0.015	0.05

<sup>1</sup>NSUR is Manning's n coefficient (dimensionless).

## Appendix C

**Appendix C1. Hydrological Simulation Program-Fortran (HSPF) pervious land area parameter values used to simulate build-up and wash-off of constituents from the land surface, and interflow and ground-water constituent contribution for the Reedy Creek watershed, Florida**

[NH4, ammonia nitrogen; NO3, nitrate nitrogen; PO4, ortho-phosphate; BOD, biochemical oxygen demand; all units are milligrams per liter]

Land segment	Land-use type	Monthly accumulation rate				Monthly accumulation limit				Interflow concentration				Ground-water concentration			
		NH4	NO3	PO4	BOD	NH4	NO3	PO4	BOD	NH4	NO3	PO4	BOD	NH4	NO3	PO4	BOD
1	Forest	0.002	0.005	0.002	0.20	0.008	0.010	0.004	0.45	0.02	0.05	0.025	2.0	0.02	0.05	0.025	2.0
1	Rangeland	0.006	0.050	0.004	0.35	0.024	0.100	0.012	0.70	0.10	0.15	0.100	3.0	0.10	0.15	0.100	3.0
1	Urban	0.008	0.030	0.004	0.30	0.032	0.060	0.012	0.60	0.10	0.10	0.160	5.0	0.10	0.15	0.160	5.0
1	Wetland	0.002	0.002	0.002	0.10	0.008	0.004	0.004	0.20	0.03	0.02	0.010	1.0	0.03	0.01	0.010	1.0
1	RIBS	0.002	0.010	0.004	0.50	0.012	0.020	0.012	1.00	0.10	5.00	0.010	1.0	0.10	5.00	0.010	1.0
3	Agriculture	0.02	0.100	0.004	0.50	0.040	0.200	0.012	1.00	0.10	0.30	0.120	5.0	0.10	0.30	0.120	5.0
3	Forest	0.002	0.005	0.002	0.20	0.008	0.010	0.004	0.45	0.02	0.05	0.025	2.0	0.02	0.05	0.025	2.0
3	Rangeland	0.006	0.050	0.004	0.35	0.024	0.100	0.012	0.70	0.10	0.15	0.100	3.0	0.10	0.15	0.100	3.0
3	Urban	0.008	0.030	0.004	0.30	0.032	0.060	0.012	0.60	0.10	0.10	0.160	5.0	0.10	0.15	0.160	5.0
3	Wetland	0.002	0.002	0.002	0.10	0.008	0.004	0.004	0.20	0.03	0.01	0.010	1.0	0.03	0.01	0.010	1.0
3	RIBS	0.002	0.0100	0.004	0.50	0.012	0.020	0.012	1.00	0.10	5.00	0.010	1.0	0.10	5.00	0.010	1.0
4	Agriculture	0.020	0.100	0.004	0.50	0.040	0.200	0.012	1.00	0.10	0.30	0.120	5.0	0.10	0.30	0.120	5.0
4	Forest	0.002	0.005	0.002	0.20	0.008	0.010	0.004	0.45	0.02	0.05	0.025	2.0	0.02	0.05	0.025	2.0
4	Rangeland	0.006	0.050	0.004	0.35	0.024	0.100	0.012	0.70	0.10	0.15	0.100	3.0	0.10	0.15	0.100	3.0
4	Urban	0.008	0.030	0.004	0.30	0.032	0.060	0.012	0.60	0.10	0.10	0.160	5.0	0.10	0.15	0.160	5.0
4	Wetland	0.002	0.002	0.002	0.10	0.008	0.004	0.004	0.20	0.03	0.01	0.010	1.0	0.03	0.01	0.010	1.0
4	RIBS	0.002	0.010	0.004	0.50	0.012	0.020	0.012	1.00	0.10	5.00	0.010	1.0	0.10	5.00	0.010	1.0
5	Agriculture	0.020	0.100	0.004	0.50	0.040	0.200	0.012	1.00	0.10	0.30	0.060	5.0	0.10	0.30	0.060	5.0
5	Forest	0.002	0.005	0.002	0.20	0.008	0.010	0.004	0.45	0.02	0.05	0.012	2.0	0.02	0.05	0.012	2.0
5	Rangeland	0.006	0.050	0.004	0.35	0.024	0.100	0.012	0.70	0.10	0.15	0.005	3.0	0.10	0.15	0.005	3.0
5	Urban	0.008	0.030	0.004	0.30	0.032	0.060	0.012	0.60	0.10	0.10	0.080	5.0	0.10	0.15	0.080	5.0
5	Wetland	0.002	0.002	0.002	0.10	0.008	0.004	0.004	0.20	0.03	0.01	0.005	1.0	0.03	0.01	0.005	1.0

**Appendix C2.** Hydrological Simulation Program-Fortran (HSPF) parameters used to simulate build-up and wash-off of constituent from impervious land areas for the Reedy Creek watershed, Florida

[NO3, nitrate nitrogen; PO4, ortho-phosphate; BOD, biochemical oxygen demand; qty, quantity; ac, acre; in., inches]

Abbrevia- tion	Explanation	Units	Constituent		
			NO3	PO4	BOD
SQO	Initial storage of constituent directly associated with overland flow on the surface of the impervious land surface.	qty/ac	0.007	0.002	1.000
POTFW	Washoff potency factor.	qty/ton	0.000	0.000	0.000
ACQOP	Ratio of constituent yield to sediment outflow.	qty/ac/day	0.006	0.001	0.150
SQOLIM	Maximum storage of of constituent directly associated with overland flow on the surface.	qty/ac	0.009	0.002	2.000
WSQOP	Rate of surface runoff that will remove 90 percent of stored constituent directly associated with overland flow per hour.	in./hr	0.5	0.5	0.5

**Appendix C3.** Hydrological Simulation Program-Fortran (HSPF) parameter values used to simulate water-quality processes in a reach or mixed reservoir for the Reedy Creek watershed, Florida

[OXRX, subroutine for simulation of primary processes which determine dissolved oxygen concentration; NUTRX, subroutine for simulation of inorganic nitrogen and phosphorus balances; PLANK, subroutine for simulation of plankton populations and associated reactions; hr, hour; ft, feet; mg, milligrams; L, liter; mg/L milligrams per liter; ly, langley; min, minute; degF, degrees Fahrenheit; ft<sup>3</sup>, cubic feet; s, second; µg, micrograms. Explanation of parameter abbreviations is given in appendix A; see table 6 for listing of stream reaches]

Water-quality subroutine	Abbreviation	Units	Stream reach					
			2-15	16	31	41	51	61
OXRX	KBOD20	/hr	0.01	0.01	0.01	0.01	0.01	0.01
OXRX	KODSET	ft/hr	0.005	0.005	0.005	0.005	0.005	0.005
OXRX	BENOD	mg/m <sup>2</sup> -hr	40.0	20.0	80.0	80.0	80.0	40.0
OXRX	TCBEN	none	1.1	1.1	1.1	1.1	1.1	1.1
OXRX	EXPOD	none	1.2	1.2	1.2	1.2	1.2	1.2
OXRX	BRBOD (1)	mg/m <sup>2</sup> -hr	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
OXRX	BRBOD (2)	mg/m <sup>2</sup> -hr	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
OXRX	EXPREL	none	2.82	2.82	2.82	2.82	2.82	2.82
OXRX	REAK	/hr	0.2	0.2	0.2	0.2	0.2	0.2
OXRX	EXPRED	none	-1.1	-1.1	-1.1	-1.1	-1.1	-1.1
OXRX	EXPREV	none	1.1	1.1	1.1	1.1	1.1	1.1
NUTRX	BRTAM(1)	mg/m <sup>2</sup> -hr	0.0	0.0	0.0	0.0	0.0	0.0
NUTRX	BRTAM(2)	mg/m <sup>2</sup> -hr	0.0	0.0	0.0	0.0	0.0	0.0
NUTRX	BRPO4(1)	mg/m <sup>2</sup> -hr	0.0	0.0	0.0	0.0	0.0	0.0
NUTRX	BRPO4(2)	mg/m <sup>2</sup> -hr	0.0	0.0	0.0	0.0	0.0	0.0
NUTRX	ANAER	mg/L	0.005	0.005	0.005	0.005	0.005	0.005
NUTRX	KTAM20	/hr	0.015	0.015	0.003	0.003	0.003	0.015
NUTRX	KNO220	/hr	0.002	0.002	0.002	0.002	0.002	0.002
NUTRX	TCNIT	none	1.07	1.07	1.07	1.07	1.07	1.07
NUTRX	KNO320	/hr	0.001	0.001	0.001	0.001	0.001	0.001
NUTRX	TCDEN	none	1.04	1.04	1.04	1.04	1.04	1.04
NUTRX	DENOXT	mg/L	5.00	5.00	5.00	5.00	5.00	5.00
NUTRX	EXPNVG	none	0.5	0.5	0.5	0.5	0.5	0.5
NUTRX	EXPNVL	none	0.6667	0.6667	0.6667	0.6667	0.6667	0.6667
PLANK	RATCLP	none	0.6	0.6	0.6	0.6	0.6	0.6
PLANK	NONREF	none	0.5	0.5	0.5	0.5	0.5	0.5
PLANK	LITSED	L/mg-ft	0.0	0.0	0.0	0.0	0.0	0.0
PLANK	ALNPR	none	0.7	0.7	0.7	0.7	0.7	0.7
PLANK	EXTB	/ft	1.0	1.0	1.0	1.0	1.0	1.0
PLANK	MALGR	/hr	0.07	0.07	0.07	0.07	0.07	0.07
PLANK	CMMMLT	ly/min	0.01	0.01	0.01	0.01	0.01	0.01
PLANK	CMMN	mg/L	0.025	0.025	0.025	0.025	0.025	0.025
PLANK	CMMNP	mg/L	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
PLANK	CMMP	mg/L	0.005	0.005	0.005	0.005	0.005	0.005
PLANK	TALGRH	degF	95.0	95.0	95.0	95.0	95.0	95.0
PLANK	TALGRL	degF	-20.0	-20.0	-20.0	-20.0	-20.0	-20.0
PLANK	TALGRM	degF	86.0	86.0	86.0	86.0	86.0	86.0
PLANK	ALR20	/hr	0.005	0.005	0.005	0.005	0.005	0.005
PLANK	ALDH	/hr	0.01	0.01	0.01	0.01	0.01	0.01
PLANK	ALDL	/hr	0.001	0.001	0.001	0.001	0.001	0.001



**Appendix C3.** Hydrological Simulation Program-Fortran (HSPF) parameter values used to simulate water-quality processes in a reach or mixed reservoir for the Reedy Creek watershed, Florida--Continued

[OXRX, subroutine for simulation of primary processes which determine dissolved oxygen concentration; NUTRX, subroutine for simulation of inorganic nitrogen and phosphorus balances; PLANK, subroutine for simulation of plankton populations and associated reactions; hr, hour; ft, feet; mg, milligrams; L, liter; mg/L milligrams per liter; ly, langley; min, minute; degF, degrees Fahrenheit; ft<sup>3</sup>, cubic feet; s, second; µg, micrograms. Explanation of parameter abbreviations is given in appendix A; see table 6 for listing of stream reaches]

Water-quality subroutine	Abbreviation	Units	Stream reach					
			2-15	16	31	41	51	61
PLANK	OXALD	/hr	0.03	0.03	0.03	0.03	0.03	0.03
PLANK	NALDH	mg/L	0.01	0.01	0.01	0.01	0.01	0.01
PLANK	PALDH	mg/L	0.002	0.002	0.002	0.002	0.002	0.002
PLANK	SEED	mg/L	0.5	0.5	0.5	0.5	0.5	0.5
PLANK	MXSTAY	mg/L	2.0	2.0	2.0	2.0	2.0	2.0
PLANK	OREF	ft <sup>3</sup> /s	20.0	20.0	20.0	20.0	20.0	20.0
PLANK	CLALDH	µg/L	20.0	20.0	20.0	20.0	20.0	20.0
PLANK	PHYSET	ft/hr	0.02	0.02	0.02	0.02	0.02	0.02
PLANK	REFSET	ft/hr	0.02	0.02	0.02	0.02	0.02	0.02
PLANK	RATCLP	none	0.6	0.6	0.6	0.6	0.6	0.6

Appendixes D-E, pages 75-221,  
are included on the CDROM  
located in the pocket on the back cover.  
WRIR 02-4018

Note to users:

Appendixes D and E are included with the online version of WRIR 02-4018.

## Appendix D



## APPENDIX D

User control input file for simulating existing land use with the Hydrological Simulation Program-Fortran

```
----- Reedy.uci -----***
RUN

GLOBAL
  Reedy Creek, Orange and Osceola Counties, Florida
  START      1990  1  1  0  0  END      1995 12 31 24  0
  RUN INTERP OUTPUT LEVEL   4    1
  RESUME     0 RUN      1                UNIT SYSTEM    1
END GLOBAL

FILES
<type> <fun>***<-----fname----->
MESSU   25   reedy.ech
WDM     27   reedy.wdm
        90   reedy.out
        91   totrept1.out
        93   totrept3.out
        95   totrept5.out
        96   totrept6.out
        81   acrrept1.out
        83   acrrept3.out
        85   acrrept5.out
        86   acrrept6.out
        71   pctrept1.out
        73   pctrept3.out
        75   pctrept5.out
        76   pctrept6.out
        51   rchflux.out
END FILES

OPN SEQUENCE
  INGRP          INDELT  1: 0
  PERLND         31
  PERLND         32
  PERLND         33
  PERLND         34
  PERLND         39
  PERLND         35
  IMPLND         34
  RCHRES         31
  RCHRES         41

  PERLND         51
  PERLND         52
  PERLND         53
  PERLND         54
  PERLND         55
  PERLND         59
  IMPLND         54
  RCHRES         51
  COPY           102
```

PERLND	61
PERLND	62
PERLND	63
PERLND	64
PERLND	65
IMPLND	64
RCHRES	61
COPY	103

PERLND	11
PERLND	12
PERLND	13
PERLND	14
PERLND	15
PERLND	16
PERLND	17
PERLND	18
PERLND	19
IMPLND	14
RCHRES	2
RCHRES	3
RCHRES	4
RCHRES	5
RCHRES	6
RCHRES	7
RCHRES	8
RCHRES	9
RCHRES	10
RCHRES	11
RCHRES	12
RCHRES	13
RCHRES	14
RCHRES	15
RCHRES	16
REPORT	1
REPORT	3
REPORT	5
REPORT	6
REPORT	11
REPORT	13
REPORT	15
REPORT	16
REPORT	21
REPORT	23
REPORT	25
REPORT	26
REPORT	100
COPY	104
COPY	105
COPY	106
COPY	1
COPY	2
COPY	3
COPY	4

END OPN SEQUENCE

REPORT

REPORT-FLAGS

Rept-opn\*\*\*

***	x	-	x	REPT	NCON	NSRC	FORM	CWID	PWID	PLIN	PCOD	PYR
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	3			93	9	7	2	12	1000	1000	5	12
	5			95	9	7	2	12	1000	1000	5	12
	6			96	9	7	2	12	1000	1000	5	12
	11			81	9	7	1	12	1000	1000	5	12
	13			83	9	7	1	12	1000	1000	5	12
	15			85	9	7	1	12	1000	1000	5	12
	16			86	9	7	1	12	1000	1000	5	12
	21			71	9	7	2	12	1000	1000	5	12
	23			73	9	7	2	12	1000	1000	5	12
	25			75	9	7	2	12	1000	1000	5	12
	26			76	9	7	2	12	1000	1000	5	12
	100			51	40	19	1	12	1000	1000	5	12

END REPORT-FLAGS

REPORT-TITLE

Rept-opn\*\*\*

***	x	-	x	<-----title----->
	1			Land Surface total-loads
	3			Land Surface total-loads
	5			Land Surface total-loads
	6			Land Surface total-loads
	11			Land Surface total-loads
	13			Land Surface total-loads
	15			Land Surface total-loads
	16			Land Surface total-loads
	21			Land Surface total-loads
	23			Land Surface total-loads
	25			Land Surface total-loads
	26			Land Surface total-loads
	100			Instream Process Fluxes

END REPORT-TITLE

REPORT-SRC

Rept-opn\*\*\*

***	x	-	x	<----source-name---->
	1			Agric
	1			Forest
	1			Range
	1			Urban P
	1			Wetland
	1			RIBs
	1			Impervious
	3			Agric
	3			Forest
	3			Range
	3			Urban P
	3			Wetland
	3			RIBs
	3			Impervious
	5			Agric
	5			Forest
	5			Range

5 Urban P  
5 Wetland  
5 RIBs  
5 Impervious  
6 Agric  
6 Forest  
6 Range  
6 Urban P  
6 Wetland  
6 RIBs  
6 Impervious  
11 Agric  
11 Forest  
11 Range  
11 Urban P  
11 Wetland  
11 RIBs  
11 Impervious  
13 Agric  
13 Forest  
13 Range  
13 Urban P  
13 Wetland  
13 RIBs  
13 Impervious  
15 Agric  
15 Forest  
15 Range  
15 Urban P  
15 Wetland  
15 RIBs  
15 Impervious  
16 Agric  
16 Forest  
16 Range  
16 Urban P  
16 Wetland  
16 RIBs  
16 Impervious  
21 Agric  
21 Forest  
21 Range  
21 Urban P  
21 Wetland  
21 RIBs  
21 Impervious  
23 Agric  
23 Forest  
23 Range  
23 Urban P  
23 Wetland  
23 RIBs  
23 Impervious  
25 Agric  
25 Forest



25 Range  
 25 Urban P  
 25 Wetland  
 25 RIBs  
 25 Impervious  
 26 Agric  
 26 Forest  
 26 Range  
 26 Urban P  
 26 Wetland  
 26 RIBs  
 26 Impervious  
 100 Rch 31  
 100 Rch 41  
 100 Rch 51  
 100 Rch 61  
 100 Rch 2  
 100 Rch 3  
 100 Rch 4  
 100 Rch 5  
 100 Rch 6  
 100 Rch 7  
 100 Rch 8  
 100 Rch 9  
 100 Rch 10  
 100 Rch 11  
 100 Rch 12  
 100 Rch 13  
 100 Rch 14  
 100 Rch 15  
 100 Rch 16

END REPORT-SRC

REPORT-CON

Rept-opn\*\*\*

***	x	-	x<-----con-name----->	TRAN	SIGD	DECP
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	1		NO3	SUM	5	3
	1		Organic N	SUM	5	3
	1		Total N	SUM	5	3
	1		PO4	SUM	5	3
	1		Organic P	SUM	5	3
	1		Total P	SUM	5	3
	1		BOD	SUM	5	3
	1		TOC	SUM	5	3
	3		NH3	SUM	5	3
	3		NO3	SUM	5	3
	3		Organic N	SUM	5	3
	3		Total N	SUM	5	3
	3		PO4	SUM	5	3
	3		Organic P	SUM	5	3
	3		Total P	SUM	5	3
	3		BOD	SUM	5	3
	3		TOC	SUM	5	3
	5		NH3	SUM	5	3
	5		NO3	SUM	5	3

5	Organic N	SUM	5	3
5	Total N	SUM	5	3
5	PO4	SUM	5	3
5	Organic P	SUM	5	3
5	Total P	SUM	5	3
5	BOD	SUM	5	3
5	TOC	SUM	5	3
6	NH3	SUM	5	3
6	NO3	SUM	5	3
6	Organic N	SUM	5	3
6	Total N	SUM	5	3
6	PO4	SUM	5	3
6	Organic P	SUM	5	3
6	Total P	SUM	5	3
6	BOD	SUM	5	3
6	TOC	SUM	5	3
11	NH3	SUM	5	3
11	NO3	SUM	5	3
11	Organic N	SUM	5	3
11	Total N	SUM	5	3
11	PO4	SUM	5	3
11	Organic P	SUM	5	3
11	Total P	SUM	5	3
11	BOD	SUM	5	3
11	TOC	SUM	5	3
13	NH3	SUM	5	3
13	NO3	SUM	5	3
13	Organic N	SUM	5	3
13	Total N	SUM	5	3
13	PO4	SUM	5	3
13	Organic P	SUM	5	3
13	Total P	SUM	5	3
13	BOD	SUM	5	3
13	TOC	SUM	5	3
15	NH3	SUM	5	3
15	NO3	SUM	5	3
15	Organic N	SUM	5	3
15	Total N	SUM	5	3
15	PO4	SUM	5	3
15	Organic P	SUM	5	3
15	Total P	SUM	5	3
15	BOD	SUM	5	3
15	TOC	SUM	5	3
16	NH3	SUM	5	3
16	NO3	SUM	5	3
16	Organic N	SUM	5	3
16	Total N	SUM	5	3
16	PO4	SUM	5	3
16	Organic P	SUM	5	3
16	Total P	SUM	5	3
16	BOD	SUM	5	3
16	TOC	SUM	5	3
21	NH3	SUM	5	3
21	NO3	SUM	5	3
21	Organic N	SUM	5	3

21	Total N	SUM	5	3
21	PO4	SUM	5	3
21	Organic P	SUM	5	3
21	Total P	SUM	5	3
21	BOD	SUM	5	3
21	TOC	SUM	5	3
23	NH3	SUM	5	3
23	NO3	SUM	5	3
23	Organic N	SUM	5	3
23	Total N	SUM	5	3
23	PO4	SUM	5	3
23	Organic P	SUM	5	3
23	Total P	SUM	5	3
23	BOD	SUM	5	3
23	TOC	SUM	5	3
25	NH3	SUM	5	3
25	NO3	SUM	5	3
25	Organic N	SUM	5	3
25	Total N	SUM	5	3
25	PO4	SUM	5	3
25	Organic P	SUM	5	3
25	Total P	SUM	5	3
25	BOD	SUM	5	3
25	TOC	SUM	5	3
26	NH3	SUM	5	3
26	NO3	SUM	5	3
26	Organic N	SUM	5	3
26	Total N	SUM	5	3
26	PO4	SUM	5	3
26	Organic P	SUM	5	3
26	Total P	SUM	5	3
26	BOD	SUM	5	3
26	TOC	SUM	5	3
100	DO-Inflow	SUM	4	2
100	DO-Reaeration	SUM	4	2
100	DO-BOD Decay	SUM	4	2
100	DO-Benthal demand	SUM	4	2
100	DO-Nitrification	SUM	4	2
100	DO-Phyto. growth	SUM	4	2
100	BOD-Inflow	SUM	4	2
100	BOD-Decay	SUM	4	2
100	BOD-Benthal release	SUM	4	2
100	BOD-Sink	SUM	4	2
100	BOD-Denitrification	SUM	4	2
100	BOD-Phyto. death	SUM	4	2
100	NH3-Inflow	SUM	4	2
100	NH3-Nitrification	SUM	4	2
100	NH3-Volatilization	SUM	4	2
100	NH3-Benthal release	SUM	4	2
100	NH3-BOD Decay	SUM	4	2
100	NH3-Phyto. growth	SUM	4	2
100	NO3-Inflow	SUM	4	2
100	NO3-Nitrification	SUM	4	2
100	NO3-Denitrification	SUM	4	2
100	NO3-BOD Decay	SUM	4	2

```

100    NO3-Phyto. growth    SUM    4    2
100    PO4-Inflow          SUM    4    2
100    PO4-Benthal release SUM    4    2
100    PO4-BOD Decay       SUM    4    2
100    PO4-Phyto. growth   SUM    4    2
100    PHY-Inflow         SUM    4    2
100    PHY-Sink           SUM    4    2
100    PHY-Death          SUM    4    2
100    PHY-Growth         SUM    4    2
100    ORN-Inflow         SUM    4    2
100    ORN-Sink           SUM    4    2
100    ORN-Phyto. death   SUM    4    2
100    ORP-Inflow         SUM    4    2
100    ORP-Sink           SUM    4    2
100    ORP-Phyto. death   SUM    4    2
100    ORC-Inflow         SUM    4    2
100    ORC-Sink           SUM    4    2
100    ORC-Phyto. death   SUM    4    2
END REPORT-CON

```

REPORT-SUMM

Rept-opn\*\*\*

```

*** x - x<--src-sum-header--> STRN <--tim-sum-header--> TTRN STTR
  1      Total Load          SUM Average          AVER    1
  3      Total Load          SUM Average          AVER    1
  5      Total Load          SUM Average          AVER    1
  6      Total Load          SUM Average          AVER    1
 11      Per acre Load       SUM Average          AVER    1
 13      Per acre Load       SUM Average          AVER    1
 15      Per acre Load       SUM Average          AVER    1
 16      Per acre Load       SUM Average          AVER    1
 21      Percent Load        PCT Average          AVER    1
 23      Percent Load        PCT Average          AVER    1
 25      Percent Load        PCT Average          AVER    1
 26      Percent Load        PCT Average          AVER    1
100                                SUM Average          AVER    1

```

END REPORT-SUMM

END REPORT

PERLND

ACTIVITY

```

<PLS >                Active Sections                ***
x - x ATMP SNOW PWAT  SED  PST  PWG PQAL MSTL PEST NITR PHOS TRAC ***
11  65  1          1      1  1  1  1
END ACTIVITY

```

PRINT-INFO

```

<PLS> ***** Print-flags ***** PIVL  PYR
x - x ATMP SNOW PWAT  SED  PST  PWG PQAL MSTL PEST NITR PHOS TRAC *****
11  65  5          5      5  5  5
END PRINT-INFO

```

GEN-INFO

<PLS >		Name	Unit-systems		Printer***
x	-	x	t-series		Engl Metr***
			in	out	***
11		AGRICULTURE- CENTRAL	1	1	90
12		FOREST- CENTRAL	1	1	90
13		RANGELAND	1	1	90
14		URBAN	1	1	90
15		WETLAND	1	1	90
16		WETLAND-AQ Q RCH 4,6	1	1	90
17		WETLAND-AQ Q RCH 14	1	1	90
18		WETLAND-AQ Q 8,15,16	1	1	90
19		RIBS	1	1	90
31		AGRICULTURE- UPPER RC	1	1	90
32		FOREST	1	1	90
33		RANGELAND	1	1	90
34		URBAN	1	1	90
35		WETLAND	1	1	90
39		RIBS	1	1	90
51		AGRICULTURE- WHIT	1	1	90
52		FOREST	1	1	90
53		RANGELAND	1	1	90
54		URBAN	1	1	90
55		WETLAND	1	1	90
59		RIBS	1	1	90
61		AGRICULTURE- DAV	1	1	90
62		FOREST	1	1	90
63		RANGELAND	1	1	90
64		URBAN	1	1	90
65		WETLAND	1	1	90

END GEN-INFO

PWAT-PARM1

*** <PLS >		Flags											
*** x	-	x	CSNO	RTOP	UZFG	VCS	VUZ	VNN	VIFW	VIRC	VLE	IFFC	HWT
11			0	1	1	0	0	0	0	0	1	0	0
12			0	1	1	0	0	0	0	0	1	0	0
13			0	1	1	0	0	0	0	0	1	0	0
14			0	1	1	0	0	0	0	0	1	0	0
15			0	1	1	0	0	0	0	0	1	0	0
16			0	1	1	0	0	0	0	0	1	0	0
17			0	1	1	0	0	0	0	0	1	0	0
18			0	1	1	0	0	0	0	0	1	0	0
19			0	1	1	0	0	0	0	0	0	0	0
31			0	1	1	0	0	0	0	0	1	0	0
32			0	1	1	0	0	0	0	0	1	0	0
33			0	1	1	0	0	0	0	0	1	0	0
34			0	1	1	0	0	0	0	0	1	0	0
35			0	1	1	0	0	0	0	0	1	0	0
39			0	1	1	0	0	0	0	0	0	0	0
51			0	1	1	0	0	0	0	0	1	0	0
52			0	1	1	0	0	0	0	0	1	0	0
53			0	1	1	0	0	0	0	0	1	0	0
54			0	1	1	0	0	0	0	0	1	0	0
55			0	1	1	0	0	0	0	0	1	0	0

59	0	1	1	0	0	0	0	0	0	0	0
61	0	1	1	0	0	0	0	0	1	0	0
62	0	1	1	0	0	0	0	0	1	0	0
63	0	1	1	0	0	0	0	0	1	0	0
64	0	1	1	0	0	0	0	0	1	0	0
65	0	1	1	0	0	0	0	0	1	0	0

END PWAT-PARM1

PWAT-PARM2

*** <PLS>	FOREST	LZSN	INFILT	LSUR	SLSUR	KVARY	AGWRC
*** x - x		(in)	(in/hr)	(ft)	(ft/ft)	(1/in)	(1/day)
11	0.0	2.000	0.100	1252.9	0.008	0.000	0.970
12	0.0	2.000	0.250	855.2	0.005	0.000	0.970
13	0.0	2.000	0.250	1182.0	0.011	0.000	0.970
14	0.0	2.000	0.070	1144.8	0.007	0.000	0.970
15	0.0	1.500	0.250	943.8	0.004	0.000	0.970
16	0.0	1.500	0.250	943.8	0.004	0.000	0.970
17	0.0	1.500	0.250	943.8	0.004	0.000	0.970
18	0.0	1.500	0.250	943.8	0.004	0.000	0.970
19	0.0	2.000	0.250	100.0	0.001	0.000	0.970
31	0.0	2.000	0.200	795.3	0.014	0.000	0.970
32	0.0	2.000	0.250	1372.0	0.028	0.000	0.970
33	0.0	2.000	0.250	1147.1	0.020	0.000	0.970
34	0.0	2.000	0.070	1223.6	0.016	0.000	0.970
35	0.0	1.500	0.250	690.7	0.004	0.000	0.970
39	0.0	2.000	0.250	100.0	0.001	0.000	0.970
51	0.0	2.000	0.200	481.9	0.013	0.000	0.970
52	0.0	2.000	0.250	433.0	0.026	0.000	0.970
53	0.0	2.000	0.250	1937.8	0.028	0.000	0.970
54	0.0	2.000	0.070	1311.2	0.031	0.000	0.970
55	0.0	1.500	0.250	510.7	0.004	0.000	0.970
59	0.0	2.000	0.250	100.0	0.001	0.000	0.970
61	0.0	2.000	0.100	792.0	0.016	0.000	0.970
62	0.0	2.000	0.250	318.6	0.016	0.000	0.970
63	0.0	2.000	0.250	847.8	0.015	0.000	0.970
64	0.0	2.000	0.070	642.1	0.010	0.000	0.970
65	0.0	1.500	0.250	662.2	0.005	0.000	0.970

END PWAT-PARM2

PWAT-PARM3

*** <PLS>	PETMAX	PETMIN	INFEXP	INFILD	DEEPPFR	BASETP	AGWETP
*** x - x	(deg F)	(deg F)					
11	40.0	35.0	2.0	2.0	0.500	0.000	0.000
12	40.0	35.0	2.0	2.0	0.500	0.000	0.000
13	40.0	35.0	2.0	2.0	0.500	0.000	0.000
14	40.0	35.0	2.0	2.0	0.500	0.000	0.000
15	40.0	35.0	2.0	2.0	0.400	0.000	0.100
16	40.0	35.0	2.0	2.0	0.400	0.000	0.100
17	40.0	35.0	2.0	2.0	0.400	0.000	0.100
18	40.0	35.0	2.0	2.0	0.400	0.000	0.100
19	40.0	35.0	2.0	2.0	0.500	0.000	0.000
31	40.0	35.0	2.0	2.0	0.500	0.000	0.000
32	40.0	35.0	2.0	2.0	0.500	0.000	0.000
33	40.0	35.0	2.0	2.0	0.500	0.000	0.000
34	40.0	35.0	2.0	2.0	0.500	0.000	0.000

35	40.0	35.0	2.0	2.0	0.400	0.000	0.100
39	40.0	35.0	2.0	2.0	0.500	0.000	0.000
51	40.0	35.0	2.0	2.0	0.500	0.000	0.000
52	40.0	35.0	2.0	2.0	0.500	0.000	0.000
53	40.0	35.0	2.0	2.0	0.500	0.000	0.000
54	40.0	35.0	2.0	2.0	0.500	0.000	0.000
55	40.0	35.0	2.0	2.0	0.400	0.000	0.100
59	40.0	35.0	2.0	2.0	0.500	0.000	0.000
61	40.0	35.0	2.0	2.0	0.500	0.000	0.000
62	40.0	35.0	2.0	2.0	0.500	0.000	0.000
63	40.0	35.0	2.0	2.0	0.500	0.000	0.000
64	40.0	35.0	2.0	2.0	0.500	0.000	0.000
65	40.0	35.0	2.0	2.0	0.400	0.000	0.100

END PWAT-PARM3

PWAT-PARM4

*** <PLS >	CEPSC	UZSN	NSUR	INTFW	IRC	LZETP
*** x - x	(in)	(in)			(1/day)	
11	0.080	0.200	0.20	0.500	0.800	0.600
12	0.100	0.560	0.35	0.600	0.800	0.600
13	0.050	0.320	0.15	0.500	0.800	0.600
14	0.050	0.320	0.10	0.500	0.800	0.600
15	0.200	0.350	0.35	0.700	0.800	0.600
16	0.200	0.350	0.35	0.700	0.800	0.600
17	0.200	0.350	0.35	0.700	0.800	0.600
18	0.200	0.350	0.35	0.700	0.800	0.600
19	0.000	0.700	0.10	0.600	0.800	0.500
31	0.080	0.200	0.20	1.000	0.900	0.600
32	0.100	0.560	0.35	1.000	0.900	0.600
33	0.050	0.320	0.15	1.000	0.900	0.600
34	0.050	0.320	0.10	1.000	0.900	0.600
35	0.200	0.350	0.35	1.000	0.900	0.600
39	0.000	0.700	0.10	1.000	0.900	0.500
51	0.080	0.200	0.20	1.000	0.900	0.600
52	0.100	0.560	0.35	1.000	0.900	0.600
53	0.050	0.320	0.15	1.000	0.900	0.600
54	0.050	0.320	0.10	1.000	0.900	0.600
55	0.200	0.350	0.35	1.000	0.900	0.600
59	0.000	0.700	0.10	1.000	0.900	0.500
61	0.080	0.200	0.20	0.500	0.800	0.600
62	0.100	0.560	0.35	0.600	0.800	0.600
63	0.050	0.320	0.15	0.500	0.800	0.600
64	0.050	0.320	0.10	0.500	0.800	0.600
65	0.200	0.350	0.35	0.700	0.800	0.600

END PWAT-PARM4

MON-LZETPARM

*** <PLS >	Lower zone evapotransp parameter at start of each month												
11	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
12	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
13	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
14	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
15	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
16	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
17	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5

18	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
31	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
32	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
33	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
34	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
35	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
51	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
52	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
53	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
54	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
55	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
61	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
62	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
63	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
64	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
65	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5

END MON-LZETPARM

PWAT-STATE1

\*\*\* <PLS> PWATER state variables (in)

*** x - x	CEPS	SURS	UZS	IFWS	LZS	AGWS	GWVS
11	0.0	0.0	0.408	0.001	3.21	0.712	0.0
12	0.0	0.0	0.778	0.001	3.09	0.704	0.0
13	0.0	0.0	0.407	0.001	2.95	0.734	0.0
14	0.0	0.0	0.405	0.001	2.74	0.49	0.0
15	0.0	0.0	0.582	0.001	2.35	0.749	0.0
16	0.0	0.0	0.582	0.001	2.35	0.749	0.0
17	0.0	0.0	0.582	0.001	2.35	0.749	0.0
18	0.0	0.0	0.582	0.001	2.35	0.749	0.0
19	0.0	0.0	0.703	0.001	2.6	0.974	0.0
31	0.0	0.0	0.401	0.001	3.38	0.818	0.0
32	0.0	0.0	0.886	0.001	3.28	0.683	0.0
33	0.0	0.0	0.407	0.001	3	0.715	0.0
34	0.0	0.0	0.514	0.001	2.84	0.455	0.0
35	0.0	0.0	0.661	0.001	2.55	0.721	0.0
39	0.0	0.0	0.724	0.001	2.68	1.013	0.0
51	0.0	0.0	0.04	0.001	1.70	0.18	0.0
52	0.0	0.0	0.03	0.001	0.40	0.09	0.0
53	0.0	0.0	0.01	0.001	0.33	0.09	0.0
54	0.0	0.0	0.01	0.001	0.37	0.07	0.0
55	0.0	0.0	0.02	0.001	0.32	0.02	0.0
59	0.0	0.0	0.02	0.001	0.81	0.17	0.0
61	0.0	0.0	0.407	0.001	3.20	0.707	0.0
62	0.0	0.0	0.858	0.001	3.19	0.785	0.0
63	0.0	0.0	0.442	0.001	3.03	0.825	0.0
64	0.0	0.0	0.502	0.001	2.75	0.489	0.0
65	0.0	0.0	0.618	0.001	2.45	0.861	0.0

END PWAT-STATE1



PSTEMP-PARM1

\*\*\* <PLS > Flags for section PSTEMP

\*\*\* x - x SLTV ULTV LGTV TSOP

11	1	1	1	1
12	1	1	1	1
13	1	1	1	1
14	1	1	1	1
15	1	1	1	1
16	1	1	1	1
17	1	1	1	1
18	1	1	1	1
19	1	1	1	1
31	1	1	1	1
32	1	1	1	1
33	1	1	1	1
34	1	1	1	1
35	1	1	1	1
39	1	1	1	1
51	1	1	1	1
52	1	1	1	1
53	1	1	1	1
54	1	1	1	1
55	1	1	1	1
59	1	1	1	1
61	1	1	1	1
62	1	1	1	1
63	1	1	1	1
64	1	1	1	1
65	1	1	1	1

END PSTEMP-PARM1

PSTEMP-PARM2

\*\*\* <PLS > ASLT BSLT ULTP1 ULTP2 LGTP1 LGTP2  
\*\*\* x - x (deg F) (degF/F) (degF/F) (deg F)

11	32.0	1.00	32.0	1.0	60.8
12	32.0	1.00	32.0	1.0	60.8
13	32.0	1.00	32.0	1.0	60.8
14	32.0	1.00	32.0	1.0	60.8
15	32.0	1.00	32.0	1.0	60.8
16	32.0	1.00	32.0	1.0	60.8
17	32.0	1.00	32.0	1.0	60.8
18	32.0	1.00	32.0	1.0	60.8
19	32.0	1.00	32.0	1.0	60.8
31	32.0	1.00	32.0	1.0	60.8
32	32.0	1.00	32.0	1.0	60.8
33	32.0	1.00	32.0	1.0	60.8
34	32.0	1.00	32.0	1.0	60.8
35	32.0	1.00	32.0	1.0	60.8
39	32.0	1.00	32.0	1.0	60.8
51	32.0	1.00	32.0	1.0	60.8
52	32.0	1.00	32.0	1.0	60.8
53	32.0	1.00	32.0	1.0	60.8
54	32.0	1.00	32.0	1.0	60.8
55	32.0	1.00	32.0	1.0	60.8
59	32.0	1.00	32.0	1.0	60.8

61	32.0	1.00	32.0	1.0	60.8
62	32.0	1.00	32.0	1.0	60.8
63	32.0	1.00	32.0	1.0	60.8
64	32.0	1.00	32.0	1.0	60.8
65	32.0	1.00	32.0	1.0	60.8

END PSTEMP-PARM2

MON-ASLT

\*\*\* <PLS > Value of ASLT at start of each month (deg F)

*** x - x	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
12	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
13	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
14	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
15	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
16	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
17	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
18	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
19	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
31	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
32	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
33	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
34	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
35	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
39	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
51	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
52	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
53	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
54	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
55	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
59	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
61	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
62	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
63	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
64	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
65	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0

END MON-ASLT

MON-BSLT

\*\*\* <PLS > Value of BSLT at start of each month (deg F/F)

*** x - x	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
12	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
13	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
14	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
15	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
16	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
17	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
18	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
19	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
31	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60

32	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
33	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
34	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
35	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
39	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
51	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
52	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
53	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
54	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
55	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
59	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
61	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
62	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
63	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
64	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
65	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55

END MON-BSLT

MON-ULTP1

\*\*\* <PLS > Value of ULTP1 at start of each month in deg F (TSOPFG=1)

*** x - x	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
12	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
13	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
14	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
15	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
16	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
17	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
18	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
19	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
31	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
32	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
33	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
34	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
35	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
39	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
51	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
52	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
53	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
54	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
55	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
59	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
61	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
62	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
63	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
64	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
65	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0

END MON-ULTP1

MON-ULTP2

\*\*\* <PLS > Value of ULTP2 at start of each month in Deg F/F (TSOPFG=1)

\*\*\* x - x

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
12	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
13	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
14	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
15	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
16	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
17	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
18	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
19	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
31	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
32	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
33	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
34	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
35	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
39	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
51	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
52	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
53	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
54	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
55	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
59	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
61	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
62	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
63	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
64	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
65	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25

END MON-ULTP2

MON-LGTP1

\*\*\* <PLS > Value of LGTP1 at start of each month in Deg F (TSOPFG=1)

\*\*\* x - x

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
12	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
13	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
14	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
15	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
16	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
17	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
18	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
19	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
31	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
32	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
33	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
34	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
35	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
39	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0

51	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
52	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
53	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
54	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
55	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
59	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0

61	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
62	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
63	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
64	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
65	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0

END MON-LGTP1

PSTEMP-TEMPS

<PLS> Initial Conditions for Section PSTEMP \*\*\*

#	#	AIRTC	SLTMP	ULTMP	LGTMP	***
1	65	56.0	56.0	56.0	68.0	

END PSTEMP-TEMPS

PWT-PARM1

<PLS> Flags for Section PWTGAS \*\*\*

#	#	IDV	ICV	GDV	GCV	***
11		1	0	1	0	
12		1	0	1	0	
13		1	0	1	0	
14		1	0	1	0	
15		1	0	1	0	
16		1	0	1	0	
17		1	0	1	0	
18		1	0	1	0	
19		1	0	1	0	
31		1	0	1	0	
32		1	0	1	0	
33		1	0	1	0	
34		1	0	1	0	
35		1	0	1	0	
39		1	0	1	0	
51		1	0	1	0	
52		1	0	1	0	
53		1	0	1	0	
54		1	0	1	0	
55		1	0	1	0	
59		1	0	1	0	
61		1	0	1	0	
62		1	0	1	0	
63		1	0	1	0	
64		1	0	1	0	
65		1	0	1	0	

END PWT-PARM1

PWT-PARM2

#	#	ELEV	IDOXP	ICO2P	ADOXP	ACO2P	***
11		80.00	6	0.00	4	0.00	
12		80.00	6	0.00	4	0.00	
13		80.00	6	0.00	4	0.00	
14		80.00	6	0.00	4	0.00	
15		80.00	6	0.00	4	0.00	
16		80.00	6	0.00	4	0.00	
17		80.00	6	0.00	4	0.00	
18		80.00	6	0.00	4	0.00	
19		80.00	6	0.00	4	0.00	
31		120.00	6	0.00	4	0.00	
32		120.00	6	0.00	4	0.00	
33		120.00	6	0.00	4	0.00	
34		120.00	6	0.00	4	0.00	
35		120.00	6	0.00	4	0.00	
39		120.00	6	0.00	4	0.00	
51		110.00	6	0.00	4	0.00	
52		110.00	6	0.00	4	0.00	
53		110.00	6	0.00	4	0.00	
54		110.00	6	0.00	4	0.00	
55		110.00	6	0.00	4	0.00	
59		110.00	6	0.00	4	0.00	
61		100.00	6	0.00	4	0.00	
62		100.00	6	0.00	4	0.00	
63		100.00	6	0.00	4	0.00	
64		100.00	6	0.00	4	0.00	
65		100.00	6	0.00	4	0.00	

END PWT-PARM2

MON-IFWDOX

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11	65	8.0	8.0	7.5	7.0	6.5	6.0	6.0	6.0	6.5	7.0	7.5	8.0	

END MON-IFWDOX

MON-GRNDDOX

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11	65	6.0	6.0	5.5	5.0	4.0	4.0	4.0	4.0	4.5	5.0	5.5	6.0	

END MON-GRNDDOX

PWT-GASES

#	#	SODOX	SOCO2	IODOX	IOCO2	AODOX	AOCO2	***
1	65	10.0	0.0	8.0	0.0	6.0	0.0	

END PWT-GASES

NQUALS

\*\*\* NQAL - NH3, NO2+NO3, ORTHO P, AND BOD \*\*\*

#	#	NQAL	***
1	65	4	

END NQUALS

PQL-AD-FLAGS

Atmospheric Deposition Flags \*\*\*

<PLS >		QUAL1		QUAL2		QUAL3		QUAL4		***
#	- #	F	C	F	C	F	C	F	C	***
11		-1	0	-1	0	0	0	0	0	
12		-1	0	-1	0	0	0	0	0	
13		-1	0	-1	0	0	0	0	0	
14		-1	0	-1	0	0	0	0	0	
15		-1	0	-1	0	0	0	0	0	
16		-1	0	-1	0	0	0	0	0	
17		-1	0	-1	0	0	0	0	0	
18		-1	0	-1	0	0	0	0	0	
19		-1	0	-1	0	0	0	0	0	
31		-1	0	-1	0	0	0	0	0	
32		-1	0	-1	0	0	0	0	0	
33		-1	0	-1	0	0	0	0	0	
34		-1	0	-1	0	0	0	0	0	
35		-1	0	-1	0	0	0	0	0	
39		-1	0	-1	0	0	0	0	0	
51		-1	0	-1	0	0	0	0	0	
52		-1	0	-1	0	0	0	0	0	
53		-1	0	-1	0	0	0	0	0	
54		-1	0	-1	0	0	0	0	0	
55		-1	0	-1	0	0	0	0	0	
59		-1	0	-1	0	0	0	0	0	
61		-1	0	-1	0	0	0	0	0	
62		-1	0	-1	0	0	0	0	0	
63		-1	0	-1	0	0	0	0	0	
64		-1	0	-1	0	0	0	0	0	
65		-1	0	-1	0	0	0	0	0	

END PQL-AD-FLAGS

QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	NH3	LBS	0	0	0	1	1	1	3	1	3	
12	NH3	LBS	0	0	0	1	1	1	3	1	3	
13	NH3	LBS	0	0	0	1	1	1	3	1	3	
14	NH3	LBS	0	0	0	1	1	1	3	1	3	
15	NH3	LBS	0	0	0	1	1	1	3	1	3	
16	NH3	LBS	0	0	0	1	1	1	3	1	3	
17	NH3	LBS	0	0	0	1	1	1	3	1	3	
18	NH3	LBS	0	0	0	1	1	1	3	1	3	
19	NH3	LBS	0	0	0	1	1	1	3	1	3	
31	NH3	LBS	0	0	0	1	1	1	3	1	3	
32	NH3	LBS	0	0	0	1	1	1	3	1	3	
33	NH3	LBS	0	0	0	1	1	1	3	1	3	
34	NH3	LBS	0	0	0	1	1	1	3	1	3	
35	NH3	LBS	0	0	0	1	1	1	3	1	3	
39	NH3	LBS	0	0	0	1	1	1	3	1	3	
51	NH3	LBS	0	0	0	1	1	1	3	1	3	
52	NH3	LBS	0	0	0	1	1	1	3	1	3	
53	NH3	LBS	0	0	0	1	1	1	3	1	3	
54	NH3	LBS	0	0	0	1	1	1	3	1	3	
55	NH3	LBS	0	0	0	1	1	1	3	1	3	
59	NH3	LBS	0	0	0	1	1	1	3	1	3	

61	NH3	LBS	0	0	0	1	1	1	3	1	3
62	NH3	LBS	0	0	0	1	1	1	3	1	3
63	NH3	LBS	0	0	0	1	1	1	3	1	3
64	NH3	LBS	0	0	0	1	1	1	3	1	3
65	NH3	LBS	0	0	0	1	1	1	3	1	3

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.004				.012	0.5			
12		.002				.004	0.5			
13		.004				.012	0.5			
14		.004				.012	0.5			
15		.002				.004	0.5			
16		.002				.004	0.5			
17		.002				.004	0.5			
18		.002				.004	0.5			
19		.004				.012	0.5			
31		.004				.012	0.5			
32		.002				.004	0.5			
33		.004				.012	0.5			
34		.004				.012	0.5			
35		.002				.004	0.5			
39		.004				.012	0.5			
51		.004				.012	0.5			
52		.002				.004	0.5			
53		.004				.012	0.5			
54		.004				.012	0.5			
55		.002				.004	0.5			
59		.004				.012	0.5			
61		.004				.012	0.5			
62		.002				.004	0.5			
63		.004				.012	0.5			
64		.004				.012	0.5			
65		.002				.004	0.5			

END QUAL-INPUT

MON-ACCUM

ACCUMULATION RATE OF NH4 (lb NH4-N/AC.DAY)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
12		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
13		.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	
14		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
15	18	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
19		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
31		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
32		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
33		.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	
34		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
35		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	



39	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
51	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
52	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
53	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
54	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008
55	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
59	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
61	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
62	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
63	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
64	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008
65	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002

END MON-ACCUM

MON-SQOLIM

STORAGE LIMIT OF NH4 (lb NH4-N/AC)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
12		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
13		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
14		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
15	18	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
19		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
31		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
32		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
33		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
34		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
35		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
39		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
51		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
52		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
53		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
54		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
55		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
59		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
61		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
62		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
63		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
64		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
65		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	

END MON-SQOLIM

MON-IFLW-CONC

		Interflow Concentration of NH4-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
12		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
13		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
14		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
15	18	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
19		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
31		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
32		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
33		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
34		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
35		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
39		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
51		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
52		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
53		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
54		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
55		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
59		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
61		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
62		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
63		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
64		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
65		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	

END MON-IFLW-CONC

MON-GRND-CONC

		Active Groundwater Concentration of NH4-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
12		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
13		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
14		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
15	18	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
19		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
31		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
32		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
33		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
34		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
35		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
39		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
51		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
52		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
53		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
54		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
55		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
59		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	

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61      .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100
62      .020 .020 .020 .020 .020 .020 .020 .020 .020 .020 .020 .020
63      .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100
64      .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100
65      .030 .030 .030 .030 .030 .030 .030 .030 .030 .030 .030 .030
END MON-GRND-CONC

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QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
12	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
13	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
14	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
15	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
16	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
17	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
18	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
19	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
31	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
32	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
33	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
34	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
35	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
39	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
51	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
52	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
53	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
54	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
55	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
59	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
61	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
62	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
63	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
64	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
65	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.040				.120	.5			
12		.005				.010	.5			
13		.040				.120	.5			
14		.040				.120	.5			
15	18	.005				.010	.5			
19		.040				.120	.5			
31		.040				.120	.5			
32		.005				.010	.5			
33		.040				.120	.5			
34		.040				.120	.5			
35		.005				.010	.5			
39		.040				.120	.5			

51	.040	.480	.5
52	.005	.100	.5
53	.040	.480	.5
54	.040	.480	.5
55	.005	.100	.5
59	.040	.480	.5
61	.040	.480	.5
62	.005	.100	.5
63	.040	.480	.5
64	.040	.480	.5
65	.005	.100	.5

END QUAL-INPUT

MON-ACCUM

		ACCUMULATION RATE												NO2 NO3 (lb NO3-N/AC.DAY)		***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***			
11		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1			
12		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050			
13		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05			
14		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03			
15	180	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020			
19		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01			
31		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1			
32		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050			
33		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05			
34		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03			
35		0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020			
39		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01			
51		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1			
52		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050			
53		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05			
54		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03			
55		0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020			
59		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01			
61		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1			
62		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050			
63		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05			
64		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03			
65		0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020			

END MON-ACCUM

MON-SQOLIM

		STORAGE LIMIT OF												NO2 NO3 (lb NO3-N/AC)		***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***			
11		0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20			
12		.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010			
13		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10			
14		0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06			
15	18	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004			
19		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020			

31	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
32	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010
33	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
34	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
35	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
39	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
51	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
52	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010
53	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
54	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
55	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
59	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
61	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
62	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010
63	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
64	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
65	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004

END MON-SQOLIM

MON-IFLW-CONC

		Interflow Concentration of NO3-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
12		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
13		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
14		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
15	18	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	
19		5	5	5	5	5	5	5	5	5	5	5	5	
31		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
32		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
33		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
34		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
39		5	5	5	5	5	5	5	5	5	5	5	5	
51		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
52		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
53		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
54		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
59		5	5	5	5	5	5	5	5	5	5	5	5	
61		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
62		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
63		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
64		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
65		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	

END MON-IFLW-CONC

MON-GRND-CONC

		Active Groundwater Concentration of NO3-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
12		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
13		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
14		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
15		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
16		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
17		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
18		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
19		5	5	5	5	5	5	5	5	5	5	5	5	
31		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
32		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
33		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
34		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
39		5	5	5	5	5	5	5	5	5	5	5	5	
51		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
52		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
53		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
54		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
59		5	5	5	5	5	5	5	5	5	5	5	5	
61		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
62		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
63		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
64		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
65		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	

END MON-GRND-CONC

QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
12	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
13	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
14	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
15	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
16	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
17	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
18	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
19	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
31	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
32	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
33	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
34	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
35	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
39	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	

51	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
52	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
53	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
54	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
55	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
59	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
61	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
62	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
63	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
64	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
65	ORTHO P	LBS	0	0	0	1	1	1	3	1	3

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.004				.012	.5			
12		.002				.004	.5			
13		.004				.012	.5			
14		.004				.012	.5			
15	18	.002				.004	.5			
19		.004				.012	.5			
31		.004				.012	.5			
32		.002				.004	.5			
33		.004				.012	.5			
34		.004				.012	.5			
35		.002				.004	.5			
39		.004				.012	.5			
51		.004				.012	.5			
52		.002				.004	.5			
53		.004				.012	.5			
54		.004				.012	.5			
55		.002				.004	.5			
59		.004				.012	.5			
61		.004				.012	.5			
62		.002				.004	.5			
63		.004				.012	.5			
64		.004				.012	.5			
65		.002				.004	.5			

END QUAL-INPUT

MON-ACCUM

ACCUMULATION RATE OF PO4 (lb PO4-P/AC.DAY)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
12		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
13		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
14		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
15	18	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
19		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	

31	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
32	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
33	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
34	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
35	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
39	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
51	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
52	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
53	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
54	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
55	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
59	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
61	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
62	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
63	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
64	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
65	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002

END MON-ACCUM

MON-SQOLIM

STORAGE LIMIT OF PO4 (lb PO4-P/AC)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
12		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
13		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
14		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
15	18	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
19		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
31		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
32		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
33		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
34		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
35		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
39		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
51		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
52		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
53		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
54		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
55		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
59		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
61		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
62		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
63		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
64		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
65		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	

END MON-SQOLIM



MON-IFLW-CONC

Interflow Concentration of PO4-P (mg/l)

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#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
12		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
13		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
14		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
15	18	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
19		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
31		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
32		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
33		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
34		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
39		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
51		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
52		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
53		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
54		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
59		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
61		0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
62		0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120
63		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050
64		0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08
65		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050

\*\*\*

END MON-IFLW-CONC

MON-GRND-CONC

Active Groundwater Concentration of PO4-P (mg/l)

\*\*\*

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
12		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
13		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
14		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
15	18	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
19		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
31		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
32		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
33		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
34		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
39		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
51		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
52		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
53		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
54		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
59		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01

\*\*\*

61 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06  
 62 0.0120.0120.0120.0120.0120.0120.0120.0120.0120.0120.0120.0120.012  
 63 0.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.005  
 64 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08  
 65 0.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.005  
 END MON-GRND-CONC

QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	BOD	LBS	0	0	0	1	1	1	3	1	3	
12	BOD	LBS	0	0	0	1	1	1	3	1	3	
13	BOD	LBS	0	0	0	1	1	1	3	1	3	
14	BOD	LBS	0	0	0	1	1	1	3	1	3	
15	BOD	LBS	0	0	0	1	1	1	3	1	3	
16	BOD	LBS	0	0	0	1	1	1	3	1	3	
17	BOD	LBS	0	0	0	1	1	1	3	1	3	
18	BOD	LBS	0	0	0	1	1	1	3	1	3	
19	BOD	LBS	0	0	0	1	1	1	3	1	3	
31	BOD	LBS	0	0	0	1	1	1	3	1	3	
32	BOD	LBS	0	0	0	1	1	1	3	1	3	
33	BOD	LBS	0	0	0	1	1	1	3	1	3	
34	BOD	LBS	0	0	0	1	1	1	3	1	3	
35	BOD	LBS	0	0	0	1	1	1	3	1	3	
39	BOD	LBS	0	0	0	1	1	1	3	1	3	
51	BOD	LBS	0	0	0	1	1	1	3	1	3	
52	BOD	LBS	0	0	0	1	1	1	3	1	3	
53	BOD	LBS	0	0	0	1	1	1	3	1	3	
54	BOD	LBS	0	0	0	1	1	1	3	1	3	
55	BOD	LBS	0	0	0	1	1	1	3	1	3	
59	BOD	LBS	0	0	0	1	1	1	3	1	3	
61	BOD	LBS	0	0	0	1	1	1	3	1	3	
62	BOD	LBS	0	0	0	1	1	1	3	1	3	
63	BOD	LBS	0	0	0	1	1	1	3	1	3	
64	BOD	LBS	0	0	0	1	1	1	3	1	3	
65	BOD	LBS	0	0	0	1	1	1	3	1	3	

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.35				5.0	.5			
12		.15				.75	.5			
13		.35				5.0	.5			
14		.60				6.0	.5			
15	18	.15				1.5	.5			
19		.35				5.0	.5			
31		.35				5.0	.5			
32		.15				.75	.5			
33		.35				5.0	.5			
34		.60				6.0	.5			
35		.15				1.5	.5			
39		.35				5.0	.5			

51	.35	5.0	.5
52	.15	.75	.5
53	.35	5.0	.5
54	.60	6.0	.5
55	.15	1.5	.5
59	.35	5.0	.5
61	.35	5.0	.5
62	.15	.75	.5
63	.35	5.0	.5
64	.60	6.0	.5
65	.15	1.5	.5

END QUAL-INPUT

MON-ACCUM

ACCUMULATION RATE FOR BOD/Organics (lb /AC.DAY) ***														
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
12		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
13		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
14		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
15	18	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
19		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
31		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
32		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
33		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
34		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
35		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
39		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
51		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
52		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
53		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
54		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
55		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
59		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
61		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
62		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
63		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
64		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
65		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	

END MON-ACCUM

MON-SQOLIM

STORAGE RATE FOR BOD/Organics (lb /AC) ***														
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
12		.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	
13		0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	
14		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	
15	18	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	
19		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	

31	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
32	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45
33	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
34	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
35	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20
39	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
51	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
52	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45
53	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
54	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
55	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20
59	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
61	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
62	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45
63	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
64	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
65	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20

END MON-SQOLIM

MON-IFLW-CONC

#	#	Interflow Concentration of BOD/Organics (mg/l) ***												***
		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	
11		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
12		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
13		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
14		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
15	18	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
19		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
31		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
32		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
33		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
34		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
35		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
39		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
51		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
52		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
53		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
54		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
55		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
59		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
61		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
62		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
63		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
64		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
65		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	

END MON-IFLW-CONC

MON-GRND-CONC

Active Groundwater Concentration of BOD/Organics (mg/l) \*\*\*

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
12		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
13		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
14		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
15	18	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
19		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
31		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
32		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
33		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
34		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
35		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
39		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
51		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
52		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
53		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
54		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
55		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
59		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
61		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
62		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
63		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
64		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
65		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	

END MON-GRND-CONC

END PERLND

IMPLND

ACTIVITY

#	#	ATMP	SNOW	IWAT	SLD	IWG	IQAL	***
14	64	1	0	1	0	1	1	

END ACTIVITY

PRINT-INFO

#	#	ATMP	SNOW	IWAT	SLD	IWG	IQAL	PIVL	PYR	***
14	64	5	0	5	0	5	5	1	12	

END PRINT-INFO

GEN-INFO

***	<ILS >	Name	Unit-systems		Printer	
***	<ILS >		t-series	Engl	Metr	
***	x - x		in	out		
	14	URBAN	1	1	90	0
	34	URBAN	1	1	90	0
	54	URBAN	1	1	90	0
	64	URBAN	1	1	90	0

END GEN-INFO

```

IWAT-PARM1
*** <ILS >           Flags
*** x - x CSNO RTOP  VRS  VNN RTLI
    14          0    1    0    0    0
    34          0    1    0    0    0
    54          0    1    0    0    0
    64          0    1    0    0    0
END IWAT-PARM1

IWAT-PARM2
*** <ILS >           LRSUR           SLSUR           NSUR           RETSC
*** x - x           (ft)                (ft)
    14          200.0    0.01015    0.015    0.05
    34          200.0    0.01015    0.015    0.05
    54          200.0    0.01015    0.015    0.05
    64          200.0    0.01015    0.015    0.05
END IWAT-PARM2

IWAT-PARM3
*** <ILS >           PETMAX           PETMIN
*** x - x           (deg F)          (deg F)
    14  64          40.0            35.0
END IWAT-PARM3

IWAT-STATE1
*** <ILS >  IWATER state variables (inches)
*** x - x           RETS           SURS
    14  64          0.0            0.0
END IWAT-STATE1

IWT-PARM1
#    # WTFV CSNO  ***
14  64    1    0
END IWT-PARM1

IWT-PARM2
#    #           ELEV           AWTF           BWTF  ***
14          80.00           34.0           0.3
34          120.00          34.0           0.3
54          110.00          34.0           0.3
64          100.00          34.0           0.3
END IWT-PARM2

MON-AWTF
*** <ILS >  Values of AWTF at start of each month (oF)
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
    14  64 29.0 29.0 30.0 34.0 40.0 50.0 50.0 50.0 45.0 40.0 35.0 30.0
END MON-AWTF

MON-BWTF
*** <ILS >  Values of BWTF at start of each month (F/F)
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
    14  64 .55 .55 .60 .60 .65 .65 .65 .65 .60 .55 .55 .55
END MON-BWTF

```

NQUALS

```

# # NQAL ***
14 64 4
END NQUALS

```

IQL-AD-FLAGS

```

      Atmospheric Deposition Flags ***
<ILS > QUAL1  QUAL2  QUAL3  QUAL4  ***
# - #   F  C   F  C   F  C   F  C   ***
14      -1  0  -1  0   0  0   0  0
34      -1  0  -1  0   0  0   0  0
54      -1  0  -1  0   0  0   0  0
64      -1  0  -1  0   0  0   0  0
END IQL-AD-FLAGS

```

QUAL-PROPS

```

# #<---QUALID-->  QTID  QSD VPFW  QSO  VQO  ***
14  NH3              LBS    0    0    1    0
34  NH3              LBS    0    0    1    0
54  NH3              LBS    0    0    1    0
64  NH3              LBS    0    0    1    0
END QUAL-PROPS

```

QUAL-INPUT

```

# #      SQO  POTFW  ACQOP  SQOLIM  WSQOP  ***
14      0.001    0  0.004  0.005    0.5
34      0.001    0  0.004  0.005    0.5
54      0.001    0  0.004  0.005    0.5
64      0.001    0  0.004  0.005    0.5
END QUAL-INPUT

```

QUAL-PROPS

```

# #<---QUALID-->  QTID  QSD VPFW  QSO  VQO  ***
14  NO2 NO3          LBS    0    0    1    0
34  NO2 NO3          LBS    0    0    1    0
54  NO2 NO3          LBS    0    0    1    0
64  NO2 NO3          LBS    0    0    1    0
END QUAL-PROPS

```

QUAL-INPUT

```

# #      SQO  POTFW  ACQOP  SQOLIM  WSQOP  ***
14      0.007    0  0.006  0.009    0.5
34      0.007    0  0.006  0.009    0.5
54      0.007    0  0.006  0.009    0.5
64      0.007    0  0.006  0.009    0.5
END QUAL-INPUT

```

QUAL-PROPS

```

# #<---QUALID-->  QTID  QSD VPFW  QSO  VQO  ***
14  ORTHO P          LBS    0    0    1    0
34  ORTHO P          LBS    0    0    1    0
54  ORTHO P          LBS    0    0    1    0
64  ORTHO P          LBS    0    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
# # SQO POTFW ACQOP SQOLIM WSQOP ***
14 0.002 0 0.001 0.002 0.5
34 0.002 0 0.001 0.002 0.5
54 0.002 0 0.001 0.002 0.5
64 0.002 0 0.001 0.002 0.5
END QUAL-INPUT

```

```

QUAL-PROPS
# #<--QUALID--> QTID QSD VPFW QSO VQO ***
14 BOD LBS 0 0 1 0
34 BOD LBS 0 0 1 0
54 BOD LBS 0 0 1 0
64 BOD LBS 0 0 1 0
END QUAL-PROPS

```

```

QUAL-INPUT
# # SQO POTFW ACQOP SQOLIM WSQOP ***
14 1.0 0. 0.15 2.0 0.500
34 1.0 0. 0.15 2.0 0.500
54 1.0 0. 0.15 2.0 0.500
64 1.0 0. 0.15 2.0 0.500
END QUAL-INPUT
END IMPLND

```

```

RCHRES
ACTIVITY
*** RCHRES Active sections
*** x - x HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUGF PKFG PHFG
1 61 1 1 0 0 0 0 1 1 1 0
END ACTIVITY

```

```

PRINT-INFO
*** RCHRES Printout level flags
*** x - x HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR
1 61 5 5 5 5 5 1 12
END PRINT-INFO

```

```

GEN-INFO
***
*** RCHRES
*** x - x
Name Nexits Unit Systems Printer
t-series Engr Metr LKFG
in out
31 EAST UPPER REEDY CK 1 1 1 90 0 1
41 WEST UPPER REEDY CK 1 1 1 90 0 1
51 WHITTENHORSE CK 1 1 1 90 0 1
61 DAVENPORT CK 1 1 1 90 0 1
2 BAY LAKE / 7 SEAS 2 1 1 90 0 1
3 UPPER L-405 1 1 1 90 0 0
4 C-4 1 1 1 90 0 0
5 L-403 - EPCOT 1 1 1 90 0 0
6 LOWER L-405 1 1 1 90 0 0
7 REEDY CK AB HWY 192 1 1 1 90 0 0
8 REEDY CK AB I-4 1 1 1 90 0 0
9 L MABEL / SOUTH L 1 1 1 90 0 1
10 L-105 1 1 1 90 0 0

```



11	L-103	1	1	1	90	0	0
12	L-107 / UPPER C-1	1	1	1	90	0	0
13	MIDDLE C-1	1	1	1	90	0	0
14	LOWER C-1	1	1	1	90	0	0
15	REEDY CK AT S-40	2	1	1	90	0	0
16	REEDY CK AT LOUGHMAN	1	1	1	90	0	0

END GEN-INFO

HYDR-PARM1

```

***      Flags for HYDR section
RCHRES  VC A1 A2 A3  ODFVFG for each *** ODGTFG for each  FUNCT for each
x  -  x  FG FG FG FG  possible  exit *** possible  exit  possible  exit
          * * * * * * * * * * * * * * * * * * * * * * * * * * * *
2          0 1 1 1    4 5          0
3   14    0 1 1 1    4          0
15         0 1 1 1    0 4          1
16   61    0 1 1 1    4          0

```

END HYDR-PARM1

HYDR-PARM2

*** RCHRES	FTABNO	LEN	DELTH	STCOR	KS	DB50
*** x - x		(miles)	(ft)	(ft)		(in)
2	2	1.00	0.1	62.5	0.0	0.01
3	3	5.56	0.1	.0	0.0	0.01
4	4	2.13	0.1	.0	0.0	0.01
5	5	3.36	0.1	.0	0.0	0.01
6	6	2.50	0.1	.0	0.0	0.01
7	7	2.01	0.1	.0	0.0	0.01
8	8	2.52	0.1	.0	0.0	0.01
9	9	2.00	0.1	88.25	0.0	0.01
10	10	1.77	0.1	.0	0.0	0.01
11	11	2.92	0.1	.0	0.0	0.01
12	12	6.75	0.1	.0	0.0	0.01
13	13	2.37	0.1	.0	0.0	0.01
14	14	4.51	0.1	.0	0.0	0.01
15	15	2.84	0.1	.0	0.0	0.01
16	16	1.0	0.1	-0.73	0.0	0.01
31	31	1.0	0.1	90.0	0.0	0.01
41	41	1.2	0.1	90.0	0.0	0.01
51	51	2.37	0.1	90.77	0.0	0.01
61	61	4.64	0.1	4.0	0.0	0.01

END HYDR-PARM2

HYDR-INIT

```

***      Initial conditions for HYDR section
*** RCHRES  VOL  CAT Initial value of COLIND  initial value of OUTDGT
*** x  -  x  ac-ft  for each possible  exit  for each possible exit,ft3
2          7230.0  0  4.0  5.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
3           0.1    0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
4           2.0    0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
5           0.1    0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
6           2.0    0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
7           5.0    0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
8           2.0    0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0
9          2700.0  0  4.0  4.0  4.0  4.0  4.0  0.0  0.0  0.0  0.0  0.0

```

10	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
11	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
12	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
13	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
14	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
15	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
16	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
31	3850.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
41	2820.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
51	2350.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
61	250.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0

END HYDR-INIT

\*\*\* Section RQUAL \*\*\*

BENTH-FLAG

RCHRES BENF \*\*\*

# - # \*\*\*

1 61 1

END BENTH-FLAG

SCOUR-PARMS

RCHRES SCRVEL SCRMUL \*\*\*

# - # \*\*\*

1 61 3. 1.

END SCOUR-PARMS

\*\*\* Section OXRX \*\*\*

OX-FLAGS

RCHRES REAM \*\*\*

# - # \*\*\*

2 61 3

END OX-FLAGS

OX-GENPARM

RCHRES KBOD20 TCBOB KODSET SUPSAT \*\*\*

# - # /hr \*\*\*

2 16 0.01 0.005

31 51 0.01 0.005

61 0.01 0.005

END OX-GENPARM

ELEV

\*\*\* RCHRES ELEV

\*\*\* x - x (ft)

2 16 80

31 41 120

51 110

61 100

END ELEV

OX-BENPARM

RCHRES	BENOD	TCBEN	EXPOD	BRBOD (1)	BRBOD (2)	EXPREL	***
# - #	mg/m2.hr			mg/m2.hr	mg/m2.hr		***
2	40	1.1	1.2	0.0001	0.0001	2.82	
3	40	1.1	1.2	0.0001	0.0001	2.82	
4	40	1.1	1.2	0.0001	0.0001	2.82	
5	40	1.1	1.2	0.0001	0.0001	2.82	
6	40	1.1	1.2	0.0001	0.0001	2.82	
7	40	1.1	1.2	0.0001	0.0001	2.82	
8	40	1.1	1.2	0.0001	0.0001	2.82	
9	40	1.1	1.2	0.0001	0.0001	2.82	
10	40	1.1	1.2	0.0001	0.0001	2.82	
11	40	1.1	1.2	0.0001	0.0001	2.82	
12	40	1.1	1.2	0.0001	0.0001	2.82	
13	40	1.1	1.2	0.0001	0.0001	2.82	
14	40	1.1	1.2	0.0001	0.0001	2.82	
15	40	1.1	1.2	0.0001	0.0001	2.82	
16	20	1.1	1.2	0.0001	0.0001	2.82	
31	80	1.1	1.2	0.0001	0.0001	2.82	
41	80	1.1	1.2	0.0001	0.0001	2.82	
51	80	1.1	1.2	0.0001	0.0001	2.82	
61	40	1.1	1.2	0.0001	0.0001	2.82	

END OX-BENPARM

OX-REAPARM

RCHRES	TCGINV	REAK	EXPRED	EXPREV	***
# - #		/hr			***
2	61	0.20	-1.1	1.1	

END OX-REAPARM

OX-INIT

RCHRES	DOX	BOD	SATDO	***
# - #	mg/l	mg/l	mg/l	***
2	61	6	0.1	

END OX-INIT

\*\*\* Section NUTRX \*\*\*

NUT-FLAGS

RCHRES	TAM	NO2	PO4	AMV	DEN	ADNH	ADPO	PHFL	***
# - #									***
1	61	1	0	1	1	0	0	2	

END NUT-FLAGS

NUT-AD-FLAGS

Atmospheric Deposition Flags \*\*\*

RCHRES	NO3	NH3	PO4	***
# - #	F C	F C	F C	***
1	61	-1 0	-1 0	0 0

END NUT-AD-FLAGS

NUT-BENPARM

RCHRES	BRTAM (1)	BRTAM (2)	BRPO4 (1)	BRPO4 (2)	ANAER	***
# - #	mg/m2.hr	mg/m2.hr	mg/m2.hr	mg/m2.hr	mg/l	***
2	61	0.0	0.0	0.0	0.005	

END NUT-BENPARM

NUT-NITDENIT

RCHRES	KTAM20	KNO220	TCNIT	KNO320	TCDEN	DENOXT	***
# - #	/hr	/hr		/hr		mg/l	***
2	0.015	0.002	1.07	0.001	1.04	5	
3	0.015	0.002	1.07	0.001	1.04	5	
4	0.015	0.002	1.07	0.001	1.04	5	
5	0.015	0.002	1.07	0.001	1.04	5	
6	0.015	0.002	1.07	0.001	1.04	5	
7	0.015	0.002	1.07	0.001	1.04	5	
8	0.015	0.002	1.07	0.001	1.04	5	
9	0.015	0.002	1.07	0.001	1.04	5	
10	0.015	0.002	1.07	0.001	1.04	5	
11	0.015	0.002	1.07	0.001	1.04	5	
12	0.015	0.002	1.07	0.001	1.04	5	
13	0.015	0.002	1.07	0.001	1.04	5	
14	0.015	0.002	1.07	0.001	1.04	5	
15	0.015	0.002	1.07	0.001	1.04	5	
16	0.015	0.002	1.07	0.001	1.04	5	
31	0.003	0.002	1.07	0.001	1.04	5	
41	0.003	0.002	1.07	0.001	1.04	5	
51	0.003	0.002	1.07	0.001	1.04	5	
61	0.015	0.002	1.07	0.001	1.04	5	

END NUT-NITDENIT

NUT-NH3VOLAT

RCHRES	EXPNVG	EXPNVL	***
# - #			***
2	.50	0.6667	
3	.50	0.6667	
4	.50	0.6667	
5	.50	0.6667	
6	.50	0.6667	
7	.50	0.6667	
8	.50	0.6667	
9	.50	0.6667	
10	.50	0.6667	
11	.50	0.6667	
12	.50	0.6667	
13	.50	0.6667	
14	.50	0.6667	
15	.50	0.6667	
16	.50	0.6667	
31	.50	0.6667	
41	.50	0.6667	
51	.50	0.6667	
61	.50	0.6667	

END NUT-NH3VOLAT

NUT-DINIT

RCHRES	NO3	TAM	NO2	PO4	PHVAL	***
# - #	mg/l	mg/l	mg/l	mg/l	ph units	***
2	.05	0.05	0.	.02	7.0	
3	.05	0.05	0.	.02	7.0	
4	.05	0.05	0.	.02	7.0	
5	.05	0.05	0.	.02	7.0	
6	.05	0.05	0.	.02	7.0	
7	.05	0.05	0.	.02	7.0	
8	.05	0.05	0.	.02	7.0	
9	.05	0.05	0.	.02	7.0	
10	.05	0.05	0.	.02	7.0	
11	.05	0.05	0.	.02	7.0	
12	.05	0.05	0.	.02	7.0	
13	.05	0.05	0.	.02	7.0	
14	.05	0.05	0.	.02	7.0	
15	.05	0.05	0.	.02	7.0	
16	.05	0.05	0.	.02	7.0	
31	.05	0.05	0.	.02	7.0	
41	.05	0.05	0.	.02	7.0	
51	.05	0.05	0.	.02	7.0	
61	.05	0.05	0.	.02	7.0	

END NUT-DINIT

\*\*\* Section PLANK \*\*\*

PLNK-FLAGS

RCHRES	PHYF	ZOOF	BALF	SDLT	AMRF	DECF	NSFG	ZFOO	***
# - #									***
1	61	1	0	0	0	1		1	

END PLNK-FLAGS

PLNK-PARM1

RCHRES	RATCLP	NONREF	LITSED	ALNPR	EXTB	MALGR	***
# - #					/ft	/hr	***
2	0.6	0.5	0.0	0.70	1.0	0.07	
3	0.6	0.5	0.0	0.70	1.0	0.07	
4	0.6	0.5	0.0	0.70	1.0	0.07	
5	0.6	0.5	0.0	0.70	1.0	0.07	
6	0.6	0.5	0.0	0.70	1.0	0.07	
7	0.6	0.5	0.0	0.70	1.0	0.07	
8	0.6	0.5	0.0	0.70	1.0	0.07	
9	0.6	0.5	0.0	0.70	1.0	0.07	
10	0.6	0.5	0.0	0.70	1.0	0.07	
11	0.6	0.5	0.0	0.70	1.0	0.07	
12	0.6	0.5	0.0	0.70	1.0	0.07	
13	0.6	0.5	0.0	0.70	1.0	0.07	
14	0.6	0.5	0.0	0.70	1.0	0.07	
15	0.6	0.5	0.0	0.70	1.0	0.07	
16	0.6	0.5	0.0	0.70	1.0	0.07	
31	0.6	0.5	0.0	0.70	1.0	0.07	
41	0.6	0.5	0.0	0.70	1.0	0.07	
51	0.6	0.5	0.0	0.70	1.0	0.07	
61	0.6	0.5	0.0	0.70	1.0	0.07	

END PLNK-PARM1

PLNK-PARM2

RCHRES	***	CMMLT	CMMN	CMMNP	CMMP	TALGRH	TALGRL	TALGRM
#	-	#	***					
2		.010	0.025	.0001	.005	95.	-20.0	86.
3		.010	0.025	.0001	.005	95.	-20.0	86.
4		.010	0.025	.0001	.005	95.	-20.0	86.
5		.010	0.025	.0001	.005	95.	-20.0	86.
6		.010	0.025	.0001	.005	95.	-20.0	86.
7		.010	0.025	.0001	.005	95.	-20.0	86.
8		.010	0.025	.0001	.005	95.	-20.0	86.
9		.010	0.025	.0001	.005	95.	-20.0	86.
10		.010	0.025	.0001	.005	95.	-20.0	86.
11		.010	0.025	.0001	.005	95.	-20.0	86.
12		.010	0.025	.0001	.005	95.	-20.0	86.
13		.010	0.025	.0001	.005	95.	-20.0	86.
14		.010	0.025	.0001	.005	95.	-20.0	86.
15		.010	0.025	.0001	.005	95.	-20.0	86.
16		.010	0.025	.0001	.005	95.	-20.0	86.
31		.010	0.025	.0001	.005	95.	-20.0	86.
41		.010	0.025	.0001	.005	95.	-20.0	86.
51		.010	0.025	.0001	.005	95.	-20.0	86.
61		.010	0.025	.0001	.005	95.	-20.0	86.

END PLNK-PARM2

PLNK-PARM3

RCHRES	***	ALR20	ALDH	ALDL	OXALD	NALDH	PALDH
#	-	#	***				
2		0.005	0.01	0.001	0.03	0.01	0.002
3		0.005	0.01	0.001	0.03	0.01	0.002
4		0.005	0.01	0.001	0.03	0.01	0.002
5		0.005	0.01	0.001	0.03	0.01	0.002
6		0.005	0.01	0.001	0.03	0.01	0.002
7		0.005	0.01	0.001	0.03	0.01	0.002
8		0.005	0.01	0.001	0.03	0.01	0.002
9		0.005	0.01	0.001	0.03	0.01	0.002
10		0.005	0.01	0.001	0.03	0.01	0.002
11		0.005	0.01	0.001	0.03	0.01	0.002
12		0.005	0.01	0.001	0.03	0.01	0.002
13		0.005	0.01	0.001	0.03	0.01	0.002
14		0.005	0.01	0.001	0.03	0.01	0.002
15		0.005	0.01	0.001	0.03	0.01	0.002
16		0.005	0.01	0.001	0.03	0.01	0.002
31		0.005	0.01	0.001	0.03	0.01	0.002
41		0.005	0.01	0.001	0.03	0.01	0.002
51		0.005	0.01	0.001	0.03	0.01	0.002
61		0.005	0.01	0.001	0.03	0.01	0.002

END PLNK-PARM3

PHYTO-PARM

RCHRES	SEED	MXSTAY	OREF	CLALDH	PHYSET	REFSET	***
# - #	mg/l	mg/l		ug/l			***
2	.5	2.	20.	20	.02	.02	
3	.5	2.	20.	20	.02	.02	
4	.5	2.	20.	20	.02	.02	
5	.5	2.	20.	20	.02	.02	
6	.5	2.	20.	20	.02	.02	
7	.5	2.	20.	20	.02	.02	
8	.5	2.	20.	20	.02	.02	
9	.5	2.	20.	20	.02	.02	
10	.5	2.	20.	20	.02	.02	
11	.5	2.	20.	20	.02	.02	
12	.5	2.	20.	20	.02	.02	
13	.5	2.	20.	20	.02	.02	
14	.5	2.	20.	20	.02	.02	
15	.5	2.	20.	20	.02	.02	
16	.5	2.	20.	20	.02	.02	
31	.5	2.	20.	20	.02	.02	
41	.5	2.	20.	20	.02	.02	
51	.5	2.	20.	20	.02	.02	
61	.5	2.	20.	20	.02	.02	

END PHYTO-PARM

PLNK-INIT

RCHRES	PHYTO	ZOO	BENAL	ORN	ORP	ORC	***
# - #	mg/l	org/l	mg/m2	mg/l	mg/l	mg/l	***
2 61	.05			.02	0.01	0.1	

END PLNK-INIT

END RCHRES

COPY

TIMESERIES

Copy-opn\*\*\*

*** x - x	NPT	NMN
101 106	7	
1 4	20	

END TIMESERIES

END COPY

EXT SOURCES

<-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> \*\*\*  
 <Name> x <Name> x tem strg<-factor->strg <Name> x x <Name> x x \*\*\*

\*\*\* Precip

\*\*\* DSN 70 = Disaggregated hourly rainfall for Conserv sites 601-604, based on  
 \*\*\* DSN 71 = Disaggregated hourly rainfall for L-101, based on Orlando r  
 \*\*\* DSN 73 = Disaggregated hourly rainfall for Conserv sites 701-901, based on  
 \*\*\* DSN 75 = Disaggregated hourly rainfall for L-410, modified based on 701-901

\*\*\* Segment 1

WDM1	71	PREC	0	ENGL	.45	PERLND	11	19	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.50	PERLND	11	19	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.05	PERLND	11	19	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.45	IMPLND	14	0	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.50	IMPLND	14	0	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.05	IMPLND	14	0	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.45	RCHRES	1	16	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.50	RCHRES	1	16	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.05	RCHRES	1	16	EXTNL	PREC	1	1

\*\*\* Segment 3

WDM1	70	PREC	0	ENGL	.15	PERLND	31	39	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.02	PERLND	31	39	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.80	PERLND	31	39	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.03	PERLND	31	39	EXTNL	PREC	1	1
WDM1	70	PREC	0	ENGL	.15	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.02	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.80	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.03	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	70	PREC	0	ENGL	.15	RCHRES	31	41	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.02	RCHRES	31	41	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.80	RCHRES	31	41	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.03	RCHRES	31	41	EXTNL	PREC	1	1

\*\*\* Segment 5

WDM1	75	PREC	0	ENGL	.80	PERLND	51	59	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.20	PERLND	51	59	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.80	IMPLND	54		EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.20	IMPLND	54		EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.80	RCHRES	51		EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.20	RCHRES	51		EXTNL	PREC	1	1

\*\*\* Segment 6

WDM1	75	PREC	0	ENGL	1.0	PERLND	61	65	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	1.0	IMPLND	64		EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	1.0	RCHRES	61		EXTNL	PREC	1	1

\*\*\* Evap

\*\*\* DSN 80 = PET from mo. pan coefficients x pan evap at Lisbon

WDM1	80	PET		ENGL		PERLND	11	69	EXTNL	PETINP		
WDM1	80	PET		ENGL		IMPLND	14	64	EXTNL	PETINP		
WDM1	80	PET		ENGL		RCHRES	1	61	EXTNL	POTEV		

\*\*\* RIBS application - dataset in units of acre-inches

\*\*\* Divide by total area of ribs for all three lines following

WDM1	91	RIBS		ENGL	.0384615	PERLND	19		EXTNL	PREC		
WDM1	91	RIBS		ENGL	.0316456	PERLND	39		EXTNL	PREC		
WDM1	91	RIBS		ENGL	.0355872	PERLND	59		EXTNL	PREC		

\*\*\* Well water pumped into Bay Lake and Seven Seas Lagoon

WDM	92	PUMP		ENGL		RCHRES	2		EXTNL	IVOL		
-----	----	------	--	------	--	--------	---	--	-------	------	--	--

\*\*\* Grove Irrigation as PREC (sprinkler) or SURLI (drip)

WDM1	94	IRRG		ENGL		PERLND	11		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	21		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	31		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	51		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	61		EXTNL	PREC		

\*\*\* Buzzard site diversion

\*\*\* Data set units are in cubic feet per second

WDM	95	FLOW		ENGL		SAME	RCHRES	15		EXTNL	OUTDGT	1
-----	----	------	--	------	--	------	--------	----	--	-------	--------	---



\*\*\* Cypress Creek discharge (treated as a point)

WDM1 22 FLOW ENGL .082645SAME RCHRES 11 EXTNL IVOL

\*\*\*Cypress Creek water-quality (treated as point source)

\*\*\*do, bod, ammon, no3, po4, orn, orp, orc

WDM 820 DO ENGL DIV RCHRES 11 INFLOW OXIF 1  
WDM 821 BOD ENGL DIV RCHRES 11 INFLOW OXIF 2  
WDM 822 NH3 ENGL DIV RCHRES 11 INFLOW NUIF1 2  
WDM 823 NO3 ENGL DIV RCHRES 11 INFLOW NUIF1 1  
WDM 824 PO4 ENGL DIV RCHRES 11 INFLOW NUIF1 4

\*\*\* Hourly air temperature at ORL MCO (degrees F)

WDM1 85 TEMP ENGL PERLND 11 65 EXTNL GATMP  
WDM1 85 TEMP ENGL IMPLND 14 64 EXTNL GATMP  
WDM1 85 TEMP ENGL RCHRES 1 61 EXTNL GATMP

\*\*\* Daily wind speed (mph)

WDM1 82 WIND ENGL SAME RCHRES 1 61 EXTNL WIND

\*\*\* Hourly solar radiation at Daytona Beach (ly/hr)

WDM1 81 SOLR ENGL RCHRES 1 61 EXTNL SOLRAD

\*\*\* Water Temperature (degrees C)

WDM1 603 TH2O METR RCHRES 2 7 HTRCH TW  
WDM1 602 TH2O METR RCHRES 8 HTRCH TW  
WDM1 603 TH2O METR RCHRES 9 12 HTRCH TW  
WDM1 602 TH2O METR RCHRES 13 HTRCH TW  
WDM1 601 TH2O METR RCHRES 14 16 HTRCH TW  
WDM1 603 TH2O METR RCHRES 31 41 HTRCH TW  
WDM1 604 TH2O METR RCHRES 51 61 HTRCH TW

\*\*\* Atmospheric Deposition (lb/ac)

WDM1 86 NH4D ENGL DIV PERLND 11 65 EXTNL PQADFX 1 1  
WDM1 86 NH4D ENGL DIV IMPLND 14 64 EXTNL IQADFX 1  
WDM1 86 NH4D ENGL DIV RCHRES 1 61 EXTNL NUADFX 2 1  
WDM1 87 NO3D ENGL DIV PERLND 11 65 EXTNL PQADFX 2 1  
WDM1 87 NO3D ENGL DIV IMPLND 14 64 EXTNL IQADFX 2  
WDM1 87 NO3D ENGL DIV RCHRES 1 61 EXTNL NUADFX 1 1

END EXT SOURCES

EXT TARGETS

<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Volume-> <Member> Tsys Aggr Amd \*\*\*  
<Name> x <Name> x x<-factor->strg <Name> x <Name>qf tem strg strg\*\*\*

\*\*\* Seven Seas Lagoon/Bay Lake combined outflow (RCHRES 2)

RCHRES 2 HYDR RO WDM 102 FLOW ENGL AGGR REPL

\*\*\* Lake Mabel/South Lake Outflow (RCHRES 9)

RCHRES 9 HYDR RO WDM 109 FLOW ENGL AGGR REPL

\*\*\* Reedy Creek below S40 near Loughman

RCHRES 15 HYDR RO WDM 115 FLOW ENGL AGGR REPL

\*\*\* Upper East Reedy Creek - Lateral 405 at S-405A

RCHRES 31 HYDR RO WDM 131 FLOW ENGL AGGR REPL

\*\*\* Upper West Reedy Creek - Reedy Creek at S46 near Vineland

RCHRES 41 HYDR RO WDM 141 FLOW ENGL AGGR REPL

\*\*\* Whittenhorse creek stage

RCHRES 51 HYDR STAGE WDM 251 STAG ENGL AGGR REPL

\*\*\* Davenport creek stage

RCHRES 61 HYDR STAGE WDM 261 STAG ENGL AGGR REPL

\*\*\* Miscellaneous temporary calibration

RCHRES 2 OXRX SATDO WDM 1002 TEST ENGL AGGR REPL  
RCHRES 3 OXRX SATDO WDM 1003 TEST ENGL AGGR REPL  
RCHRES 4 OXRX SATDO WDM 1004 TEST ENGL AGGR REPL  
RCHRES 5 OXRX SATDO WDM 1005 TEST ENGL AGGR REPL  
RCHRES 6 OXRX SATDO WDM 1006 TEST ENGL AGGR REPL  
RCHRES 7 OXRX SATDO WDM 1007 TEST ENGL AGGR REPL  
RCHRES 8 OXRX SATDO WDM 1008 TEST ENGL AGGR REPL  
RCHRES 9 OXRX SATDO WDM 1009 TEST ENGL AGGR REPL  
RCHRES 10 OXRX SATDO WDM 1010 TEST ENGL AGGR REPL  
RCHRES 11 OXRX SATDO WDM 1011 TEST ENGL AGGR REPL  
RCHRES 12 OXRX SATDO WDM 1012 TEST ENGL AGGR REPL  
RCHRES 13 OXRX SATDO WDM 1013 TEST ENGL AGGR REPL  
RCHRES 14 OXRX SATDO WDM 1014 TEST ENGL AGGR REPL  
RCHRES 15 OXRX SATDO WDM 1015 TEST ENGL AGGR REPL  
RCHRES 16 OXRX SATDO WDM 1016 TEST ENGL AGGR REPL  
RCHRES 31 OXRX SATDO WDM 1031 TEST ENGL AGGR REPL  
RCHRES 41 OXRX SATDO WDM 1041 TEST ENGL AGGR REPL  
RCHRES 51 OXRX SATDO WDM 1051 TEST ENGL AGGR REPL  
RCHRES 61 OXRX SATDO WDM 1061 TEST ENGL AGGR REPL

\*\*\* WQ DSNS for Loughman \*\*\*

\*\*\* REACH 16 \*\*\*

RCHRES 16 NUTRX DNUST 1 AVER WDM1 2001 NO3X ENGL AGGR REPL  
RCHRES 16 NUTRX DNUST 2 AVER WDM1 2002 NH3X ENGL AGGR REPL  
RCHRES 16 PLANK PKST3 4 AVER WDM1 2003 ORGN ENGL AGGR REPL  
RCHRES 16 PLANK PKST4 1 AVER WDM1 2004 TOTN ENGL AGGR REPL  
RCHRES 16 NUTRX DNUST 4 AVER WDM1 2005 PO4X ENGL AGGR REPL  
RCHRES 16 PLANK PKST3 5 AVER WDM1 2006 ORGP ENGL AGGR REPL  
RCHRES 16 PLANK PKST4 2 AVER WDM1 2007 TOTP ENGL AGGR REPL  
RCHRES 16 PLANK PHYCLA AVER WDM1 2008 CHLA ENGL AGGR REPL  
RCHRES 16 PLANK PKST3 6 AVER WDM1 2009 TOCX ENGL AGGR REPL  
RCHRES 16 OXRX DOX AVER WDM1 2010 DOXX ENGL AGGR REPL  
RCHRES 16 OXRX BOD AVER WDM1 2011 BODX ENGL AGGR REPL  
RCHRES 16 PLANK TPKCF1 4 SUM WDM1 2012 TNLD ENGL AGGR REPL  
RCHRES 16 PLANK TPKCF1 5 SUM WDM1 2013 TPLD ENGL AGGR REPL  
RCHRES 16 NUTRX NUCF1 1 SUM WDM1 2014 NO3L ENGL AGGR REPL  
RCHRES 16 NUTRX NUCF1 2 SUM WDM1 2225 NH3L ENGL AGGR REPL  
RCHRES 16 NUTRX NUCF1 4 SUM WDM1 2226 PO4L ENGL AGGR REPL

\*\*\* WQ DSNS for Davenport Creek \*\*\*

\*\*\* REACH 61 \*\*\*

RCHRES 61 NUTRX DNUST 1 AVER WDM1 2015 NO3X ENGL AGGR REPL  
RCHRES 61 NUTRX DNUST 2 AVER WDM1 2016 NH3X ENGL AGGR REPL  
RCHRES 61 PLANK PKST3 4 AVER WDM1 2017 ORGN ENGL AGGR REPL  
RCHRES 61 PLANK PKST4 1 AVER WDM1 2018 TOTN ENGL AGGR REPL  
RCHRES 61 NUTRX DNUST 4 AVER WDM1 2019 PO4X ENGL AGGR REPL  
RCHRES 61 PLANK PKST3 5 AVER WDM1 2020 ORGP ENGL AGGR REPL  
RCHRES 61 PLANK PKST4 2 AVER WDM1 2021 TOTP ENGL AGGR REPL

RCHRES	61	PLANK	PHYTO		AVER	WDM1	2022	CHLA	ENGL	AGGR	REPL
RCHRES	61	PLANK	PKST3	6	AVER	WDM1	2023	TOCX	ENGL	AGGR	REPL
RCHRES	61	OXR	DOX		AVER	WDM1	2024	DOXX	ENGL	AGGR	REPL
RCHRES	61	OXR	BOD		AVER	WDM1	2025	BODX	ENGL	AGGR	REPL
RCHRES	61	PLANK	TPKCF1	4	SUM	WDM1	2026	TNLD	ENGL	AGGR	REPL
RCHRES	61	PLANK	TPKCF1	5	SUM	WDM1	2027	TPLD	ENGL	AGGR	REPL
RCHRES	61	NUTRX	NUCF1	1	SUM	WDM1	2028	NO3L	ENGL	AGGR	REPL
RCHRES	61	NUTRX	NUCF1	2	SUM	WDM1	2227	NH3L	ENGL	AGGR	REPL
RCHRES	61	NUTRX	NUCF1	4	SUM	WDM1	2228	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Reedy Creek at S-40 \*\*\*

\*\*\* REACH 15 \*\*\*

RCHRES	15	NUTRX	DNUST	1	AVER	WDM1	2029	NO3X	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	2	AVER	WDM1	2030	NH3X	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	4	AVER	WDM1	2031	ORGN	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST4	1	AVER	WDM1	2032	TOTN	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	4	AVER	WDM1	2033	PO4X	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	5	AVER	WDM1	2034	ORGP	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST4	2	AVER	WDM1	2035	TOTP	ENGL	AGGR	REPL
RCHRES	15	PLANK	PHYTO		AVER	WDM1	2036	CHLA	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	6	AVER	WDM1	2037	TOCX	ENGL	AGGR	REPL
RCHRES	15	OXR	DOX		AVER	WDM1	2038	DOXX	ENGL	AGGR	REPL
RCHRES	15	OXR	BOD		AVER	WDM1	2039	BODX	ENGL	AGGR	REPL
RCHRES	15	PLANK	TPKCF1	4	SUM	WDM1	2040	TNLD	ENGL	AGGR	REPL
RCHRES	15	PLANK	TPKCF1	5	SUM	WDM1	2041	TPLD	ENGL	AGGR	REPL
RCHRES	15	NUTRX	NUCF1	1	SUM	WDM1	2042	NO3L	ENGL	AGGR	REPL
RCHRES	15	NUTRX	NUCF1	2	SUM	WDM1	2229	NH3L	ENGL	AGGR	REPL
RCHRES	15	NUTRX	NUCF1	4	SUM	WDM1	2230	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Reedy Creek near Vineland \*\*\*

\*\*\* REACH 7 \*\*\*

RCHRES	7	NUTRX	DNUST	1	AVER	WDM1	2043	NO3X	ENGL	AGGR	REPL
RCHRES	7	NUTRX	DNUST	2	AVER	WDM1	2044	NH3X	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	4	AVER	WDM1	2045	ORGN	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST4	1	AVER	WDM1	2046	TOTN	ENGL	AGGR	REPL
RCHRES	7	NUTRX	DNUST	4	AVER	WDM1	2047	PO4X	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	5	AVER	WDM1	2048	ORGP	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST4	2	AVER	WDM1	2049	TOTP	ENGL	AGGR	REPL
RCHRES	7	PLANK	PHYTO		AVER	WDM1	2050	CHLA	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	6	AVER	WDM1	2051	TOCX	ENGL	AGGR	REPL
RCHRES	7	OXR	DOX		AVER	WDM1	2052	DOXX	ENGL	AGGR	REPL
RCHRES	7	OXR	BOD		AVER	WDM1	2053	BODX	ENGL	AGGR	REPL
RCHRES	7	PLANK	TPKCF1	4	SUM	WDM1	2054	TNLD	ENGL	AGGR	REPL
RCHRES	7	PLANK	TPKCF1	5	SUM	WDM1	2055	TPLD	ENGL	AGGR	REPL
RCHRES	7	NUTRX	NUCF1	1	SUM	WDM1	2056	NO3L	ENGL	AGGR	REPL
RCHRES	7	NUTRX	NUCF1	2	SUM	WDM1	2231	NH3L	ENGL	AGGR	REPL
RCHRES	7	NUTRX	NUCF1	4	SUM	WDM1	2232	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Bonnet Creek near Vineland \*\*\*

\*\*\* REACH 13 \*\*\*

RCHRES	13	NUTRX	DNUST	1	AVER	WDM1	2057	NO3X	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	2	AVER	WDM1	2058	NH3X	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	4	AVER	WDM1	2059	ORGN	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST4	1	AVER	WDM1	2060	TOTN	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	4	AVER	WDM1	2061	PO4X	ENGL	AGGR	REPL

RCHRES	13	PLANK	PKST3	5	AVER	WDM1	2062	ORGP	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST4	2	AVER	WDM1	2063	TOTP	ENGL	AGGR	REPL
RCHRES	13	PLANK	PHYTO		AVER	WDM1	2064	CHLA	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	6	AVER	WDM1	2065	TOCX	ENGL	AGGR	REPL
RCHRES	13	OXRX	DOX		AVER	WDM1	2066	DOXX	ENGL	AGGR	REPL
RCHRES	13	OXRX	BOD		AVER	WDM1	2067	BODX	ENGL	AGGR	REPL
RCHRES	13	PLANK	TPKCF1	4	SUM	WDM1	2068	TNLD	ENGL	AGGR	REPL
RCHRES	13	PLANK	TPKCF1	5	SUM	WDM1	2069	TPLD	ENGL	AGGR	REPL
RCHRES	13	NUTRX	NUCF1	1	SUM	WDM1	2070	NO3L	ENGL	AGGR	REPL
RCHRES	13	NUTRX	NUCF1	2	SUM	WDM1	2233	NH3L	ENGL	AGGR	REPL
RCHRES	13	NUTRX	NUCF1	4	SUM	WDM1	2234	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Whittenhorse Creek \*\*\*

\*\*\* REACH 51 \*\*\*

RCHRES	51	NUTRX	DNUST	1	AVER	WDM1	2071	NO3X	ENGL	AGGR	REPL
RCHRES	51	NUTRX	DNUST	2	AVER	WDM1	2072	NH3X	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST3	4	AVER	WDM1	2073	ORGN	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST4	1	AVER	WDM1	2074	TOTN	ENGL	AGGR	REPL
RCHRES	51	NUTRX	DNUST	4	AVER	WDM1	2075	PO4X	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST3	5	AVER	WDM1	2076	ORGP	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST4	2	AVER	WDM1	2077	TOTP	ENGL	AGGR	REPL
RCHRES	51	PLANK	PHYTO		AVER	WDM1	2078	CHLA	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST3	6	AVER	WDM1	2079	TOCX	ENGL	AGGR	REPL
RCHRES	51	OXRX	DOX		AVER	WDM1	2080	DOXX	ENGL	AGGR	REPL
RCHRES	51	OXRX	BOD		AVER	WDM1	2081	BODX	ENGL	AGGR	REPL
RCHRES	51	PLANK	TPKCF1	4	SUM	WDM1	2082	TNLD	ENGL	AGGR	REPL
RCHRES	51	PLANK	TPKCF1	5	SUM	WDM1	2083	TPLD	ENGL	AGGR	REPL
RCHRES	51	NUTRX	NUCF1	1	SUM	WDM1	2084	NO3L	ENGL	AGGR	REPL
RCHRES	51	NUTRX	NUCF1	2	SUM	WDM1	2235	NH3L	ENGL	AGGR	REPL
RCHRES	51	NUTRX	NUCF1	4	SUM	WDM1	2236	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Upper West Reedy Creek @ S-46 \*\*\*

\*\*\* REACH 41 \*\*\*

RCHRES	41	NUTRX	DNUST	1	AVER	WDM1	2085	NO3X	ENGL	AGGR	REPL
RCHRES	41	NUTRX	DNUST	2	AVER	WDM1	2086	NH3X	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST3	4	AVER	WDM1	2087	ORGN	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST4	1	AVER	WDM1	2088	TOTN	ENGL	AGGR	REPL
RCHRES	41	NUTRX	DNUST	4	AVER	WDM1	2089	PO4X	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST3	5	AVER	WDM1	2090	ORGP	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST4	2	AVER	WDM1	2091	TOTP	ENGL	AGGR	REPL
RCHRES	41	PLANK	PHYTO		AVER	WDM1	2092	CHLA	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST3	6	AVER	WDM1	2093	TOCX	ENGL	AGGR	REPL
RCHRES	41	OXRX	DOX		AVER	WDM1	2094	DOXX	ENGL	AGGR	REPL
RCHRES	41	OXRX	BOD		AVER	WDM1	2095	BODX	ENGL	AGGR	REPL
RCHRES	41	PLANK	TPKCF1	4	SUM	WDM1	2096	TNLD	ENGL	AGGR	REPL
RCHRES	41	PLANK	TPKCF1	5	SUM	WDM1	2097	TPLD	ENGL	AGGR	REPL
RCHRES	41	NUTRX	NUCF1	1	SUM	WDM1	2098	NO3L	ENGL	AGGR	REPL
RCHRES	41	NUTRX	NUCF1	2	SUM	WDM1	2237	NH3L	ENGL	AGGR	REPL
RCHRES	41	NUTRX	NUCF1	4	SUM	WDM1	2238	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Upper East Reedy Creek @ S-405A \*\*\*

\*\*\* REACH 31 \*\*\*

RCHRES	31	NUTRX	DNUST	1	AVER	WDM1	2099	NO3X	ENGL	AGGR	REPL
RCHRES	31	NUTRX	DNUST	2	AVER	WDM1	2100	NH3X	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST3	4	AVER	WDM1	2101	ORGN	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST4	1	AVER	WDM1	2102	TOTN	ENGL	AGGR	REPL
RCHRES	31	NUTRX	DNUST	4	AVER	WDM1	2103	PO4X	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST3	5	AVER	WDM1	2104	ORGP	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST4	2	AVER	WDM1	2105	TOTP	ENGL	AGGR	REPL
RCHRES	31	PLANK	PHYTO		AVER	WDM1	2106	CHLA	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST3	6	AVER	WDM1	2107	TOCX	ENGL	AGGR	REPL
RCHRES	31	OXR	DOX		AVER	WDM1	2108	DOXX	ENGL	AGGR	REPL
RCHRES	31	OXR	BOD		AVER	WDM1	2109	BODX	ENGL	AGGR	REPL
RCHRES	31	PLANK	TPKCF1	4	SUM	WDM1	2110	TNLD	ENGL	AGGR	REPL
RCHRES	31	PLANK	TPKCF1	5	SUM	WDM1	2111	TPLD	ENGL	AGGR	REPL
RCHRES	31	NUTRX	NUCF1	1	SUM	WDM1	2112	NO3L	ENGL	AGGR	REPL
RCHRES	31	NUTRX	NUCF1	2	SUM	WDM1	2239	NH3L	ENGL	AGGR	REPL
RCHRES	31	NUTRX	NUCF1	4	SUM	WDM1	2240	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Lateral 405 at S-405 \*\*\*

\*\*\* REACH 3 \*\*\*

RCHRES	3	NUTRX	DNUST	1	AVER	WDM1	2113	NO3X	ENGL	AGGR	REPL
RCHRES	3	NUTRX	DNUST	2	AVER	WDM1	2114	NH3X	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST3	4	AVER	WDM1	2115	ORGN	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST4	1	AVER	WDM1	2116	TOTN	ENGL	AGGR	REPL
RCHRES	3	NUTRX	DNUST	4	AVER	WDM1	2117	PO4X	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST3	5	AVER	WDM1	2118	ORGP	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST4	2	AVER	WDM1	2119	TOTP	ENGL	AGGR	REPL
RCHRES	3	PLANK	PHYTO		AVER	WDM1	2120	CHLA	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST3	6	AVER	WDM1	2121	TOCX	ENGL	AGGR	REPL
RCHRES	3	OXR	DOX		AVER	WDM1	2122	DOXX	ENGL	AGGR	REPL
RCHRES	3	OXR	BOD		AVER	WDM1	2123	BODX	ENGL	AGGR	REPL
RCHRES	3	PLANK	TPKCF1	4	SUM	WDM1	2124	TNLD	ENGL	AGGR	REPL
RCHRES	3	PLANK	TPKCF1	5	SUM	WDM1	2125	TPLD	ENGL	AGGR	REPL
RCHRES	3	NUTRX	NUCF1	1	SUM	WDM1	2126	NO3L	ENGL	AGGR	REPL
RCHRES	3	NUTRX	NUCF1	2	SUM	WDM1	2241	NH3L	ENGL	AGGR	REPL
RCHRES	3	NUTRX	NUCF1	4	SUM	WDM1	2242	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Reedy Creek at I-4 \*\*\*

\*\*\* REACH 8 \*\*\*

RCHRES	8	NUTRX	DNUST	1	AVER	WDM1	2127	NO3X	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	2	AVER	WDM1	2128	NH3X	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	4	AVER	WDM1	2129	ORGN	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST4	1	AVER	WDM1	2130	TOTN	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	4	AVER	WDM1	2131	PO4X	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	5	AVER	WDM1	2132	ORGP	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST4	2	AVER	WDM1	2133	TOTP	ENGL	AGGR	REPL
RCHRES	8	PLANK	PHYTO		AVER	WDM1	2134	CHLA	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	6	AVER	WDM1	2135	TOCX	ENGL	AGGR	REPL
RCHRES	8	OXR	DOX		AVER	WDM1	2136	DOXX	ENGL	AGGR	REPL
RCHRES	8	OXR	BOD		AVER	WDM1	2137	BODX	ENGL	AGGR	REPL
RCHRES	8	PLANK	TPKCF1	4	SUM	WDM1	2138	TNLD	ENGL	AGGR	REPL
RCHRES	8	PLANK	TPKCF1	5	SUM	WDM1	2139	TPLD	ENGL	AGGR	REPL
RCHRES	8	NUTRX	NUCF1	1	SUM	WDM1	2140	NO3L	ENGL	AGGR	REPL
RCHRES	8	NUTRX	NUCF1	2	SUM	WDM1	2243	NH3L	ENGL	AGGR	REPL
RCHRES	8	NUTRX	NUCF1	4	SUM	WDM1	2244	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Bay Lake/Seven Seas \*\*\*

\*\*\* REACH 2 \*\*\*

RCHRES	2	NUTRX	DNUST	1	AVER	WDM1	2141	NO3X	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	2	AVER	WDM1	2142	NH3X	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	4	AVER	WDM1	2143	ORGN	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST4	1	AVER	WDM1	2144	TOTN	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	4	AVER	WDM1	2145	PO4X	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	5	AVER	WDM1	2146	ORGP	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST4	2	AVER	WDM1	2147	TOTP	ENGL	AGGR	REPL
RCHRES	2	PLANK	PHYTO		AVER	WDM1	2148	CHLA	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	6	AVER	WDM1	2149	TOCX	ENGL	AGGR	REPL
RCHRES	2	OXX	DOX		AVER	WDM1	2150	DOXX	ENGL	AGGR	REPL
RCHRES	2	OXX	BOD		AVER	WDM1	2151	BODX	ENGL	AGGR	REPL
RCHRES	2	PLANK	TPKCF1	4	SUM	WDM1	2152	TNLD	ENGL	AGGR	REPL
RCHRES	2	PLANK	TPKCF1	5	SUM	WDM1	2153	TPLD	ENGL	AGGR	REPL
RCHRES	2	NUTRX	NUCF1	1	SUM	WDM1	2154	NO3L	ENGL	AGGR	REPL
RCHRES	2	NUTRX	NUCF1	2	SUM	WDM1	2245	NH3L	ENGL	AGGR	REPL
RCHRES	2	NUTRX	NUCF1	4	SUM	WDM1	2246	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Lake Mabel/South Lake

\*\*\* REACH 9 \*\*\*

RCHRES	9	NUTRX	DNUST	1	AVER	WDM1	2155	NO3X	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	2	AVER	WDM1	2156	NH3X	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	4	AVER	WDM1	2157	ORGN	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST4	1	AVER	WDM1	2158	TOTN	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	4	AVER	WDM1	2159	PO4X	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	5	AVER	WDM1	2160	ORGP	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST4	2	AVER	WDM1	2161	TOTP	ENGL	AGGR	REPL
RCHRES	9	PLANK	PHYTO		AVER	WDM1	2162	CHLA	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	6	AVER	WDM1	2163	TOCX	ENGL	AGGR	REPL
RCHRES	9	OXX	DOX		AVER	WDM1	2164	DOXX	ENGL	AGGR	REPL
RCHRES	9	OXX	BOD		AVER	WDM1	2165	BODX	ENGL	AGGR	REPL
RCHRES	9	PLANK	TPKCF1	4	SUM	WDM1	2166	TNLD	ENGL	AGGR	REPL
RCHRES	9	PLANK	TPKCF1	5	SUM	WDM1	2167	TPLD	ENGL	AGGR	REPL
RCHRES	9	NUTRX	NUCF1	1	SUM	WDM1	2168	NO3L	ENGL	AGGR	REPL
RCHRES	9	NUTRX	NUCF1	2	SUM	WDM1	2247	NH3L	ENGL	AGGR	REPL
RCHRES	9	NUTRX	NUCF1	4	SUM	WDM1	2248	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Lower L-405 \*\*\*

\*\*\* REACH 6 \*\*\*

RCHRES	6	NUTRX	DNUST	1	AVER	WDM1	2169	NO3X	ENGL	AGGR	REPL
RCHRES	6	NUTRX	DNUST	2	AVER	WDM1	2170	NH3X	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST3	4	AVER	WDM1	2171	ORGN	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST4	1	AVER	WDM1	2172	TOTN	ENGL	AGGR	REPL
RCHRES	6	NUTRX	DNUST	4	AVER	WDM1	2173	PO4X	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST3	5	AVER	WDM1	2174	ORGP	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST4	2	AVER	WDM1	2175	TOTP	ENGL	AGGR	REPL
RCHRES	6	PLANK	PHYTO		AVER	WDM1	2176	CHLA	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST3	6	AVER	WDM1	2177	TOCX	ENGL	AGGR	REPL
RCHRES	6	OXX	DOX		AVER	WDM1	2178	DOXX	ENGL	AGGR	REPL
RCHRES	6	OXX	BOD		AVER	WDM1	2179	BODX	ENGL	AGGR	REPL
RCHRES	6	PLANK	TPKCF1	4	SUM	WDM1	2180	TNLD	ENGL	AGGR	REPL
RCHRES	6	PLANK	TPKCF1	5	SUM	WDM1	2181	TPLD	ENGL	AGGR	REPL
RCHRES	6	NUTRX	NUCF1	1	SUM	WDM1	2182	NO3L	ENGL	AGGR	REPL
RCHRES	6	NUTRX	NUCF1	2	SUM	WDM1	2249	NH3L	ENGL	AGGR	REPL
RCHRES	6	NUTRX	NUCF1	4	SUM	WDM1	2250	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-103, Buena Vista \*\*\*

\*\*\* REACH 11 \*\*\*

RCHRES	11	NUTRX	DNUST	1	AVER	WDM1	2183	NO3X	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	2	AVER	WDM1	2184	NH3X	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	4	AVER	WDM1	2185	ORGN	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST4	1	AVER	WDM1	2186	TOTN	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	4	AVER	WDM1	2187	PO4X	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	5	AVER	WDM1	2188	ORGP	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST4	2	AVER	WDM1	2189	TOTP	ENGL	AGGR	REPL
RCHRES	11	PLANK	PHYTO		AVER	WDM1	2190	CHLA	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	6	AVER	WDM1	2191	TOCX	ENGL	AGGR	REPL
RCHRES	11	OXR	DOX		AVER	WDM1	2192	DOXX	ENGL	AGGR	REPL
RCHRES	11	OXR	BOD		AVER	WDM1	2193	BODX	ENGL	AGGR	REPL
RCHRES	11	PLANK	TPKCF1	4	SUM	WDM1	2194	TNLD	ENGL	AGGR	REPL
RCHRES	11	PLANK	TPKCF1	5	SUM	WDM1	2195	TPLD	ENGL	AGGR	REPL
RCHRES	11	NUTRX	NUCF1	1	SUM	WDM1	2196	NO3L	ENGL	AGGR	REPL
RCHRES	11	NUTRX	NUCF1	2	SUM	WDM1	2251	NH3L	ENGL	AGGR	REPL
RCHRES	11	NUTRX	NUCF1	4	SUM	WDM1	2252	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-105 \*\*\*

\*\*\* REACH 10 \*\*\*

RCHRES	10	NUTRX	DNUST	1	AVER	WDM1	2197	NO3X	ENGL	AGGR	REPL
RCHRES	10	NUTRX	DNUST	2	AVER	WDM1	2198	NH3X	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST3	4	AVER	WDM1	2199	ORGN	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST4	1	AVER	WDM1	2200	TOTN	ENGL	AGGR	REPL
RCHRES	10	NUTRX	DNUST	4	AVER	WDM1	2201	PO4X	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST3	5	AVER	WDM1	2202	ORGP	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST4	2	AVER	WDM1	2203	TOTP	ENGL	AGGR	REPL
RCHRES	10	PLANK	PHYTO		AVER	WDM1	2204	CHLA	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST3	6	AVER	WDM1	2205	TOCX	ENGL	AGGR	REPL
RCHRES	10	OXR	DOX		AVER	WDM1	2206	DOXX	ENGL	AGGR	REPL
RCHRES	10	OXR	BOD		AVER	WDM1	2207	BODX	ENGL	AGGR	REPL
RCHRES	10	PLANK	TPKCF1	4	SUM	WDM1	2208	TNLD	ENGL	AGGR	REPL
RCHRES	10	PLANK	TPKCF1	5	SUM	WDM1	2209	TPLD	ENGL	AGGR	REPL
RCHRES	10	NUTRX	NUCF1	1	SUM	WDM1	2210	NO3L	ENGL	AGGR	REPL
RCHRES	10	NUTRX	NUCF1	2	SUM	WDM1	2253	NH3L	ENGL	AGGR	REPL
RCHRES	10	NUTRX	NUCF1	4	SUM	WDM1	2254	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-403 - EPCOT \*\*\*

\*\*\* REACH 5 \*\*\*

RCHRES	5	NUTRX	DNUST	1	AVER	WDM1	2211	NO3X	ENGL	AGGR	REPL
RCHRES	5	NUTRX	DNUST	2	AVER	WDM1	2212	NH3X	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST3	4	AVER	WDM1	2213	ORGN	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST4	1	AVER	WDM1	2214	TOTN	ENGL	AGGR	REPL
RCHRES	5	NUTRX	DNUST	4	AVER	WDM1	2215	PO4X	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST3	5	AVER	WDM1	2216	ORGP	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST4	2	AVER	WDM1	2217	TOTP	ENGL	AGGR	REPL
RCHRES	5	PLANK	PHYTO		AVER	WDM1	2218	CHLA	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST3	6	AVER	WDM1	2219	TOCX	ENGL	AGGR	REPL
RCHRES	5	OXR	DOX		AVER	WDM1	2220	DOXX	ENGL	AGGR	REPL
RCHRES	5	OXR	BOD		AVER	WDM1	2221	BODX	ENGL	AGGR	REPL
RCHRES	5	PLANK	TPKCF1	4	SUM	WDM1	2222	TNLD	ENGL	AGGR	REPL
RCHRES	5	PLANK	TPKCF1	5	SUM	WDM1	2223	TPLD	ENGL	AGGR	REPL
RCHRES	5	NUTRX	NUCF1	1	SUM	WDM1	2224	NO3L	ENGL	AGGR	REPL
RCHRES	5	NUTRX	NUCF1	2	SUM	WDM1	2255	NH3L	ENGL	AGGR	REPL
RCHRES	5	NUTRX	NUCF1	4	SUM	WDM1	2256	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for C-4 \*\*\*

\*\*\* REACH 4 \*\*\*

RCHRES	4	NUTRX	DNUST	1	AVER	WDM1	2257	NO3X	ENGL	AGGR	REPL
RCHRES	4	NUTRX	DNUST	2	AVER	WDM1	2258	NH3X	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST3	4	AVER	WDM1	2259	ORGN	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST4	1	AVER	WDM1	2260	TOTN	ENGL	AGGR	REPL
RCHRES	4	NUTRX	DNUST	4	AVER	WDM1	2261	PO4X	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST3	5	AVER	WDM1	2262	ORGP	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST4	2	AVER	WDM1	2263	TOTP	ENGL	AGGR	REPL
RCHRES	4	PLANK	PHYTO		AVER	WDM1	2264	CHLA	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST3	6	AVER	WDM1	2265	TOCX	ENGL	AGGR	REPL
RCHRES	4	OXX	DOX		AVER	WDM1	2266	DOXX	ENGL	AGGR	REPL
RCHRES	4	OXX	BOD		AVER	WDM1	2267	BODX	ENGL	AGGR	REPL
RCHRES	4	PLANK	TPKCF1	4	SUM	WDM1	2268	TNLD	ENGL	AGGR	REPL
RCHRES	4	PLANK	TPKCF1	5	SUM	WDM1	2269	TPLD	ENGL	AGGR	REPL
RCHRES	4	NUTRX	NUCF1	1	SUM	WDM1	2270	NO3L	ENGL	AGGR	REPL
RCHRES	4	NUTRX	NUCF1	2	SUM	WDM1	2271	NH3L	ENGL	AGGR	REPL
RCHRES	4	NUTRX	NUCF1	4	SUM	WDM1	2272	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-107/UPPER C-1 \*\*\*

\*\*\* REACH 12 \*\*\*

RCHRES	12	NUTRX	DNUST	1	AVER	WDM1	2273	NO3X	ENGL	AGGR	REPL
RCHRES	12	NUTRX	DNUST	2	AVER	WDM1	2274	NH3X	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST3	4	AVER	WDM1	2275	ORGN	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST4	1	AVER	WDM1	2276	TOTN	ENGL	AGGR	REPL
RCHRES	12	NUTRX	DNUST	4	AVER	WDM1	2277	PO4X	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST3	5	AVER	WDM1	2278	ORGP	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST4	2	AVER	WDM1	2279	TOTP	ENGL	AGGR	REPL
RCHRES	12	PLANK	PHYTO		AVER	WDM1	2280	CHLA	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST3	6	AVER	WDM1	2281	TOCX	ENGL	AGGR	REPL
RCHRES	12	OXX	DOX		AVER	WDM1	2282	DOXX	ENGL	AGGR	REPL
RCHRES	12	OXX	BOD		AVER	WDM1	2283	BODX	ENGL	AGGR	REPL
RCHRES	12	PLANK	TPKCF1	4	SUM	WDM1	2284	TNLD	ENGL	AGGR	REPL
RCHRES	12	PLANK	TPKCF1	5	SUM	WDM1	2285	TPLD	ENGL	AGGR	REPL
RCHRES	12	NUTRX	NUCF1	1	SUM	WDM1	2286	NO3L	ENGL	AGGR	REPL
RCHRES	12	NUTRX	NUCF1	2	SUM	WDM1	2287	NH3L	ENGL	AGGR	REPL
RCHRES	12	NUTRX	NUCF1	4	SUM	WDM1	2288	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for LOWER C-1 \*\*\*

\*\*\* REACH 14 \*\*\*

RCHRES	14	NUTRX	DNUST	1	AVER	WDM1	2289	NO3X	ENGL	AGGR	REPL
RCHRES	14	NUTRX	DNUST	2	AVER	WDM1	2290	NH3X	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST3	4	AVER	WDM1	2291	ORGN	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST4	1	AVER	WDM1	2292	TOTN	ENGL	AGGR	REPL
RCHRES	14	NUTRX	DNUST	4	AVER	WDM1	2293	PO4X	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST3	5	AVER	WDM1	2294	ORGP	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST4	2	AVER	WDM1	2295	TOTP	ENGL	AGGR	REPL
RCHRES	14	PLANK	PHYTO		AVER	WDM1	2296	CHLA	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST3	6	AVER	WDM1	2297	TOCX	ENGL	AGGR	REPL
RCHRES	14	OXX	DOX		AVER	WDM1	2298	DOXX	ENGL	AGGR	REPL
RCHRES	14	OXX	BOD		AVER	WDM1	2299	BODX	ENGL	AGGR	REPL
RCHRES	14	PLANK	TPKCF1	4	SUM	WDM1	2300	TNLD	ENGL	AGGR	REPL
RCHRES	14	PLANK	TPKCF1	5	SUM	WDM1	2301	TPLD	ENGL	AGGR	REPL
RCHRES	14	NUTRX	NUCF1	1	SUM	WDM1	2302	NO3L	ENGL	AGGR	REPL
RCHRES	14	NUTRX	NUCF1	2	SUM	WDM1	2303	NH3L	ENGL	AGGR	REPL
RCHRES	14	NUTRX	NUCF1	4	SUM	WDM1	2304	PO4L	ENGL	AGGR	REPL



\*\*\* WHITTENHORSE CREEK

\*\*\* All acreage of segment 5 in Whittenhorse basin, i.e. area rch 51

RCHRES	51	HYDR	RO		1.0	WDM	411	FLOW	ENGL	AGGR	REPL
RCHRES	51	ROFLOW	ROVOL		.00163049	WDM	418	SIMQ	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	1	0.0001359	WDM	412	SURO	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	2	0.0001359	WDM	413	IFWO	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	3	0.0001359	WDM	414	AGWO	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	4	0.0001359	WDM	419	PETX	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	5	0.0001359	WDM	415	SAET	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	6	0.0001359	WDM	416	UZSX	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	7	0.0001359	WDM	417	LZSX	ENGL	AGGR	REPL

\*\*\* DAVENPORT CREEK

\*\*\* All acreage of segment 6 in Davenport basin, i.e. area rch 61

RCHRES	61	HYDR	RO		1.0	WDM	421	FLOW	ENGL	AGGR	REPL
RCHRES	61	ROFLOW	ROVOL		.00116923	WDM	428	SIMQ	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	1	0.0000974	WDM	422	SURO	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	2	0.0000974	WDM	423	IFWO	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	3	0.0000974	WDM	424	AGWO	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	4	0.0000974	WDM	429	PETX	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	5	0.0000974	WDM	425	SAET	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	6	0.0000974	WDM	426	UZSX	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	7	0.0000974	WDM	427	LZSX	ENGL	AGGR	REPL

\*\*\* REEDY CREEK @ HWY 192

\*\*\* Sum of areas rch 1, 2 (except half direct lake contrib area), rch 3-7

\*\*\* All segment 3

\*\*\* All Whittenhorse

RCHRES	7	HYDR	RO		1.0	WDM	431	FLOW	ENGL	AGGR	REPL
RCHRES	7	ROFLOW	ROVOL		2.7686E-4	WDM	438	SIMQ	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	1	2.3223E-5	WDM	432	SURO	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	2	2.3223E-5	WDM	433	IFWO	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	3	2.3223E-5	WDM	434	AGWO	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	4	2.3223E-5	WDM	439	PETX	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	5	2.3223E-5	WDM	435	SAET	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	6	2.3223E-5	WDM	436	UZSX	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	7	2.3223E-5	WDM	437	LZSX	ENGL	AGGR	REPL

\*\*\* BONNETT CREEK

\*\*\* Sum of areas rch 2 (except half direct lake contrib area), rch 9-13

\*\*\* All segment 2

RCHRES	13	HYDR	RO		1.0	WDM	441	FLOW	ENGL	AGGR	REPL
RCHRES	13	ROFLOW	ROVOL		1.3820E-3	WDM	448	SIMQ	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	1	1.1517E-4	WDM	442	SURO	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	2	1.1517E-4	WDM	443	IFWO	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	3	1.1517E-4	WDM	444	AGWO	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	4	1.1517E-4	WDM	449	PETX	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	5	1.1517E-4	WDM	445	SAET	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	6	1.1517E-4	WDM	446	UZSX	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	7	1.1517E-4	WDM	447	LZSX	ENGL	AGGR	REPL

\*\*\* REEDY CREEK @ LOUGHMAN

\*\*\* All segments 1-6

RCHRES	16	HYDR	RO	1.0	WDM	451	FLOW	ENGL	AGGR	REPL	
RCHRES	16	ROFLOW	ROVOL	1.5678E-4	WDM	458	SIMQ	ENGL	AGGR	REPL	
COPY	106	OUTPUT	MEAN	1	1.3065E-5	WDM	452	SURO	ENGL	AGGR	REPL
COPY	106	OUTPUT	MEAN	2	1.3065E-5	WDM	453	IFWO	ENGL	AGGR	REPL
COPY	106	OUTPUT	MEAN	3	1.3065E-5	WDM	454	AGWO	ENGL	AGGR	REPL
COPY	106	OUTPUT	MEAN	4	1.3065E-5	WDM	459	PETX	ENGL	AGGR	REPL
COPY	106	OUTPUT	MEAN	5	1.3065E-5	WDM	455	SAET	ENGL	AGGR	REPL
COPY	106	OUTPUT	MEAN	6	1.3065E-5	WDM	456	UZSX	ENGL	AGGR	REPL
COPY	106	OUTPUT	MEAN	7	1.3065E-5	WDM	457	LZSX	ENGL	AGGR	REPL

END EXT TARGETS

SCHEMATIC

<-Volume->		<--Area-->		<-Volume->	<ML#>	***
<Name>	x	<-factor->		<Name>	x	***

\*\*\* Internal Basin

PERLND	11	***	0.0	RCHRES	2	1
PERLND	12		26.0	RCHRES	2	1
PERLND	13	***	0.0	RCHRES	2	1
PERLND	14		5.7	RCHRES	2	1
PERLND	15		2.5	RCHRES	2	1
IMPLND	14		12.5	RCHRES	2	2
PERLND	11		3.7	RCHRES	3	1
PERLND	12		679.6	RCHRES	3	1
PERLND	13		84.9	RCHRES	3	1
PERLND	14		596.0	RCHRES	3	1
PERLND	15		936.6	RCHRES	3	1
IMPLND	14		519.8	RCHRES	3	2
PERLND	11		325.6	RCHRES	4	1
PERLND	12		84.7	RCHRES	4	1
PERLND	13		141.7	RCHRES	4	1
PERLND	14		269.4	RCHRES	4	1
PERLND	16		963.8	RCHRES	4	1
PERLND	19		26.0	RCHRES	4	1
IMPLND	14		76.8	RCHRES	4	2
PERLND	11	***	0.0	RCHRES	5	1
PERLND	12		47.6	RCHRES	5	1
PERLND	13		74.1	RCHRES	5	1
PERLND	14		177.4	RCHRES	5	1
PERLND	15		236.0	RCHRES	5	1
IMPLND	14		268.2	RCHRES	5	2
PERLND	11		655.8	RCHRES	6	1
PERLND	12		555.1	RCHRES	6	1
PERLND	13		1501.6	RCHRES	6	1
PERLND	14		1023.6	RCHRES	6	1
PERLND	16		3735.1	RCHRES	6	1
IMPLND	14		638.7	RCHRES	6	2

PERLND	11	***	0.0	RCHRES	7	1
PERLND	12		592.4	RCHRES	7	1
PERLND	13		610.0	RCHRES	7	1
PERLND	14		61.3	RCHRES	7	1
PERLND	15		1822.9	RCHRES	7	1
IMPLND	14		30.0	RCHRES	7	2
PERLND	11		794.9	RCHRES	8	1
PERLND	12		320.4	RCHRES	8	1
PERLND	13		532.6	RCHRES	8	1
PERLND	14		70.1	RCHRES	8	1
PERLND	18		1697.9	RCHRES	8	1
IMPLND	14		47.0	RCHRES	8	2
PERLND	11		138.2	RCHRES	9	1
PERLND	12		22.4	RCHRES	9	1
PERLND	13		163.5	RCHRES	9	1
PERLND	14		213.8	RCHRES	9	1
PERLND	15		465.0	RCHRES	9	1
IMPLND	14		61.8	RCHRES	9	2
PERLND	11	***	0.0	RCHRES	10	1
PERLND	12		16.5	RCHRES	10	1
PERLND	13		116.1	RCHRES	10	1
PERLND	14		243.5	RCHRES	10	1
PERLND	15		424.8	RCHRES	10	1
IMPLND	14		60.9	RCHRES	10	2
PERLND	11	***	0.0	RCHRES	11	1
PERLND	12		312.3	RCHRES	11	1
PERLND	13		41.0	RCHRES	11	1
PERLND	14		217.7	RCHRES	11	1
PERLND	15		791.7	RCHRES	11	1
IMPLND	14		773.5	RCHRES	11	2
PERLND	11		70.3	RCHRES	12	1
PERLND	12		390.3	RCHRES	12	1
PERLND	13		92.5	RCHRES	12	1
PERLND	14		141.8	RCHRES	12	1
PERLND	15		1301.0	RCHRES	12	1
IMPLND	14		52.2	RCHRES	12	2
PERLND	11	***	0.0	RCHRES	13	1
PERLND	12		282.7	RCHRES	13	1
PERLND	13		950.5	RCHRES	13	1
PERLND	14		84.8	RCHRES	13	1
PERLND	15		874.0	RCHRES	13	1
IMPLND	14		357.0	RCHRES	13	2
PERLND	11	***	0.0	RCHRES	14	1
PERLND	12		555.4	RCHRES	14	1
PERLND	13		1228.0	RCHRES	14	1
PERLND	14		119.4	RCHRES	14	1
PERLND	17		2552.2	RCHRES	14	1
IMPLND	14		101.7	RCHRES	14	2

PERLND	11		1320.7	RCHRES	15	1
PERLND	12		120.3	RCHRES	15	1
PERLND	13		1308.4	RCHRES	15	1
PERLND	14		79.0	RCHRES	15	1
PERLND	18		2966.1	RCHRES	15	1
IMPLND	14		23.6	RCHRES	15	2
PERLND	11	***	0.0	RCHRES	16	1
PERLND	12		111.3	RCHRES	16	1
PERLND	13		530.0	RCHRES	16	1
PERLND	14		47.6	RCHRES	16	1
PERLND	18		1133.6	RCHRES	16	1
IMPLND	14		19.8	RCHRES	16	2
*** East Upper Reedy						
PERLND	31		2161.1	RCHRES	31	1
PERLND	32		169.6	RCHRES	31	1
PERLND	33		2306.1	RCHRES	31	1
PERLND	34		64.4	RCHRES	31	1
PERLND	35		2684.5	RCHRES	31	1
IMPLND	34		30.3	RCHRES	31	2
*** West Upper Reedy						
PERLND	31		4002.0	RCHRES	41	1
PERLND	32		215.9	RCHRES	41	1
PERLND	33		3694.5	RCHRES	41	1
PERLND	34		137.5	RCHRES	41	1
PERLND	35		2240.7	RCHRES	41	1
PERLND	39		31.6	RCHRES	41	1
IMPLND	34		53.2	RCHRES	41	2
*** Whittenhorse						
PERLND	51		2118.5	RCHRES	51	1
PERLND	52		184.2	RCHRES	51	1
PERLND	53		1481.6	RCHRES	51	1
PERLND	54		100.9	RCHRES	51	1
PERLND	55		3400.0	RCHRES	51	1
PERLND	59		28.1	RCHRES	51	1
IMPLND	54		46.6	RCHRES	51	2
*** Davenport						
PERLND	61		4854.3	RCHRES	61	1
PERLND	62		304.6	RCHRES	61	1
PERLND	63		1704.5	RCHRES	61	1
PERLND	64		385.4	RCHRES	61	1
PERLND	65		2854.3	RCHRES	61	1
IMPLND	64		160.1	RCHRES	61	2
*** Reach Connections						
RCHRES	31			RCHRES	3	3
RCHRES	41			RCHRES	4	3
RCHRES	51			RCHRES	4	3
RCHRES	2			RCHRES	3	4
RCHRES	2			RCHRES	10	5

RCHRES	3		RCHRES	6	3
RCHRES	4		RCHRES	6	3
RCHRES	5		RCHRES	6	3
RCHRES	6		RCHRES	7	3
RCHRES	7		RCHRES	8	3
RCHRES	8		RCHRES	15	3
RCHRES	9		RCHRES	12	3
RCHRES	10		RCHRES	12	3
RCHRES	11		RCHRES	13	3
RCHRES	12		RCHRES	13	3
RCHRES	13		RCHRES	14	3
RCHRES	14		RCHRES	15	3
RCHRES	61		RCHRES	15	3
RCHRES	15		RCHRES	16	5

\*\*\* HSPEXP Datasets

\*\*\* Whittenhorse 02266200

\*\*\* All acreage of Segment 5

PERLND	51	2118.5	COPY	102	90
PERLND	52	184.2	COPY	102	90
PERLND	53	1481.6	COPY	102	90
PERLND	54	100.9	COPY	102	90
PERLND	55	3400.0	COPY	102	90
PERLND	59	28.1	COPY	102	90
IMPLND	54	46.6	COPY	102	91

\*\*\* Davenport 02266480

\*\*\* All acreage of Segment 6

PERLND	61	4854.3	COPY	103	90
PERLND	62	304.6	COPY	103	90
PERLND	63	1704.5	COPY	103	90
PERLND	64	385.4	COPY	103	90
PERLND	65	2854.3	COPY	103	90
IMPLND	64	160.1	COPY	103	91

\*\*\* Reedy @ Hwy 192 02266300

\*\*\* sum areas rch 1, 2 (except half direct lake contrib area), 3-7

PERLND	11	985.1	COPY	104	90
PERLND	12	1972.3	COPY	104	90
PERLND	13	2412.3	COPY	104	90
PERLND	14	2130.5	COPY	104	90
PERLND	15	937.8	COPY	104	90
PERLND	16	965.0	COPY	104	90
PERLND	19	26.0	COPY	104	90
IMPLND	14	1539.8	COPY	104	91

\*\*\* all Segment 3

PERLND	31	6163.1	COPY	104	90
PERLND	32	385.5	COPY	104	90
PERLND	33	6000.6	COPY	104	90
PERLND	34	201.9	COPY	104	90
PERLND	35	4925.3	COPY	104	90
PERLND	39	31.6	COPY	104	90
IMPLND	34	83.5	COPY	104	91

\*\*\* all Whittenhorse

PERLND	51	2118.5	COPY	104	90
PERLND	52	184.2	COPY	104	90
PERLND	53	1481.6	COPY	104	90
PERLND	54	100.9	COPY	104	90
PERLND	55	3400.0	COPY	104	90
PERLND	59	28.1	COPY	104	90
IMPLND	54	46.6	COPY	104	91

\*\*\* Bonnett 02264100

\*\*\* sum areas rch 2 (half lake contrib area only), 9-13

PERLND	11	208.5	COPY	105	90
PERLND	12	1037.2	COPY	105	90
PERLND	13	1363.6	COPY	105	90
PERLND	14	904.4	COPY	105	90
PERLND	15	3857.9	COPY	105	90
IMPLND	14	1311.6	COPY	105	91

\*\*\* Reedy @ Loughman 02266500

\*\*\* all segment 1

PERLND	11	3309.3	COPY	106	90
PERLND	12	4116.9	COPY	106	90
PERLND	13	7374.8	COPY	106	90
PERLND	14	3350.9	COPY	106	90
PERLND	15	6854.6	COPY	106	90
PERLND	16	4698.9	COPY	106	90
PERLND	17	2552.2	COPY	106	90
PERLND	18	5797.5	COPY	106	90
PERLND	19	26.0	COPY	106	90
IMPLND	14	3043.6	COPY	106	91

\*\*\* all segment 3

PERLND	31	6163.1	COPY	106	90
PERLND	32	385.5	COPY	106	90
PERLND	33	6000.6	COPY	106	90
PERLND	34	201.9	COPY	106	90
PERLND	35	4925.3	COPY	106	90
PERLND	39	31.6	COPY	106	90
IMPLND	34	83.5	COPY	106	91

\*\*\* all segment 5

PERLND	51	2118.5	COPY	106	90
PERLND	52	184.2	COPY	106	90
PERLND	53	1481.6	COPY	106	90
PERLND	54	100.9	COPY	106	90
PERLND	55	3400.0	COPY	106	90
PERLND	59	28.1	COPY	106	90
IMPLND	54	46.6	COPY	106	91

\*\*\* All Segment 6

PERLND	61	4854.3	COPY	106	90
PERLND	62	304.6	COPY	106	90
PERLND	63	1704.5	COPY	106	90
PERLND	64	385.4	COPY	106	90
PERLND	65	2854.3	COPY	106	90
IMPLND	64	160.1	COPY	106	91

\*\*\* Total loadings report

\*\*\* all segment 1

PERLND	11	3309.3	REPORT	1	8	1
PERLND	12	4116.9	REPORT	1	8	2
PERLND	13	7374.8	REPORT	1	8	3
PERLND	14	3350.9	REPORT	1	8	4
PERLND	15	6854.6	REPORT	1	8	5
PERLND	16	4698.9	REPORT	1	8	5
PERLND	17	2552.2	REPORT	1	8	5
PERLND	18	5797.5	REPORT	1	8	5
PERLND	19	26.0	REPORT	1	8	6
IMPLND	14	3043.6	REPORT	1	9	7

\*\*\* all segment 3

PERLND	31	6163.1	REPORT	3	8	1
PERLND	32	385.5	REPORT	3	8	2
PERLND	33	6000.6	REPORT	3	8	3
PERLND	34	201.9	REPORT	3	8	4
PERLND	35	4925.3	REPORT	3	8	5
PERLND	39	31.6	REPORT	3	8	6
IMPLND	34	83.5	REPORT	3	9	7

\*\*\* all segment 5

PERLND	51	2118.5	REPORT	5	8	1
PERLND	52	184.2	REPORT	5	8	2
PERLND	53	1481.6	REPORT	5	8	3
PERLND	54	100.9	REPORT	5	8	4
PERLND	55	3400.0	REPORT	5	8	5
PERLND	59	28.1	REPORT	5	8	6
IMPLND	54	46.6	REPORT	5	9	7

\*\*\* all segment 6

PERLND	61	4854.3	REPORT	6	8	1
PERLND	62	304.6	REPORT	6	8	2
PERLND	63	1704.5	REPORT	6	8	3
PERLND	64	385.4	REPORT	6	8	4
PERLND	65	2854.3	REPORT	6	8	5
IMPLND	64	160.1	REPORT	6	9	7

\*\*\* Per acre loadings report \*\*\*

\*\*\* all segment 1

PERLND	11		REPORT	11	8	1
PERLND	12		REPORT	11	8	2
PERLND	13		REPORT	11	8	3
PERLND	14		REPORT	11	8	4
PERLND	15	.3444	REPORT	11	8	5
PERLND	16	.2361	REPORT	11	8	5
PERLND	17	.1282	REPORT	11	8	5
PERLND	18	.2913	REPORT	11	8	5
PERLND	19		REPORT	11	8	6
IMPLND	14		REPORT	11	9	7

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*** all segment 3
PERLND 31          REPORT 13      8      1
PERLND 32          REPORT 13      8      2
PERLND 33          REPORT 13      8      3
PERLND 34          REPORT 13      8      4
PERLND 35          REPORT 13      8      5
PERLND 39          REPORT 13      8      6
IMPLND 34          REPORT 13      9      7

*** all segment 5
PERLND 51          REPORT 15      8      1
PERLND 52          REPORT 15      8      2
PERLND 53          REPORT 15      8      3
PERLND 54          REPORT 15      8      4
PERLND 55          REPORT 15      8      5
PERLND 59          REPORT 15      8      6
IMPLND 54          REPORT 15      9      7

*** all segment 6
PERLND 61          REPORT 16      8      1
PERLND 62          REPORT 16      8      2
PERLND 63          REPORT 16      8      3
PERLND 64          REPORT 16      8      4
PERLND 65          REPORT 16      8      5
IMPLND 64          REPORT 16      9      7

*** Percent loads report
*** all segment 1
PERLND 11          3309.3    REPORT 21      8      1
PERLND 12          4116.9    REPORT 21      8      2
PERLND 13          7374.8    REPORT 21      8      3
PERLND 14          3350.9    REPORT 21      8      4
PERLND 15          6854.6    REPORT 21      8      5
PERLND 16          4698.9    REPORT 21      8      5
PERLND 17          2552.2    REPORT 21      8      5
PERLND 18          5797.5    REPORT 21      8      5
PERLND 19           26.0     REPORT 21      8      6
IMPLND 14          3043.6    REPORT 21      9      7

*** all segment 3
PERLND 31          6163.1    REPORT 23      8      1
PERLND 32          385.5     REPORT 23      8      2
PERLND 33          6000.6    REPORT 23      8      3
PERLND 34          201.9     REPORT 23      8      4
PERLND 35          4925.3    REPORT 23      8      5
PERLND 39           31.6     REPORT 23      8      6
IMPLND 34          83.5      REPORT 23      9      7

*** all segment 5
PERLND 51          2118.5    REPORT 25      8      1
PERLND 52          184.2     REPORT 25      8      2
PERLND 53          1481.6    REPORT 25      8      3
PERLND 54          100.9     REPORT 25      8      4
PERLND 55          3400.0    REPORT 25      8      5
PERLND 59           28.1     REPORT 25      8      6
IMPLND 54          46.6      REPORT 25      9      7

```



\*\*\* all segment 6

PERLND	61	4854.3	REPORT	26	8	1
PERLND	62	304.6	REPORT	26	8	2
PERLND	63	1704.5	REPORT	26	8	3
PERLND	64	385.4	REPORT	26	8	4
PERLND	65	2854.3	REPORT	26	8	5
IMPLND	64	160.1	REPORT	26	9	7

RCHRES	31		REPORT	100	10	1
RCHRES	41		REPORT	100	10	2
RCHRES	51		REPORT	100	10	3
RCHRES	61		REPORT	100	10	4
RCHRES	2		REPORT	100	10	5
RCHRES	3		REPORT	100	10	6
RCHRES	4		REPORT	100	10	7
RCHRES	5		REPORT	100	10	8
RCHRES	6		REPORT	100	10	9
RCHRES	7		REPORT	100	10	10
RCHRES	8		REPORT	100	10	11
RCHRES	9		REPORT	100	10	12
RCHRES	10		REPORT	100	10	13
RCHRES	11		REPORT	100	10	14
RCHRES	12		REPORT	100	10	15
RCHRES	13		REPORT	100	10	16
RCHRES	14		REPORT	100	10	17
RCHRES	15		REPORT	100	10	18
RCHRES	16		REPORT	100	10	19

END SCHEMATIC

MASS-LINK

MASS-LINK		10						
<-Volume->	<-Grp>	<-Member->	<--Mult-->	Tran	<-Target vols>	<-Grp>	<-Member->	***
<Name>		<Name>	x	x<-factor->	strg	<Name>	<Name>	x x ***
RCHRES	OXR	OXIF	1		REPORT	INPUT	TIMSER 1	
RCHRES	OXR	OXCF3	1		REPORT	INPUT	TIMSER 2	
RCHRES	OXR	OXCF3	2		REPORT	INPUT	TIMSER 3	
RCHRES	OXR	OXCF3	3		REPORT	INPUT	TIMSER 4	
RCHRES	OXR	OXCF3	4		REPORT	INPUT	TIMSER 5	
RCHRES	OXR	OXCF3	5		REPORT	INPUT	TIMSER 6	
RCHRES	OXR	OXIF	2		REPORT	INPUT	TIMSER 7	
RCHRES	OXR	OXCF4	1		REPORT	INPUT	TIMSER 8	
RCHRES	OXR	OXCF4	2		REPORT	INPUT	TIMSER 9	
RCHRES	OXR	OXCF4	3		REPORT	INPUT	TIMSER10	
RCHRES	OXR	OXCF4	4		REPORT	INPUT	TIMSER11	
RCHRES	OXR	OXCF4	5		REPORT	INPUT	TIMSER12	
RCHRES	NUTRX	NUIF1	2		REPORT	INPUT	TIMSER13	
RCHRES	NUTRX	NUCF5	1		REPORT	INPUT	TIMSER14	
RCHRES	NUTRX	NUCF5	2		REPORT	INPUT	TIMSER15	
RCHRES	NUTRX	NUCF5	3		REPORT	INPUT	TIMSER16	
RCHRES	NUTRX	NUCF5	4		REPORT	INPUT	TIMSER17	
RCHRES	NUTRX	NUCF5	5		REPORT	INPUT	TIMSER18	
RCHRES	NUTRX	NUIF1	1		REPORT	INPUT	TIMSER19	
RCHRES	NUTRX	NUCF4	1		REPORT	INPUT	TIMSER20	

RCHRES	NUTRX	NUCF4	2	REPORT	INPUT	TIMSER21
RCHRES	NUTRX	NUCF4	3	REPORT	INPUT	TIMSER22
RCHRES	NUTRX	NUCF4	4	REPORT	INPUT	TIMSER23
RCHRES	NUTRX	NUIF1	4	REPORT	INPUT	TIMSER24
RCHRES	NUTRX	NUCF7	1	REPORT	INPUT	TIMSER25
RCHRES	NUTRX	NUCF7	2	REPORT	INPUT	TIMSER26
RCHRES	NUTRX	NUCF7	3	REPORT	INPUT	TIMSER27
RCHRES	PLANK	PKIF	1	REPORT	INPUT	TIMSER28
RCHRES	PLANK	PKCF5	1	REPORT	INPUT	TIMSER29
RCHRES	PLANK	PKCF5	3	REPORT	INPUT	TIMSER30
RCHRES	PLANK	PKCF5	4	REPORT	INPUT	TIMSER31
RCHRES	PLANK	PKIF	3	REPORT	INPUT	TIMSER32
RCHRES	PLANK	PKCF8	1	REPORT	INPUT	TIMSER33
RCHRES	PLANK	PKCF8	2	REPORT	INPUT	TIMSER34
RCHRES	PLANK	PKIF	4	REPORT	INPUT	TIMSER35
RCHRES	PLANK	PKCF9	1	REPORT	INPUT	TIMSER36
RCHRES	PLANK	PKCF9	2	REPORT	INPUT	TIMSER37
RCHRES	PLANK	PKIF	5	REPORT	INPUT	TIMSER38
RCHRES	PLANK	PKCF10	1	REPORT	INPUT	TIMSER39
RCHRES	PLANK	PKCF10	2	REPORT	INPUT	TIMSER40

END MASS-LINK 10

MASS-LINK 9

<-Volume->	<-Grp>	<-Member->	<--Mult-->	Tran	<-Target vols>	<-Grp>	<-Member->	***
<Name>		<Name>	x	x<-factor->	strg	<Name>	<Name>	x x ***
IMPLND	IQUAL	SOQUAL	1		REPORT	INPUT	TIMSER	1
IMPLND	IQUAL	SOQUAL	2		REPORT	INPUT	TIMSER	2
IMPLND	IQUAL	SOQUAL	4	0.0480	REPORT	INPUT	TIMSER	3
IMPLND	IQUAL	SOQUAL	1		REPORT	INPUT	TIMSER	4
IMPLND	IQUAL	SOQUAL	2		REPORT	INPUT	TIMSER	4
IMPLND	IQUAL	SOQUAL	4	0.0480	REPORT	INPUT	TIMSER	4
IMPLND	IQUAL	SOQUAL	3		REPORT	INPUT	TIMSER	5
IMPLND	IQUAL	SOQUAL	4	0.0023	REPORT	INPUT	TIMSER	6
IMPLND	IQUAL	SOQUAL	3		REPORT	INPUT	TIMSER	7
IMPLND	IQUAL	SOQUAL	4	0.0023	REPORT	INPUT	TIMSER	7
IMPLND	IQUAL	SOQUAL	4	0.400	REPORT	INPUT	TIMSER	8
IMPLND	IQUAL	SOQUAL	4	0.301	REPORT	INPUT	TIMSER	9

END MASS-LINK 9

MASS-LINK 8

<-Volume->	<-Grp>	<-Member->	<--Mult-->	Tran	<-Target vols>	<-Grp>	<-Member->	***
<Name>		<Name>	x	x<-factor->	strg	<Name>	<Name>	x x ***
PERLND	PQUAL	POQUAL	1		REPORT	INPUT	TIMSER	1
PERLND	PQUAL	POQUAL	2		REPORT	INPUT	TIMSER	2
PERLND	PQUAL	POQUAL	4	0.0480	REPORT	INPUT	TIMSER	3
PERLND	PQUAL	POQUAL	1		REPORT	INPUT	TIMSER	4
PERLND	PQUAL	POQUAL	2		REPORT	INPUT	TIMSER	4
PERLND	PQUAL	POQUAL	4	0.0480	REPORT	INPUT	TIMSER	4
PERLND	PQUAL	POQUAL	3		REPORT	INPUT	TIMSER	5
PERLND	PQUAL	POQUAL	4	0.0023	REPORT	INPUT	TIMSER	6
PERLND	PQUAL	POQUAL	3		REPORT	INPUT	TIMSER	7
PERLND	PQUAL	POQUAL	4	0.0023	REPORT	INPUT	TIMSER	7
PERLND	PQUAL	POQUAL	4	0.400	REPORT	INPUT	TIMSER	8
PERLND	PQUAL	POQUAL	4	0.301	REPORT	INPUT	TIMSER	9

END MASS-LINK 8

```

    MASS-LINK          1
<-Volume-> <-Grp> <-Member-><--Mult--> Tran<-Target vols> <-Grp> <-Member->***
<Name>***          <Name> x x<-factor-> strg<Name>          <Name> x x
PERLND    PWATER  PERO          0.0833333    RCHRES          INFLOW  IVOL
PERLND    PWTGAS  PODOXM          RCHRES          INFLOW  OXIF    1
PERLND    PQUAL   POQUAL  1          RCHRES          INFLOW  NUIF1   2
PERLND    PQUAL   POQUAL  2          RCHRES          INFLOW  NUIF1   1
PERLND    PQUAL   POQUAL  3          RCHRES          INFLOW  NUIF1   4
PERLND    PQUAL   POQUAL  4          0.40           RCHRES          INFLOW  OXIF    2
PERLND    PQUAL   POQUAL  4          0.048          RCHRES          INFLOW  PKIF    3
PERLND    PQUAL   POQUAL  4          0.0023         RCHRES          INFLOW  PKIF    4
PERLND    PQUAL   POQUAL  4          0.301          RCHRES          INFLOW  PKIF    5
    END MASS-LINK      1

    MASS-LINK          2
<-Volume-> <-Grp> <-Member-><--Mult--> Tran<-Target vols> <-Grp> <-Member->***
<Name>***          <Name> x x<-factor-> strg<Name>          <Name> x x
IMPLND    IWATER  SURO          0.0833333    RCHRES          INFLOW  IVOL
IMPLND    IWTGAS  SODOXM          RCHRES          INFLOW  OXIF    1
IMPLND    IQUAL   SOQUAL  1          RCHRES          INFLOW  NUIF1   2
IMPLND    IQUAL   SOQUAL  2          RCHRES          INFLOW  NUIF1   1
IMPLND    IQUAL   SOQUAL  3          RCHRES          INFLOW  NUIF1   4
IMPLND    IQUAL   SOQUAL  4          0.40           RCHRES          INFLOW  OXIF    2
IMPLND    IQUAL   SOQUAL  4          0.048          RCHRES          INFLOW  PKIF    3
IMPLND    IQUAL   SOQUAL  4          0.0023         RCHRES          INFLOW  PKIF    4
IMPLND    IQUAL   SOQUAL  4          0.301          RCHRES          INFLOW  PKIF    5
    END MASS-LINK      2

    MASS-LINK          3
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    ROFLOW          RCHRES          INFLOW
    END MASS-LINK      3

    MASS-LINK          4
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          1          RCHRES          INFLOW
    END MASS-LINK      4

    MASS-LINK          5
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          2          RCHRES          INFLOW
    END MASS-LINK      5

    MASS-LINK          6
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          3          RCHRES          INFLOW
    END MASS-LINK      6

    MASS-LINK          7
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          4          RCHRES          INFLOW
    END MASS-LINK      7

```

```

    MASS-LINK          90
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
PERLND    PWATER  SURO          COPY          INPUT  MEAN    1
PERLND    PWATER  IFWO          COPY          INPUT  MEAN    2
PERLND    PWATER  AGWO          COPY          INPUT  MEAN    3
PERLND    PWATER  PET           COPY          INPUT  MEAN    4
PERLND    PWATER  TAET          COPY          INPUT  MEAN    5
PERLND    PWATER  UZS           COPY          INPUT  MEAN    6
PERLND    PWATER  LZS           COPY          INPUT  MEAN    7
    END MASS-LINK    90

```

```

    MASS-LINK          91
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
IMPLND    IWATER  SURO          COPY          INPUT  MEAN    1
IMPLND    IWATER  PET           COPY          INPUT  MEAN    4
IMPLND    IWATER  IMPEV         COPY          INPUT  MEAN    5
    END MASS-LINK    91
END MASS-LINK

```

FTABLES

```

    FTABLE          2
    14      5
    DEPTH          AREA          VOLUME          DISCH1          DISCH2 ***
    (FT)          (ACRES)        (AC-FT)         (CFS)           (CFS) ***
    0.0           0.0           0.0             0               0
    1.0           2.1           0.7             0               0
    6.0           8.2           29.9            0               0
    10.0          36.9          123.3           0               0
    14.0          124.6         408.1           0               0
    18.0          332.5         1054.3          0               0
    22.0          411.2         2424.5          0               0
    26.0          466.4         4185.8          0               0
    30.0          524.2         6178.6          0               0
    31.0          527.1         6702.8          0               0
    32.0          569.8         7229.9          0               0
    33.0          583.5         7745.6          52.00          208.01
    34.0          596.5         8266.5          104.52          418.08
    35.0          611.5         8788.3          157.14          628.55
    END FTABLE    2

```

```

    FTABLE          3
    15      4
    DEPTH          AREA          VOLUME          DISCH ***
    (FT)          (ACRES)        (AC-FT)         (CFS) ***
    0.00           0.0           0.0             0.0
    0.74           25.1          17.1            13.6
    1.48           29.0          37.0            44.7
    2.21           32.9          59.9            91.3
    2.95           36.8          85.6            153.6
    3.69           40.7          114.2           231.9
    4.43           44.6          145.6           327.0
    5.90           52.4          217.2           570.9

```

7.38	60.2	300.2	892.0
8.85	68.0	394.8	1297.
11.80	635.5	1432.5	3104.
14.75	1203.1	4144.4	7550.
17.70	1770.6	8530.5	16025.
20.65	2338.1	14590.8	29680.
23.60	2905.6	22325.3	49543.

END FTABLE 3

FTABLE 4

15 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
1.00	2.3	1.9	0.2	
2.00	3.2	4.6	0.9	
3.00	4.1	8.2	1.9	
4.00	4.9	12.7	3.5	
5.00	5.8	18.1	5.6	
6.00	6.7	24.4	8.3	
8.00	8.5	39.5	15.9	
10.00	10.2	58.2	26.6	
12.00	12.0	80.4	40.9	
16.00	306.5	717.4	123.2	
20.00	601.0	2532.4	367.5	
24.00	895.5	5525.4	863.3	
28.00	1190.0	9696.5	1685.	
32.00	1484.5	15045.6	2898.	

END FTABLE 4

FTABLE 5

15 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
1.33	14.3	17.6	128.9	
2.67	16.7	38.3	423.1	
4.00	19.0	62.1	863.4	
5.33	21.4	89.0	1451.	
6.67	23.7	119.1	2190.	
8.00	26.0	152.2	3090.	
10.67	30.7	227.9	5399.	
13.33	35.4	316.1	8445.	
16.00	40.1	416.8	12294.	
21.33	660.3	2284.6	26168.	
26.67	1280.6	7460.3	50366.	
32.00	1900.8	15944.0	89001.	
37.33	2521.0	27735.5	145505.	
42.67	3141.3	42835.0	222956.	

END FTABLE 5

```

FTABLE      6
  15      4
    DEPTH      AREA      VOLUME      DISCH ***
      (FT)    (ACRES)    (AC-FT)    (CFS) ***
    0.00      0.0      0.0      0.0
    0.57     11.5      6.2      5.9
    1.13     12.7     13.0     19.1
    1.70     13.9     20.5     38.4
    2.27     15.1     28.7     63.4
    2.83     16.2     37.6     94.3
    3.40     17.4     47.1    131.0
    4.53     19.8     68.2    222.4
    5.67     22.2     92.0    339.0
    6.80     24.5    118.5    482.3
    9.07    220.8    396.5    997.8
   11.33    417.0   1119.4   1973.
   13.60    613.3   2287.1   3616.
   15.87    809.5   3899.7   6102.
   18.13   1005.8   5957.0   9584.
END FTABLE  6

```

```

FTABLE      7
  15      4
    DEPTH      AREA      VOLUME      DISCH ***
      (FT)    (ACRES)    (AC-FT)    (CFS) ***
    0.00      0.0      0.0      0.0
    0.38    269.6     98.3     56.7
    0.77    296.0    206.7    184.0
    1.15    322.3    325.2    369.9
    1.53    348.7    453.8    611.7
    1.92    375.0    592.6    909.0
    2.30    401.4    741.4   1262.
    3.07    454.1   1069.3   2140.
    3.83    506.8   1437.7   3258.
    4.60    559.5   1846.4   4629.
    6.13    666.1   2786.1   8807.
    7.67    772.7   3889.2  14237.
    9.20    879.3   5155.6  20997.
   10.73    985.8   6585.5  29160.
   12.27   1092.4   8178.9  38800.
END FTABLE  7

```

```

FTABLE      8
  15      4
    DEPTH      AREA      VOLUME      DISCH ***
      (FT)    (ACRES)    (AC-FT)    (CFS) ***
    0.00      0.0      0.0      0.0
    0.54     87.7     42.1     14.4
    1.08    107.6     95.0     48.7
    1.63    127.5    158.7    102.4
    2.17    147.4    233.1    176.5
    2.71    167.3    318.4    272.6
    3.25    187.2    414.4    392.5
    4.33    227.1    638.8    710.0
    5.42    266.9    906.4   1142.

```

6.50	306.7	1217.1	1701.
8.67	495.7	2086.4	3614.
10.83	684.7	3365.2	6436.
13.00	873.8	5053.6	10376.
15.17	1062.8	7151.5	15616.
17.33	1251.8	9658.9	22317.

END FTABLE 8

FTABLE 9

10	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0	0	0	0	
0.01	406.641	0	0	
1	421.107	445.873	0	
2	435.720	896.251	0	
3	450.332	1346.628	0	
4	464.945	1797.005	0	
5	479.557	2247.382	0	
6	494.170	2697.760	0	
7	508.783	3148.137	227.1	
8	523.395	3598.514	454.1	

END FTABLE 9

FTABLE 10

15	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0.00	0.0	0.0	0.0	
1.71	2.9	3.5	8.1	
3.42	4.4	9.8	32.4	
5.13	6.0	18.7	77.7	
6.83	7.6	30.3	148.3	
8.54	9.2	44.6	248.7	
10.25	10.7	61.6	382.6	
13.67	13.9	103.6	765.8	
17.08	17.0	156.4	1326.	
20.50	20.2	219.9	2089.	
27.33	439.0	1788.9	6256.	
34.17	857.9	6220.1	17971.	
41.00	1276.8	13513.7	41312.	
47.83	1695.7	23669.6	79656.	
54.67	2114.5	36687.8	136014.	

END FTABLE 10

FTABLE 11

15	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0.00	0.0	0.0	0.0	
1.00	4.4	3.6	7.8	
2.00	6.0	8.8	28.0	
3.00	7.6	15.6	61.6	
4.00	9.2	24.0	110.6	
5.00	10.8	34.0	177.0	

6.00	12.4	45.6	262.6
8.00	15.6	73.5	498.6
10.00	18.7	107.8	832.1
12.00	21.9	148.5	1276.
16.00	425.9	1044.0	3792.
20.00	829.8	3555.3	11204.
24.00	1233.8	7682.5	26215.
28.00	1637.7	13425.4	51062.
32.00	2041.7	20784.1	87738.

END FTABLE 11

FTABLE 12			
15	4		
DEPTH	AREA	VOLUME	DISCH ***
(FT)	(ACRES)	(AC-FT)	(CFS) ***
0.00	0.0	0.0	0.0
1.27	14.6	14.7	16.8
2.54	20.6	37.2	62.0
3.81	26.7	67.2	139.9
5.08	32.7	104.9	256.1
6.35	38.7	150.3	415.9
7.63	44.8	203.4	624.3
10.17	56.8	332.5	1206.
12.71	68.9	492.2	2039.
15.25	80.9	682.5	3155.
20.33	1269.2	4114.1	10265.
25.42	2457.5	13586.3	32999.
30.50	3645.9	29099.1	80174.
35.58	4834.2	50652.5	159080.
40.67	6022.5	78246.5	276217.

END FTABLE 12

FTABLE 13			
15	4		
DEPTH	AREA	VOLUME	DISCH ***
(FT)	(ACRES)	(AC-FT)	(CFS) ***
0.00	0.0	0.0	0.0
1.35	13.8	17.3	50.0
2.70	15.8	37.3	163.9
4.05	17.9	60.0	333.2
5.40	19.9	85.5	557.7
6.75	21.9	113.7	838.8
8.10	23.9	144.6	1179.
10.80	28.0	214.7	2045.
13.50	32.0	295.7	3179.
16.20	36.1	387.7	4603.
21.60	479.3	1779.2	10436.
27.00	922.5	5564.1	23326.
32.40	1365.7	11742.4	46807.
37.80	1809.0	20314.2	83810.
43.20	2252.2	31279.3	136949.

END FTABLE 13



```

FTABLE      14
15      4
  DEPTH      AREA      VOLUME      DISCH ***
  (FT)      (ACRES)    (AC-FT)    (CFS) ***
  0.00      0.0        0.0        0.0
  1.32      28.0       34.8       76.0
  2.64      31.5       74.1      247.0
  3.96      34.9      117.9      498.1
  5.28      38.3      166.2      827.0
  6.60      41.7      219.1     1234.
  7.92      45.2      276.5     1721.
 10.57      52.0      404.9     2947.
 13.21      58.9      551.4     4527.
 15.85      65.7      716.0     6486.
 21.13     891.3     3244.2    14395.
 26.42    1716.9    10134.2   31869.
 31.70    2542.5    21386.0   63733.
 36.98    3368.0    36999.5  113983.
 42.27    4193.6    56974.8  186187.
END FTABLE 14

```

```

FTABLE      15
15      4
  DEPTH      AREA      VOLUME      DISCH ***
  (FT)      (ACRES)    (AC-FT)    (CFS) ***
  0.00      0.0        0.0        0.0
  0.88     229.4      176.5     107.8
  1.76     286.8      403.4     368.7
  2.64     344.1      680.7     780.9
  3.52     401.5     1008.5    1357.
  4.40     458.8     1386.6    2110.
  5.28     516.2     1815.2    3057.
  7.03     630.9     2823.7    5585.
  8.79     745.6     4033.9    9054.
 10.55     860.3     5445.7   13572.
 14.07    1206.1     9079.1   28863.
 17.58    1551.8    13928.4  50439.
 21.10    1897.6    19993.6  79279.
 24.62    2243.3    27274.7  116247.
 28.13    2589.1    35771.7  162147.
END FTABLE 15

```

```

FTABLE      16
16      4
  DEPTH      AREA      VOLUME      DISCH ***
  (FT)      (ACRES)    (AC-FT)    (CFS) ***
  0.00      0.00       0.0        0.0
  0.01      1.49       0.1        0.0
  0.23      1.72       0.2        0.14
  0.73      2.34       0.82       0.41
  1.23      3.18       2.34       1.11
  1.73      4.33       4.63       3.05
  2.23      5.89       7.69       8.34
  2.73      8.01      11.5       22.8
  3.23     10.9      16.1       62.4

```

3.73	14.8	21.5	170.6
4.23	20.1	27.7	466.6
4.73	27.4	34.6	1276.
5.23	37.2	42.3	3491.
5.73	50.6	50.7	9550.
6.23	68.9	60.0	26121.
6.73	93.7	70.0	71450.

END FTABLE 16

FTABLE 31

10 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
0.01	600.0	3.0	0.0	
1.00	612.4	603.2	0.0	
2.00	625.1	1221.9	0.0	
3.00	637.9	1853.5	0.0	
4.00	650.9	2497.8	0.0	
5.00	663.9	3155.2	0.0	
6.00	677.1	3825.7	0.0	
7.00	690.4	4509.5	446.6	
8.00	703.9	5206.7	901.9	

END FTABLE 31

FTABLE 41

10 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
0.01	435.8	2.2	0.0	
1.00	446.4	438.8	0.0	
2.00	457.2	890.6	0.0	
3.00	468.2	1353.3	0.0	
4.00	479.2	1827.0	0.0	
5.00	490.5	2311.9	0.0	
6.00	501.8	2808.0	0.0	
7.00	513.3	3315.6	331.5	
8.00	524.9	3834.7	670.5	

END FTABLE 41

FTABLE 51

15 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.0	820.00	0.00	0.0	
0.5	830.00	412.50	0.0	
1.0	840.00	830.00	0.0	
1.5	850.00	1252.50	0.0	
2.0	860.00	1680.00	0.0	
2.5	870.14	2112.54	0.1	
3.0	880.28	2550.14	4.0	
3.5	890.42	2992.82	17.0	
4.0	900.57	3440.56	60.0	
4.5	910.60	3893.36	280.0	

5.0	920.60	4351.16	1000.0
5.5	930.60	4813.96	4500.0
6.0	940.60	5281.76	17000.0
6.5	950.60	5754.56	75000.0
7.0	960.60	6232.36	250000.0

END FTABLE 51

FTABLE 61

22 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.0	61.6	0.0	0.0	
0.2	104.67	16.63	1.00	
0.4	146.76	41.77	1.80	
1.0	272.92	167.68	6.90	
1.5	377.94	330.39	13.0	
2.0	482.87	545.60	21.0	
2.5	587.74	813.25	37.0	
3.0	692.54	1133.32	53.0	
3.5	797.29	1505.78	79.0	
4.0	902.00	1930.60	140.0	
4.5	1006.66	2407.76	220.0	
5.0	1111.19	2937.23	350.0	
5.5	1283.64	3535.94	725.0	
6.0	1456.06	4220.86	1100.0	
6.5	1628.46	4992.00	2000.0	
7.0	1800.83	5849.32	2600.0	
7.5	1973.18	6792.82	4800.0	
8.0	2145.52	7822.50	7000.0	
8.5	2317.83	8938.33	13000.0	
9.0	2490.13	10140.32	19000.0	
9.5	2662.41	11428.46	29500.0	
10.0	2834.68	12802.73	40000.0	

END FTABLE 61

END FTABLES

END RUN



## Appendix E



## APPENDIX E

User control input file for simulating future land use with the Hydrological Simulation Program-Fortran

```
----- FLUSE08.uci-----***
RUN

GLOBAL
  Reedy Creek, Orange and Osceola Counties, Florida
  START      1990  1  1  0  0  END      1995 12 31 24  0
  RUN INTERP OUTPUT LEVEL    4    1
  RESUME     0 RUN    1                UNIT SYSTEM    1
END GLOBAL

FILES
<type> <fun>***<-----fname----->
MESSU    25  FLUSE08.ech
WDM      27  reedy.wdm
          90  FLUSE08.out
          91  FLUSE08.totrept1.out
          93  FLUSE08.totrept3.out
          95  FLUSE08.totrept5.out
          96  FLUSE08.totrept6.out
          81  FLUSE08.accrept1.out
          83  FLUSE08.accrept3.out
          85  FLUSE08.accrept5.out
          86  FLUSE08.accrept6.out
          71  FLUSE08.pctrept1.out
          73  FLUSE08.pctrept3.out
          75  FLUSE08.pctrept5.out
          76  FLUSE08.pctrept6.out
          51  FLUSE08.rchflux.out
END FILES

OPN SEQUENCE
  INGRP          INDELT  1: 0
  PERLND         31
  PERLND         32
  PERLND         33
  PERLND         34
  PERLND         39
  PERLND         35
  IMPLND         34
  RCHRES         31
  RCHRES         41

  PERLND         51
  PERLND         52
  PERLND         53
  PERLND         54
  PERLND         55
  PERLND         59
  IMPLND         54
  RCHRES         51
  COPY           102
```

PERLND	61
PERLND	62
PERLND	63
PERLND	64
PERLND	65
IMPLND	64
RCHRES	61
COPY	103

PERLND	11
PERLND	12
PERLND	13
PERLND	14
PERLND	15
PERLND	16
PERLND	17
PERLND	18
PERLND	19
IMPLND	14
RCHRES	2
RCHRES	3
RCHRES	4
RCHRES	5
RCHRES	6
RCHRES	7
RCHRES	8
RCHRES	9
RCHRES	10
RCHRES	11
RCHRES	12
RCHRES	13
RCHRES	14
RCHRES	15
RCHRES	16
REPORT	1
REPORT	3
REPORT	5
REPORT	6
REPORT	11
REPORT	13
REPORT	15
REPORT	16
REPORT	21
REPORT	23
REPORT	25
REPORT	26
REPORT	100
COPY	104
COPY	105
COPY	106
COPY	1
COPY	2
COPY	3
COPY	4

END OPN SEQUENCE



REPORT

REPORT-FLAGS

Rept-opn\*\*\*

***	x	-	x	REPT	NCON	NSRC	FORM	CWID	PWID	PLIN	PCOD	PYR
	1			91	9	7	2	12	1000	1000	5	12
	3			93	9	7	2	12	1000	1000	5	12
	5			95	9	7	2	12	1000	1000	5	12
	6			96	9	7	2	12	1000	1000	5	12
	11			81	9	7	1	12	1000	1000	5	12
	13			83	9	7	1	12	1000	1000	5	12
	15			85	9	7	1	12	1000	1000	5	12
	16			86	9	7	1	12	1000	1000	5	12
	21			71	9	7	2	12	1000	1000	5	12
	23			73	9	7	2	12	1000	1000	5	12
	25			75	9	7	2	12	1000	1000	5	12
	26			76	9	7	2	12	1000	1000	5	12
	100			51	40	19	1	12	1000	1000	5	12

END REPORT-FLAGS

REPORT-TITLE

Rept-opn\*\*\*

***	x	-	x	<-----title----->
	1			Land Surface total-loads
	3			Land Surface total-loads
	5			Land Surface total-loads
	6			Land Surface total-loads
	11			Land Surface total-loads
	13			Land Surface total-loads
	15			Land Surface total-loads
	16			Land Surface total-loads
	21			Land Surface total-loads
	23			Land Surface total-loads
	25			Land Surface total-loads
	26			Land Surface total-loads
	100			Instream Process Fluxes

END REPORT-TITLE

REPORT-SRC

Rept-opn\*\*\*

***	x	-	x	<----source-name---->
	1			Agric
	1			Forest
	1			Range
	1			Urban P
	1			Wetland
	1			RIBs
	1			Impervious
	3			Agric
	3			Forest
	3			Range
	3			Urban P
	3			Wetland
	3			RIBs
	3			Impervious
	5			Agric
	5			Forest
	5			Range

5 Urban P  
5 Wetland  
5 RIBs  
5 Impervious  
6 Agric  
6 Forest  
6 Range  
6 Urban P  
6 Wetland  
6 RIBs  
6 Impervious  
11 Agric  
11 Forest  
11 Range  
11 Urban P  
11 Wetland  
11 RIBs  
11 Impervious  
13 Agric  
13 Forest  
13 Range  
13 Urban P  
13 Wetland  
13 RIBs  
13 Impervious  
15 Agric  
15 Forest  
15 Range  
15 Urban P  
15 Wetland  
15 RIBs  
15 Impervious  
16 Agric  
16 Forest  
16 Range  
16 Urban P  
16 Wetland  
16 RIBs  
16 Impervious  
21 Agric  
21 Forest  
21 Range  
21 Urban P  
21 Wetland  
21 RIBs  
21 Impervious  
23 Agric  
23 Forest  
23 Range  
23 Urban P  
23 Wetland  
23 RIBs  
23 Impervious  
25 Agric  
25 Forest

25 Range  
 25 Urban P  
 25 Wetland  
 25 RIBs  
 25 Impervious  
 26 Agric  
 26 Forest  
 26 Range  
 26 Urban P  
 26 Wetland  
 26 RIBs  
 26 Impervious  
 100 Rch 31  
 100 Rch 41  
 100 Rch 51  
 100 Rch 61  
 100 Rch 2  
 100 Rch 3  
 100 Rch 4  
 100 Rch 5  
 100 Rch 6  
 100 Rch 7  
 100 Rch 8  
 100 Rch 9  
 100 Rch 10  
 100 Rch 11  
 100 Rch 12  
 100 Rch 13  
 100 Rch 14  
 100 Rch 15  
 100 Rch 16

END REPORT-SRC

REPORT-CON

Rept-opn\*\*\*

***	x	-	x<-----con-name----->	TRAN	SIGD	DECP
1			NH3	SUM	5	3
1			NO3	SUM	5	3
1			Organic N	SUM	5	3
1			Total N	SUM	5	3
1			PO4	SUM	5	3
1			Organic P	SUM	5	3
1			Total P	SUM	5	3
1			BOD	SUM	5	3
1			TOC	SUM	5	3
3			NH3	SUM	5	3
3			NO3	SUM	5	3
3			Organic N	SUM	5	3
3			Total N	SUM	5	3
3			PO4	SUM	5	3
3			Organic P	SUM	5	3
3			Total P	SUM	5	3
3			BOD	SUM	5	3
3			TOC	SUM	5	3
5			NH3	SUM	5	3
5			NO3	SUM	5	3

5	Organic N	SUM	5	3
5	Total N	SUM	5	3
5	PO4	SUM	5	3
5	Organic P	SUM	5	3
5	Total P	SUM	5	3
5	BOD	SUM	5	3
5	TOC	SUM	5	3
6	NH3	SUM	5	3
6	NO3	SUM	5	3
6	Organic N	SUM	5	3
6	Total N	SUM	5	3
6	PO4	SUM	5	3
6	Organic P	SUM	5	3
6	Total P	SUM	5	3
6	BOD	SUM	5	3
6	TOC	SUM	5	3
11	NH3	SUM	5	3
11	NO3	SUM	5	3
11	Organic N	SUM	5	3
11	Total N	SUM	5	3
11	PO4	SUM	5	3
11	Organic P	SUM	5	3
11	Total P	SUM	5	3
11	BOD	SUM	5	3
11	TOC	SUM	5	3
13	NH3	SUM	5	3
13	NO3	SUM	5	3
13	Organic N	SUM	5	3
13	Total N	SUM	5	3
13	PO4	SUM	5	3
13	Organic P	SUM	5	3
13	Total P	SUM	5	3
13	BOD	SUM	5	3
13	TOC	SUM	5	3
15	NH3	SUM	5	3
15	NO3	SUM	5	3
15	Organic N	SUM	5	3
15	Total N	SUM	5	3
15	PO4	SUM	5	3
15	Organic P	SUM	5	3
15	Total P	SUM	5	3
15	BOD	SUM	5	3
15	TOC	SUM	5	3
16	NH3	SUM	5	3
16	NO3	SUM	5	3
16	Organic N	SUM	5	3
16	Total N	SUM	5	3
16	PO4	SUM	5	3
16	Organic P	SUM	5	3
16	Total P	SUM	5	3
16	BOD	SUM	5	3
16	TOC	SUM	5	3
21	NH3	SUM	5	3
21	NO3	SUM	5	3
21	Organic N	SUM	5	3

21	Total N	SUM	5	3
21	PO4	SUM	5	3
21	Organic P	SUM	5	3
21	Total P	SUM	5	3
21	BOD	SUM	5	3
21	TOC	SUM	5	3
23	NH3	SUM	5	3
23	NO3	SUM	5	3
23	Organic N	SUM	5	3
23	Total N	SUM	5	3
23	PO4	SUM	5	3
23	Organic P	SUM	5	3
23	Total P	SUM	5	3
23	BOD	SUM	5	3
23	TOC	SUM	5	3
25	NH3	SUM	5	3
25	NO3	SUM	5	3
25	Organic N	SUM	5	3
25	Total N	SUM	5	3
25	PO4	SUM	5	3
25	Organic P	SUM	5	3
25	Total P	SUM	5	3
25	BOD	SUM	5	3
25	TOC	SUM	5	3
26	NH3	SUM	5	3
26	NO3	SUM	5	3
26	Organic N	SUM	5	3
26	Total N	SUM	5	3
26	PO4	SUM	5	3
26	Organic P	SUM	5	3
26	Total P	SUM	5	3
26	BOD	SUM	5	3
26	TOC	SUM	5	3
100	DO-Inflow	SUM	4	2
100	DO-Reaeration	SUM	4	2
100	DO-BOD Decay	SUM	4	2
100	DO-Benthal demand	SUM	4	2
100	DO-Nitrification	SUM	4	2
100	DO-Phyto. growth	SUM	4	2
100	BOD-Inflow	SUM	4	2
100	BOD-Decay	SUM	4	2
100	BOD-Benthal release	SUM	4	2
100	BOD-Sink	SUM	4	2
100	BOD-Denitrification	SUM	4	2
100	BOD-Phyto. death	SUM	4	2
100	NH3-Inflow	SUM	4	2
100	NH3-Nitrification	SUM	4	2
100	NH3-Volatilization	SUM	4	2
100	NH3-Benthal release	SUM	4	2
100	NH3-BOD Decay	SUM	4	2
100	NH3-Phyto. growth	SUM	4	2
100	NO3-Inflow	SUM	4	2
100	NO3-Nitrification	SUM	4	2
100	NO3-Denitrification	SUM	4	2
100	NO3-BOD Decay	SUM	4	2

```

100    NO3-Phyto. growth    SUM    4    2
100    PO4-Inflow          SUM    4    2
100    PO4-Benthal release SUM    4    2
100    PO4-BOD Decay       SUM    4    2
100    PO4-Phyto. growth   SUM    4    2
100    PHY-Inflow         SUM    4    2
100    PHY-Sink           SUM    4    2
100    PHY-Death          SUM    4    2
100    PHY-Growth         SUM    4    2
100    ORN-Inflow         SUM    4    2
100    ORN-Sink           SUM    4    2
100    ORN-Phyto. death   SUM    4    2
100    ORP-Inflow         SUM    4    2
100    ORP-Sink           SUM    4    2
100    ORP-Phyto. death   SUM    4    2
100    ORC-Inflow         SUM    4    2
100    ORC-Sink           SUM    4    2
100    ORC-Phyto. death   SUM    4    2
END REPORT-CON

```

REPORT-SUMM

Rept-opn\*\*\*

```

*** x - x<--src-sum-header--> STRN <--tim-sum-header--> TTRN STTR
   1      Total Load          SUM Average          AVER    1
   3      Total Load          SUM Average          AVER    1
   5      Total Load          SUM Average          AVER    1
   6      Total Load          SUM Average          AVER    1
  11      Per acre Load      SUM Average          AVER    1
  13      Per acre Load      SUM Average          AVER    1
  15      Per acre Load      SUM Average          AVER    1
  16      Per acre Load      SUM Average          AVER    1
  21      Percent Load       PCT Average          AVER    1
  23      Percent Load       PCT Average          AVER    1
  25      Percent Load       PCT Average          AVER    1
  26      Percent Load       PCT Average          AVER    1
 100                                SUM Average          AVER    1

```

END REPORT-SUMM

END REPORT

PERLND

ACTIVITY

```

<PLS >                Active Sections                ***
x - x ATMP SNOW PWAT  SED  PST  PWG PQAL MSTL PEST NITR PHOS TRAC ***
11  65  1          1          1  1  1  1
END ACTIVITY

```

PRINT-INFO

```

<PLS> ***** Print-flags ***** PIVL  PYR
x - x ATMP SNOW PWAT  SED  PST  PWG PQAL MSTL PEST NITR PHOS TRAC *****
11  65  5          5          5  5  5
END PRINT-INFO

```

GEN-INFO

<PLS >		Name	Unit-systems		Printer***
x	-	x	t-series		Engl Metr***
			in	out	***
11		AGRICULTURE- CENTRAL	1	1	90
12		FOREST- CENTRAL	1	1	90
13		RANGELAND	1	1	90
14		URBAN	1	1	90
15		WETLAND	1	1	90
16		WETLAND-AQ Q RCH 4,6	1	1	90
17		WETLAND-AQ Q RCH 14	1	1	90
18		WETLAND-AQ Q 8,15,16	1	1	90
19		RIBS	1	1	90
31		AGRICULTURE- UPPER RC	1	1	90
32		FOREST	1	1	90
33		RANGELAND	1	1	90
34		URBAN	1	1	90
35		WETLAND	1	1	90
39		RIBS	1	1	90
51		AGRICULTURE- WHIT	1	1	90
52		FOREST	1	1	90
53		RANGELAND	1	1	90
54		URBAN	1	1	90
55		WETLAND	1	1	90
59		RIBS	1	1	90
61		AGRICULTURE- DAV	1	1	90
62		FOREST	1	1	90
63		RANGELAND	1	1	90
64		URBAN	1	1	90
65		WETLAND	1	1	90

END GEN-INFO

PWAT-PARM1

*** <PLS >		Flags											
*** x	-	x	CSNO	RTOP	UZFG	VCS	VUZ	VNN	VIFW	VIRC	VLE	IFFC	HWT
11			0	1	1	0	0	0	0	0	1	0	0
12			0	1	1	0	0	0	0	0	1	0	0
13			0	1	1	0	0	0	0	0	1	0	0
14			0	1	1	0	0	0	0	0	1	0	0
15			0	1	1	0	0	0	0	0	1	0	0
16			0	1	1	0	0	0	0	0	1	0	0
17			0	1	1	0	0	0	0	0	1	0	0
18			0	1	1	0	0	0	0	0	1	0	0
19			0	1	1	0	0	0	0	0	0	0	0
31			0	1	1	0	0	0	0	0	1	0	0
32			0	1	1	0	0	0	0	0	1	0	0
33			0	1	1	0	0	0	0	0	1	0	0
34			0	1	1	0	0	0	0	0	1	0	0
35			0	1	1	0	0	0	0	0	1	0	0
39			0	1	1	0	0	0	0	0	0	0	0
51			0	1	1	0	0	0	0	0	1	0	0
52			0	1	1	0	0	0	0	0	1	0	0
53			0	1	1	0	0	0	0	0	1	0	0
54			0	1	1	0	0	0	0	0	1	0	0
55			0	1	1	0	0	0	0	0	1	0	0

59	0	1	1	0	0	0	0	0	0	0
61	0	1	1	0	0	0	0	1	0	0
62	0	1	1	0	0	0	0	1	0	0
63	0	1	1	0	0	0	0	1	0	0
64	0	1	1	0	0	0	0	1	0	0
65	0	1	1	0	0	0	0	1	0	0

END PWAT-PARM1

PWAT-PARM2

*** <PLS>	FOREST	LZSN	INFILT	LSUR	SLSUR	KVARY	AGWRC
*** x - x		(in)	(in/hr)	(ft)	(ft/ft)	(1/in)	(1/day)
11	0.0	2.000	0.100	1252.9	0.008	0.000	0.970
12	0.0	2.000	0.250	855.2	0.005	0.000	0.970
13	0.0	2.000	0.250	1182.0	0.011	0.000	0.970
14	0.0	2.000	0.070	1144.8	0.007	0.000	0.970
15	0.0	1.500	0.250	943.8	0.004	0.000	0.970
16	0.0	1.500	0.250	943.8	0.004	0.000	0.970
17	0.0	1.500	0.250	943.8	0.004	0.000	0.970
18	0.0	1.500	0.250	943.8	0.004	0.000	0.970
19	0.0	2.000	0.250	100.0	0.001	0.000	0.970
31	0.0	2.000	0.200	795.3	0.014	0.000	0.970
32	0.0	2.000	0.250	1372.0	0.028	0.000	0.970
33	0.0	2.000	0.250	1147.1	0.020	0.000	0.970
34	0.0	2.000	0.070	1223.6	0.016	0.000	0.970
35	0.0	1.500	0.250	690.7	0.004	0.000	0.970
39	0.0	2.000	0.250	100.0	0.001	0.000	0.970
51	0.0	2.000	0.200	481.9	0.013	0.000	0.970
52	0.0	2.000	0.250	433.0	0.026	0.000	0.970
53	0.0	2.000	0.250	1937.8	0.028	0.000	0.970
54	0.0	2.000	0.070	1311.2	0.031	0.000	0.970
55	0.0	1.500	0.250	510.7	0.004	0.000	0.970
59	0.0	2.000	0.250	100.0	0.001	0.000	0.970
61	0.0	2.000	0.100	792.0	0.016	0.000	0.970
62	0.0	2.000	0.250	318.6	0.016	0.000	0.970
63	0.0	2.000	0.250	847.8	0.015	0.000	0.970
64	0.0	2.000	0.070	642.1	0.010	0.000	0.970
65	0.0	1.500	0.250	662.2	0.005	0.000	0.970

END PWAT-PARM2

PWAT-PARM3

*** <PLS>	PETMAX	PETMIN	INFEXP	INFILD	DEEPPFR	BASETP	AGWETP
*** x - x	(deg F)	(deg F)					
11	40.0	35.0	2.0	2.0	0.500	0.000	0.000
12	40.0	35.0	2.0	2.0	0.500	0.000	0.000
13	40.0	35.0	2.0	2.0	0.500	0.000	0.000
14	40.0	35.0	2.0	2.0	0.500	0.000	0.000
15	40.0	35.0	2.0	2.0	0.400	0.000	0.100
16	40.0	35.0	2.0	2.0	0.400	0.000	0.100
17	40.0	35.0	2.0	2.0	0.400	0.000	0.100
18	40.0	35.0	2.0	2.0	0.400	0.000	0.100
19	40.0	35.0	2.0	2.0	0.500	0.000	0.000
31	40.0	35.0	2.0	2.0	0.500	0.000	0.000
32	40.0	35.0	2.0	2.0	0.500	0.000	0.000
33	40.0	35.0	2.0	2.0	0.500	0.000	0.000
34	40.0	35.0	2.0	2.0	0.500	0.000	0.000



35	40.0	35.0	2.0	2.0	0.400	0.000	0.100
39	40.0	35.0	2.0	2.0	0.500	0.000	0.000
51	40.0	35.0	2.0	2.0	0.500	0.000	0.000
52	40.0	35.0	2.0	2.0	0.500	0.000	0.000
53	40.0	35.0	2.0	2.0	0.500	0.000	0.000
54	40.0	35.0	2.0	2.0	0.500	0.000	0.000
55	40.0	35.0	2.0	2.0	0.400	0.000	0.100
59	40.0	35.0	2.0	2.0	0.500	0.000	0.000
61	40.0	35.0	2.0	2.0	0.500	0.000	0.000
62	40.0	35.0	2.0	2.0	0.500	0.000	0.000
63	40.0	35.0	2.0	2.0	0.500	0.000	0.000
64	40.0	35.0	2.0	2.0	0.500	0.000	0.000
65	40.0	35.0	2.0	2.0	0.400	0.000	0.100

END PWAT-PARM3

PWAT-PARM4

*** <PLS >	CEPSC	UZSN	NSUR	INTFW	IRC	LZETP
*** x - x	(in)	(in)			(1/day)	
11	0.080	0.200	0.20	0.500	0.800	0.600
12	0.100	0.560	0.35	0.600	0.800	0.600
13	0.050	0.320	0.15	0.500	0.800	0.600
14	0.050	0.320	0.10	0.500	0.800	0.600
15	0.200	0.350	0.35	0.700	0.800	0.600
16	0.200	0.350	0.35	0.700	0.800	0.600
17	0.200	0.350	0.35	0.700	0.800	0.600
18	0.200	0.350	0.35	0.700	0.800	0.600
19	0.000	0.700	0.10	0.600	0.800	0.500
31	0.080	0.200	0.20	1.000	0.900	0.600
32	0.100	0.560	0.35	1.000	0.900	0.600
33	0.050	0.320	0.15	1.000	0.900	0.600
34	0.050	0.320	0.10	1.000	0.900	0.600
35	0.200	0.350	0.35	1.000	0.900	0.600
39	0.000	0.700	0.10	1.000	0.900	0.500
51	0.080	0.200	0.20	1.000	0.900	0.600
52	0.100	0.560	0.35	1.000	0.900	0.600
53	0.050	0.320	0.15	1.000	0.900	0.600
54	0.050	0.320	0.10	1.000	0.900	0.600
55	0.200	0.350	0.35	1.000	0.900	0.600
59	0.000	0.700	0.10	1.000	0.900	0.500
61	0.080	0.200	0.20	0.500	0.800	0.600
62	0.100	0.560	0.35	0.600	0.800	0.600
63	0.050	0.320	0.15	0.500	0.800	0.600
64	0.050	0.320	0.10	0.500	0.800	0.600
65	0.200	0.350	0.35	0.700	0.800	0.600

END PWAT-PARM4

MON-LZETPARM

*** <PLS >	Lower zone evapotransp parameter at start of each month											
11	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
12	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
13	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
14	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
15	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
16	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
17	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
18	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5

31	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
32	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
33	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
34	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
35	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
51	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
52	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
53	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
54	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
55	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5
61	.1	.2	.8	.8	.8	.8	.8	.8	.8	.8	.6	.1
62	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
63	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
64	.2	.3	.8	.8	.8	.8	.8	.8	.8	.8	.6	.2
65	.5	.6	.8	.8	.8	.8	.8	.8	.8	.8	.6	.5

END MON-LZETPARM

PWAT-STATE1

\*\*\* <PLS> PWATER state variables (in)

*** x - x	CEPS	SURS	UZS	IFWS	LZS	AGWS	GWVS
11	0.0	0.0	0.408	0.001	3.21	0.712	0.0
12	0.0	0.0	0.778	0.001	3.09	0.704	0.0
13	0.0	0.0	0.407	0.001	2.95	0.734	0.0
14	0.0	0.0	0.405	0.001	2.74	0.49	0.0
15	0.0	0.0	0.582	0.001	2.35	0.749	0.0
16	0.0	0.0	0.582	0.001	2.35	0.749	0.0
17	0.0	0.0	0.582	0.001	2.35	0.749	0.0
18	0.0	0.0	0.582	0.001	2.35	0.749	0.0
19	0.0	0.0	0.703	0.001	2.6	0.974	0.0
31	0.0	0.0	0.401	0.001	3.38	0.818	0.0
32	0.0	0.0	0.886	0.001	3.28	0.683	0.0
33	0.0	0.0	0.407	0.001	3	0.715	0.0
34	0.0	0.0	0.514	0.001	2.84	0.455	0.0
35	0.0	0.0	0.661	0.001	2.55	0.721	0.0
39	0.0	0.0	0.724	0.001	2.68	1.013	0.0
51	0.0	0.0	0.04	0.001	1.70	0.18	0.0
52	0.0	0.0	0.03	0.001	0.40	0.09	0.0
53	0.0	0.0	0.01	0.001	0.33	0.09	0.0
54	0.0	0.0	0.01	0.001	0.37	0.07	0.0
55	0.0	0.0	0.02	0.001	0.32	0.02	0.0
59	0.0	0.0	0.02	0.001	0.81	0.17	0.0
61	0.0	0.0	0.407	0.001	3.20	0.707	0.0
62	0.0	0.0	0.858	0.001	3.19	0.785	0.0
63	0.0	0.0	0.442	0.001	3.03	0.825	0.0
64	0.0	0.0	0.502	0.001	2.75	0.489	0.0
65	0.0	0.0	0.618	0.001	2.45	0.861	0.0

END PWAT-STATE1

PSTEMP-PARM1

\*\*\* <PLS > Flags for section PSTEMP

\*\*\* x - x SLTV ULTV LGTV TSOP

11	1	1	1	1
12	1	1	1	1
13	1	1	1	1
14	1	1	1	1
15	1	1	1	1
16	1	1	1	1
17	1	1	1	1
18	1	1	1	1
19	1	1	1	1
31	1	1	1	1
32	1	1	1	1
33	1	1	1	1
34	1	1	1	1
35	1	1	1	1
39	1	1	1	1
51	1	1	1	1
52	1	1	1	1
53	1	1	1	1
54	1	1	1	1
55	1	1	1	1
59	1	1	1	1
61	1	1	1	1
62	1	1	1	1
63	1	1	1	1
64	1	1	1	1
65	1	1	1	1

END PSTEMP-PARM1

PSTEMP-PARM2

\*\*\* <PLS > ASLT BSLT ULTP1 ULTP2 LGTP1 LGTP2

\*\*\* x - x (deg F) (degF/F) (degF/F) (deg F)

	ASLT (deg F)	BSLT (degF/F)	ULTP1	ULTP2 (degF/F)	LGTP1	LGTP2 (deg F)
11	32.0	1.00	32.0	1.0	60.8	
12	32.0	1.00	32.0	1.0	60.8	
13	32.0	1.00	32.0	1.0	60.8	
14	32.0	1.00	32.0	1.0	60.8	
15	32.0	1.00	32.0	1.0	60.8	
16	32.0	1.00	32.0	1.0	60.8	
17	32.0	1.00	32.0	1.0	60.8	
18	32.0	1.00	32.0	1.0	60.8	
19	32.0	1.00	32.0	1.0	60.8	
31	32.0	1.00	32.0	1.0	60.8	
32	32.0	1.00	32.0	1.0	60.8	
33	32.0	1.00	32.0	1.0	60.8	
34	32.0	1.00	32.0	1.0	60.8	
35	32.0	1.00	32.0	1.0	60.8	
39	32.0	1.00	32.0	1.0	60.8	
51	32.0	1.00	32.0	1.0	60.8	
52	32.0	1.00	32.0	1.0	60.8	
53	32.0	1.00	32.0	1.0	60.8	
54	32.0	1.00	32.0	1.0	60.8	
55	32.0	1.00	32.0	1.0	60.8	
59	32.0	1.00	32.0	1.0	60.8	

61	32.0	1.00	32.0	1.0	60.8
62	32.0	1.00	32.0	1.0	60.8
63	32.0	1.00	32.0	1.0	60.8
64	32.0	1.00	32.0	1.0	60.8
65	32.0	1.00	32.0	1.0	60.8

END PSTEMP-PARM2

MON-ASLT

\*\*\* <PLS > Value of ASLT at start of each month (deg F)

\*\*\* x - x

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
12	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
13	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
14	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
15	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
16	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
17	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
18	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
19	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
31	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
32	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
33	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
34	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
35	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
39	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
51	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
52	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
53	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
54	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
55	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
59	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
61	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
62	33.0	33.0	35.0	41.0	52.0	54.0	55.0	55.0	53.0	47.0	40.0	35.0
63	29.0	29.0	30.0	34.0	54.0	60.0	60.0	60.0	58.0	40.0	35.0	30.0
64	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0
65	30.0	30.0	32.0	38.0	52.0	57.0	58.0	57.0	55.0	42.0	36.0	32.0

END MON-ASLT

MON-BSLT

\*\*\* <PLS > Value of BSLT at start of each month (deg F/F)

\*\*\* x - x

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
12	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
13	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
14	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
15	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
16	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
17	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
18	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
19	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60

31	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
32	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
33	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
34	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
35	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
39	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
51	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
52	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
53	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
54	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
55	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
59	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
61	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
62	0.4	.40	.42	.50	.55	.60	.60	.60	.60	.55	.45	.42
63	.55	.55	.65	.70	.80	.80	.80	.75	.70	.65	.60	.60
64	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55
65	0.5	.50	.55	.65	.75	.75	.75	.75	.70	.65	.60	.55

END MON-BSLT

MON-ULTP1

\*\*\* <PLS > Value of ULTP1 at start of each month in deg F (TSOPFG=1)

*** x - x	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
12	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
13	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
14	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
15	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
16	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
17	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
18	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
19	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
31	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
32	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
33	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
34	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
35	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
39	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
51	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
52	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
53	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
54	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
55	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
59	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
61	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
62	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0
63	34.0	34.0	35.0	37.0	42.0	52.0	54.0	54.0	52.0	43.0	37.0	35.0
64	35.0	35.0	36.0	39.0	43.0	48.0	50.0	50.0	50.0	44.0	38.0	36.0
65	36.0	36.0	37.0	40.0	45.0	48.0	48.0	48.0	48.0	45.0	40.0	38.0

END MON-ULTP1

MON-ULTP2

\*\*\* <PLS > Value of ULTP2 at start of each month in Deg F/F (TSOPFG=1)

\*\*\* x - x

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
12	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
13	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
14	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
15	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
16	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
17	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
18	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
19	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
31	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
32	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
33	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
34	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
35	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
39	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
51	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
52	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
53	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
54	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
55	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
59	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
61	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
62	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25
63	0.3	0.3	.35	.45	.55	.65	0.7	0.7	0.7	.65	.55	.35
64	.25	.25	0.3	.40	0.5	.60	.65	.65	.65	.55	.45	.30
65	.22	.22	.25	.40	0.5	.55	.55	.55	.55	.50	.45	.25

END MON-ULTP2

MON-LGTP1

\*\*\* <PLS > Value of LGTP1 at start of each month in Deg F (TSOPFG=1)

\*\*\* x - x

	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
12	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
13	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
14	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
15	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
16	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
17	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
18	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
19	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
31	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
32	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
33	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
34	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
35	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
39	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0

51	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
52	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
53	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
54	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
55	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
59	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0

61	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
62	38.0	38.0	38.0	43.0	50.0	55.0	61.0	63.0	62.0	60.0	50.0	40.0
63	35.0	35.0	35.0	40.0	52.0	58.0	67.0	69.0	68.0	62.0	42.0	35.0
64	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0
65	38.0	38.0	38.0	42.0	50.0	62.0	66.0	67.0	65.0	55.0	45.0	40.0

END MON-LGTP1

PSTEMP-TEMPS

<PLS> Initial Conditions for Section PSTEMP \*\*\*

#	#	AIRTC	SLTMP	ULTMP	LGTMP	***
1	65	56.0	56.0	56.0	68.0	

END PSTEMP-TEMPS

PWT-PARM1

<PLS> Flags for Section PWTGAS \*\*\*

#	#	IDV	ICV	GDV	GCV	***
11		1	0	1	0	
12		1	0	1	0	
13		1	0	1	0	
14		1	0	1	0	
15		1	0	1	0	
16		1	0	1	0	
17		1	0	1	0	
18		1	0	1	0	
19		1	0	1	0	
31		1	0	1	0	
32		1	0	1	0	
33		1	0	1	0	
34		1	0	1	0	
35		1	0	1	0	
39		1	0	1	0	
51		1	0	1	0	
52		1	0	1	0	
53		1	0	1	0	
54		1	0	1	0	
55		1	0	1	0	
59		1	0	1	0	
61		1	0	1	0	
62		1	0	1	0	
63		1	0	1	0	
64		1	0	1	0	
65		1	0	1	0	

END PWT-PARM1

PWT-PARM2

#	#	ELEV	IDOXP	ICO2P	ADOXP	ACO2P	***
11		80.00	6	0.00	4	0.00	
12		80.00	6	0.00	4	0.00	
13		80.00	6	0.00	4	0.00	
14		80.00	6	0.00	4	0.00	
15		80.00	6	0.00	4	0.00	
16		80.00	6	0.00	4	0.00	
17		80.00	6	0.00	4	0.00	
18		80.00	6	0.00	4	0.00	
19		80.00	6	0.00	4	0.00	
31		120.00	6	0.00	4	0.00	
32		120.00	6	0.00	4	0.00	
33		120.00	6	0.00	4	0.00	
34		120.00	6	0.00	4	0.00	
35		120.00	6	0.00	4	0.00	
39		120.00	6	0.00	4	0.00	
51		110.00	6	0.00	4	0.00	
52		110.00	6	0.00	4	0.00	
53		110.00	6	0.00	4	0.00	
54		110.00	6	0.00	4	0.00	
55		110.00	6	0.00	4	0.00	
59		110.00	6	0.00	4	0.00	
61		100.00	6	0.00	4	0.00	
62		100.00	6	0.00	4	0.00	
63		100.00	6	0.00	4	0.00	
64		100.00	6	0.00	4	0.00	
65		100.00	6	0.00	4	0.00	

END PWT-PARM2

MON-IFWDOX

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11	65	8.0	8.0	7.5	7.0	6.5	6.0	6.0	6.0	6.5	7.0	7.5	8.0	

END MON-IFWDOX

MON-GRNDDOX

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11	65	6.0	6.0	5.5	5.0	4.0	4.0	4.0	4.0	4.5	5.0	5.5	6.0	

END MON-GRNDDOX

PWT-GASES

#	#	SODOX	SOCO2	IODOX	IOCO2	AODOX	AOCO2	***
1	65	10.0	0.0	8.0	0.0	6.0	0.0	

END PWT-GASES

NQUALS

\*\*\* NQAL - NH3, NO2+NO3, ORTHO P, AND BOD \*\*\*

#	#	NQAL	***
1	65	4	

END NQUALS



PQL-AD-FLAGS

Atmospheric Deposition Flags \*\*\*

<PLS >		QUAL1		QUAL2		QUAL3		QUAL4		***
#	- #	F	C	F	C	F	C	F	C	***
11		-1	0	-1	0	0	0	0	0	
12		-1	0	-1	0	0	0	0	0	
13		-1	0	-1	0	0	0	0	0	
14		-1	0	-1	0	0	0	0	0	
15		-1	0	-1	0	0	0	0	0	
16		-1	0	-1	0	0	0	0	0	
17		-1	0	-1	0	0	0	0	0	
18		-1	0	-1	0	0	0	0	0	
19		-1	0	-1	0	0	0	0	0	
31		-1	0	-1	0	0	0	0	0	
32		-1	0	-1	0	0	0	0	0	
33		-1	0	-1	0	0	0	0	0	
34		-1	0	-1	0	0	0	0	0	
35		-1	0	-1	0	0	0	0	0	
39		-1	0	-1	0	0	0	0	0	
51		-1	0	-1	0	0	0	0	0	
52		-1	0	-1	0	0	0	0	0	
53		-1	0	-1	0	0	0	0	0	
54		-1	0	-1	0	0	0	0	0	
55		-1	0	-1	0	0	0	0	0	
59		-1	0	-1	0	0	0	0	0	
61		-1	0	-1	0	0	0	0	0	
62		-1	0	-1	0	0	0	0	0	
63		-1	0	-1	0	0	0	0	0	
64		-1	0	-1	0	0	0	0	0	
65		-1	0	-1	0	0	0	0	0	

END PQL-AD-FLAGS

QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	NH3	LBS	0	0	0	1	1	1	3	1	3	
12	NH3	LBS	0	0	0	1	1	1	3	1	3	
13	NH3	LBS	0	0	0	1	1	1	3	1	3	
14	NH3	LBS	0	0	0	1	1	1	3	1	3	
15	NH3	LBS	0	0	0	1	1	1	3	1	3	
16	NH3	LBS	0	0	0	1	1	1	3	1	3	
17	NH3	LBS	0	0	0	1	1	1	3	1	3	
18	NH3	LBS	0	0	0	1	1	1	3	1	3	
19	NH3	LBS	0	0	0	1	1	1	3	1	3	
31	NH3	LBS	0	0	0	1	1	1	3	1	3	
32	NH3	LBS	0	0	0	1	1	1	3	1	3	
33	NH3	LBS	0	0	0	1	1	1	3	1	3	
34	NH3	LBS	0	0	0	1	1	1	3	1	3	
35	NH3	LBS	0	0	0	1	1	1	3	1	3	
39	NH3	LBS	0	0	0	1	1	1	3	1	3	
51	NH3	LBS	0	0	0	1	1	1	3	1	3	
52	NH3	LBS	0	0	0	1	1	1	3	1	3	
53	NH3	LBS	0	0	0	1	1	1	3	1	3	
54	NH3	LBS	0	0	0	1	1	1	3	1	3	
55	NH3	LBS	0	0	0	1	1	1	3	1	3	
59	NH3	LBS	0	0	0	1	1	1	3	1	3	

61	NH3	LBS	0	0	0	1	1	1	3	1	3
62	NH3	LBS	0	0	0	1	1	1	3	1	3
63	NH3	LBS	0	0	0	1	1	1	3	1	3
64	NH3	LBS	0	0	0	1	1	1	3	1	3
65	NH3	LBS	0	0	0	1	1	1	3	1	3

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.004				.012	0.5			
12		.002				.004	0.5			
13		.004				.012	0.5			
14		.004				.012	0.5			
15		.002				.004	0.5			
16		.002				.004	0.5			
17		.002				.004	0.5			
18		.002				.004	0.5			
19		.004				.012	0.5			
31		.004				.012	0.5			
32		.002				.004	0.5			
33		.004				.012	0.5			
34		.004				.012	0.5			
35		.002				.004	0.5			
39		.004				.012	0.5			
51		.004				.012	0.5			
52		.002				.004	0.5			
53		.004				.012	0.5			
54		.004				.012	0.5			
55		.002				.004	0.5			
59		.004				.012	0.5			
61		.004				.012	0.5			
62		.002				.004	0.5			
63		.004				.012	0.5			
64		.004				.012	0.5			
65		.002				.004	0.5			

END QUAL-INPUT

MON-ACCUM

ACCUMULATION RATE OF NH4 (lb NH4-N/AC.DAY)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
12		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
13		.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	
14		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
15	18	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
19		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
31		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
32		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
33		.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	
34		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
35		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
39		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	

51	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
52	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
53	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
54	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008
55	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
59	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
61	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
62	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
63	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006	.006
64	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008
65	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002

END MON-ACCUM

MON-SQOLIM

STORAGE LIMIT OF NH4 (lb NH4-N/AC)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
12		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
13		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
14		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
15	18	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
19		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
31		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
32		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
33		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
34		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
35		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
39		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
51		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
52		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
53		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
54		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
55		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
59		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
61		.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	.040	
62		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	
63		.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	.024	
64		.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	.032	
65		.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	.008	

END MON-SQOLIM

MON-IFLW-CONC

		Interflow Concentration of NH4-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
12		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
13		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
14		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
15	18	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
19		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
31		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
32		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
33		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
34		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
35		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
39		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
51		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
52		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
53		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
54		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
55		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
59		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
61		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
62		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
63		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
64		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
65		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	

END MON-IFLW-CONC

MON-GRND-CONC

		Active Groundwater Concentration of NH4-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
12		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
13		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
14		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
15	18	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
19		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
31		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
32		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
33		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
34		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
35		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
39		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
51		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
52		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	
53		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
54		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	
55		.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	.030	
59		.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	.100	

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61      .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100
62      .020 .020 .020 .020 .020 .020 .020 .020 .020 .020 .020 .020
63      .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100
64      .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100 .100
65      .030 .030 .030 .030 .030 .030 .030 .030 .030 .030 .030 .030
END MON-GRND-CONC

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QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
12	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
13	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
14	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
15	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
16	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
17	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
18	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
19	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
31	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
32	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
33	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
34	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
35	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
39	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
51	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
52	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
53	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
54	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
55	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
59	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
61	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
62	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
63	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
64	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	
65	NO2 NO3	LBS	0	0	0	1	1	1	3	1	3	

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.040				.120	.5			
12		.005				.010	.5			
13		.040				.120	.5			
14		.040				.120	.5			
15	18	.005				.010	.5			
19		.040				.120	.5			
31		.040				.120	.5			
32		.005				.010	.5			
33		.040				.120	.5			
34		.040				.120	.5			
35		.005				.010	.5			
39		.040				.120	.5			

51	.040	.480	.5
52	.005	.100	.5
53	.040	.480	.5
54	.040	.480	.5
55	.005	.100	.5
59	.040	.480	.5
61	.040	.480	.5
62	.005	.100	.5
63	.040	.480	.5
64	.040	.480	.5
65	.005	.100	.5

END QUAL-INPUT

MON-ACCUM

		ACCUMULATION RATE												NO2 NO3 (lb NO3-N/AC.DAY)		***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***		
11		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1		
12		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050		
13		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05		
14		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03		
15	180	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020		
19		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
31		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1		
32		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050		
33		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05		
34		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03		
35		0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020		
39		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
51		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1		
52		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050		
53		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05		
54		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03		
55		0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020		
59		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
61		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1		
62		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050		
63		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05		
64		0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03	0.03		
65		0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020	0.0020		

END MON-ACCUM

MON-SQOLIM

		STORAGE LIMIT OF												NO2 NO3 (lb NO3-N/AC)		***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***		
11		0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20		
12		.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010		
13		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10		
14		0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06		
15	18	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004		
19		.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020		

31	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
32	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010
33	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
34	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
35	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
39	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
51	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
52	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010
53	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
54	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
55	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
59	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020	.020
61	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20	0.20
62	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010	.010
63	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10
64	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
65	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004

END MON-SQOLIM

MON-IFLW-CONC

		Interflow Concentration of NO3-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
12		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
13		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
14		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
15	18	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	
19		5	5	5	5	5	5	5	5	5	5	5	5	
31		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
32		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
33		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
34		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
39		5	5	5	5	5	5	5	5	5	5	5	5	
51		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
52		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
53		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
54		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
59		5	5	5	5	5	5	5	5	5	5	5	5	
61		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
62		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
63		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
64		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
65		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	

END MON-IFLW-CONC

MON-GRND-CONC

		Active Groundwater Concentration of NO3-N (mg/l)												***
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
12		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
13		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
14		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
15		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
16		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
17		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
18		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
19		5	5	5	5	5	5	5	5	5	5	5	5	
31		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
32		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
33		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
34		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
39		5	5	5	5	5	5	5	5	5	5	5	5	
51		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
52		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
53		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
54		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	
59		5	5	5	5	5	5	5	5	5	5	5	5	
61		0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	0.3	
62		0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	
63		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
64		0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	0.15	
65		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	

END MON-GRND-CONC

QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
12	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
13	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
14	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
15	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
16	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
17	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
18	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
19	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
31	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
32	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
33	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
34	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
35	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	
39	ORTHO P	LBS	0	0	0	1	1	1	3	1	3	



51	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
52	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
53	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
54	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
55	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
59	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
61	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
62	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
63	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
64	ORTHO P	LBS	0	0	0	1	1	1	3	1	3
65	ORTHO P	LBS	0	0	0	1	1	1	3	1	3

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.004				.012	.5			
12		.002				.004	.5			
13		.004				.012	.5			
14		.004				.012	.5			
15	18	.002				.004	.5			
19		.004				.012	.5			
31		.004				.012	.5			
32		.002				.004	.5			
33		.004				.012	.5			
34		.004				.012	.5			
35		.002				.004	.5			
39		.004				.012	.5			
51		.004				.012	.5			
52		.002				.004	.5			
53		.004				.012	.5			
54		.004				.012	.5			
55		.002				.004	.5			
59		.004				.012	.5			
61		.004				.012	.5			
62		.002				.004	.5			
63		.004				.012	.5			
64		.004				.012	.5			
65		.002				.004	.5			

END QUAL-INPUT

MON-ACCUM

ACCUMULATION RATE OF PO4 (lb PO4-P/AC.DAY)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
12		.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
13		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
14		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
15	18	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	
19		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	

31	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
32	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
33	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
34	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
35	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
39	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
51	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
52	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
53	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
54	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
55	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
59	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
61	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
62	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002
63	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
64	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004
65	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002	.002

END MON-ACCUM

MON-SQOLIM

STORAGE LIMIT OF PO4 (lb PO4-P/AC)													***	
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
12		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
13		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
14		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
15	18	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
19		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
31		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
32		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
33		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
34		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
35		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
39		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
51		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
52		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
53		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
54		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
55		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
59		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
61		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
62		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	
63		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
64		.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	.012	
65		.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	.004	

END MON-SQOLIM

MON-IFLW-CONC

Interflow Concentration of PO4-P (mg/l)

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#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
12		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
13		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
14		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
15	18	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
19		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
31		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
32		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
33		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
34		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
39		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
51		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
52		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
53		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
54		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
59		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
61		0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06	0.06
62		0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120	0.0120
63		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050
64		0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08	0.08
65		0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050	0.0050

\*\*\*

END MON-IFLW-CONC

MON-GRND-CONC

Active Groundwater Concentration of PO4-P (mg/l)

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#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC
11		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
12		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
13		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
14		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
15	18	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
19		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
31		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
32		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
33		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
34		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
35		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
39		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
51		0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12	0.12
52		0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250	0.0250
53		0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1	0.1
54		0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16	0.16
55		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
59		0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01

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61 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.06  
 62 0.0120.0120.0120.0120.0120.0120.0120.0120.0120.0120.0120.0120.012  
 63 0.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.005  
 64 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08 0.08  
 65 0.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.0050.005  
 END MON-GRND-CONC

QUAL-PROPS

#	#<--QUALID-->	QTID	QSD	VPFW	VPFS	QSO	VQO	QIFW	VIQC	QAGW	VAQC	***
11	BOD	LBS	0	0	0	1	1	1	3	1	3	
12	BOD	LBS	0	0	0	1	1	1	3	1	3	
13	BOD	LBS	0	0	0	1	1	1	3	1	3	
14	BOD	LBS	0	0	0	1	1	1	3	1	3	
15	BOD	LBS	0	0	0	1	1	1	3	1	3	
16	BOD	LBS	0	0	0	1	1	1	3	1	3	
17	BOD	LBS	0	0	0	1	1	1	3	1	3	
18	BOD	LBS	0	0	0	1	1	1	3	1	3	
19	BOD	LBS	0	0	0	1	1	1	3	1	3	
31	BOD	LBS	0	0	0	1	1	1	3	1	3	
32	BOD	LBS	0	0	0	1	1	1	3	1	3	
33	BOD	LBS	0	0	0	1	1	1	3	1	3	
34	BOD	LBS	0	0	0	1	1	1	3	1	3	
35	BOD	LBS	0	0	0	1	1	1	3	1	3	
39	BOD	LBS	0	0	0	1	1	1	3	1	3	
51	BOD	LBS	0	0	0	1	1	1	3	1	3	
52	BOD	LBS	0	0	0	1	1	1	3	1	3	
53	BOD	LBS	0	0	0	1	1	1	3	1	3	
54	BOD	LBS	0	0	0	1	1	1	3	1	3	
55	BOD	LBS	0	0	0	1	1	1	3	1	3	
59	BOD	LBS	0	0	0	1	1	1	3	1	3	
61	BOD	LBS	0	0	0	1	1	1	3	1	3	
62	BOD	LBS	0	0	0	1	1	1	3	1	3	
63	BOD	LBS	0	0	0	1	1	1	3	1	3	
64	BOD	LBS	0	0	0	1	1	1	3	1	3	
65	BOD	LBS	0	0	0	1	1	1	3	1	3	

END QUAL-PROPS

QUAL-INPUT

#	#	SQO	POTFW	POTFS	ACQOP	SQOLIM	WSQOP	IOQC	AOQC	***
11		.35				5.0	.5			
12		.15				.75	.5			
13		.35				5.0	.5			
14		.60				6.0	.5			
15	18	.15				1.5	.5			
19		.35				5.0	.5			
31		.35				5.0	.5			
32		.15				.75	.5			
33		.35				5.0	.5			
34		.60				6.0	.5			
35		.15				1.5	.5			
39		.35				5.0	.5			

51	.35	5.0	.5
52	.15	.75	.5
53	.35	5.0	.5
54	.60	6.0	.5
55	.15	1.5	.5
59	.35	5.0	.5
61	.35	5.0	.5
62	.15	.75	.5
63	.35	5.0	.5
64	.60	6.0	.5
65	.15	1.5	.5

END QUAL-INPUT

MON-ACCUM

ACCUMULATION RATE FOR BOD/Organics (lb /AC.DAY) ***														
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
12		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
13		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
14		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
15	18	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
19		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
31		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
32		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
33		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
34		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
35		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
39		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
51		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
52		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
53		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
54		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
55		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	
59		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
61		0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	
62		0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	
63		0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	0.35	
64		0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	
65		0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	0.10	

END MON-ACCUM

MON-SQOLIM

STORAGE RATE FOR BOD/Organics (lb /AC) ***														
#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
12		.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	
13		0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	
14		0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	
15	18	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	
19		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	

31	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
32	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45
33	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
34	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
35	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20
39	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
51	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
52	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45
53	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
54	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
55	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20
59	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
61	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
62	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45	.45
63	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7	0.7
64	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6	0.6
65	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20	.20

END MON-SQOLIM

MON-IFLW-CONC

#	#	Interflow Concentration of BOD/Organics (mg/l) ***												***
		JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	
11		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
12		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
13		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
14		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
15	18	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
19		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
31		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
32		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
33		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
34		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
35		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
39		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
51		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
52		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
53		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
54		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
55		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
59		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
61		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
62		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
63		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
64		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
65		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	

END MON-IFLW-CONC

MON-GRND-CONC

Active Groundwater Concentration of BOD/Organics (mg/l) \*\*\*

#	#	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	***
11		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
12		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
13		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
14		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
15	18	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
19		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
31		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
32		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
33		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
34		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
35		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
39		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
51		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
52		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
53		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
54		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
55		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
59		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	
61		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
62		2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	2.0	
63		3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	3.0	
64		5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
65		1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	

END MON-GRND-CONC

END PERLND

IMPLND

ACTIVITY

#	#	ATMP	SNOW	IWAT	SLD	IWG	IQAL	***
14	64	1	0	1	0	1	1	

END ACTIVITY

PRINT-INFO

#	#	ATMP	SNOW	IWAT	SLD	IWG	IQAL	PIVL	PYR	***
14	64	5	0	5	0	5	5	1	12	

END PRINT-INFO

GEN-INFO

***	<ILS >	Name	Unit-systems		Printer	
***	<ILS >		t-series	Engl	Metr	
***	x - x		in	out		
	14	URBAN	1	1	90	0
	34	URBAN	1	1	90	0
	54	URBAN	1	1	90	0
	64	URBAN	1	1	90	0

END GEN-INFO

```

IWAT-PARM1
*** <ILS >      Flags
*** x - x CSNO RTOP  VRS  VNN  RTLI
    14      0    1    0    0    0
    34      0    1    0    0    0
    54      0    1    0    0    0
    64      0    1    0    0    0
END IWAT-PARM1

IWAT-PARM2
*** <ILS >      LRSUR      SLSUR      NSUR      RETSC
*** x - x      (ft)
    14      200.0    0.01015    0.015    0.05
    34      200.0    0.01015    0.015    0.05
    54      200.0    0.01015    0.015    0.05
    64      200.0    0.01015    0.015    0.05
END IWAT-PARM2

IWAT-PARM3
*** <ILS >      PETMAX      PETMIN
*** x - x      (deg F)      (deg F)
    14  64      40.0      35.0
END IWAT-PARM3

IWAT-STATE1
*** <ILS >  IWATER state variables (inches)
*** x - x      RETS      SURS
    14  64      0.0      0.0
END IWAT-STATE1

IWT-PARM1
#  # WTFV CSNO ***
    14  64  1  0
END IWT-PARM1

IWT-PARM2
#  #      ELEV      AWTF      BWTF ***
    14      80.00    34.0    0.3
    34      120.00   34.0    0.3
    54      110.00   34.0    0.3
    64      100.00   34.0    0.3
END IWT-PARM2

MON-AWTF
*** <ILS >  Values of AWTF at start of each month (oF)
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
    14  64 29.0 29.0 30.0 34.0 40.0 50.0 50.0 50.0 45.0 40.0 35.0 30.0
END MON-AWTF

MON-BWTF
*** <ILS >  Values of BWTF at start of each month (F/F)
*** x - x  JAN  FEB  MAR  APR  MAY  JUN  JUL  AUG  SEP  OCT  NOV  DEC
    14  64 .55 .55 .60 .60 .65 .65 .65 .65 .60 .55 .55 .55
END MON-BWTF

```



NQUALS

```

# # NQAL ***
14 64 4
END NQUALS

```

IQL-AD-FLAGS

```

      Atmospheric Deposition Flags ***
<ILS >  QUAL1  QUAL2  QUAL3  QUAL4  ***
# - #    F  C    F  C    F  C    F  C    ***
14      -1  0   -1  0    0  0    0  0
34      -1  0   -1  0    0  0    0  0
54      -1  0   -1  0    0  0    0  0
64      -1  0   -1  0    0  0    0  0
END IQL-AD-FLAGS

```

QUAL-PROPS

```

# #<--QUALID-->  QTID  QSD  VPFW  QSO  VQO  ***
14  NH3          LBS    0    0    1    0
34  NH3          LBS    0    0    1    0
54  NH3          LBS    0    0    1    0
64  NH3          LBS    0    0    1    0
END QUAL-PROPS

```

QUAL-INPUT

```

# #      SQO  POTFW  ACQOP  SQOLIM  WSQOP  ***
14      0.001    0  0.004  0.005    0.5
34      0.001    0  0.004  0.005    0.5
54      0.001    0  0.004  0.005    0.5
64      0.001    0  0.004  0.005    0.5
END QUAL-INPUT

```

QUAL-PROPS

```

# #<--QUALID-->  QTID  QSD  VPFW  QSO  VQO  ***
14  NO2 NO3      LBS    0    0    1    0
34  NO2 NO3      LBS    0    0    1    0
54  NO2 NO3      LBS    0    0    1    0
64  NO2 NO3      LBS    0    0    1    0
END QUAL-PROPS

```

QUAL-INPUT

```

# #      SQO  POTFW  ACQOP  SQOLIM  WSQOP  ***
14      0.007    0  0.006  0.009    0.5
34      0.007    0  0.006  0.009    0.5
54      0.007    0  0.006  0.009    0.5
64      0.007    0  0.006  0.009    0.5
END QUAL-INPUT

```

QUAL-PROPS

```

# #<--QUALID-->  QTID  QSD  VPFW  QSO  VQO  ***
14  ORTHO P      LBS    0    0    1    0
34  ORTHO P      LBS    0    0    1    0
54  ORTHO P      LBS    0    0    1    0
64  ORTHO P      LBS    0    0    1    0
END QUAL-PROPS

```

```

QUAL-INPUT
# # SQO POTFW ACQOP SQOLIM WSQOP ***
14 0.002 0 0.001 0.002 0.5
34 0.002 0 0.001 0.002 0.5
54 0.002 0 0.001 0.002 0.5
64 0.002 0 0.001 0.002 0.5
END QUAL-INPUT

```

```

QUAL-PROPS
# #<--QUALID--> QTID QSD VPFW QSO VQO ***
14 BOD LBS 0 0 1 0
34 BOD LBS 0 0 1 0
54 BOD LBS 0 0 1 0
64 BOD LBS 0 0 1 0
END QUAL-PROPS

```

```

QUAL-INPUT
# # SQO POTFW ACQOP SQOLIM WSQOP ***
14 1.0 0. 0.15 2.0 0.500
34 1.0 0. 0.15 2.0 0.500
54 1.0 0. 0.15 2.0 0.500
64 1.0 0. 0.15 2.0 0.500
END QUAL-INPUT
END IMPLND

```

```

RCHRES
ACTIVITY
*** RCHRES Active sections
*** x - x HYFG ADFG CNFG HTFG SDFG GQFG OXFG NUFG PKFG PHFG
1 61 1 1 0 0 0 0 1 1 1 0
END ACTIVITY

```

```

PRINT-INFO
*** RCHRES Printout level flags
*** x - x HYDR ADCA CONS HEAT SED GQL OXRX NUTR PLNK PHCB PIVL PYR
1 61 5 5 5 5 5 1 12
END PRINT-INFO

```

```

GEN-INFO
***
*** RCHRES
*** x - x
Name Nexits Unit Systems Printer
t-series Engl Metr LKFG
in out
31 EAST UPPER REEDY CK 1 1 1 90 0 1
41 WEST UPPER REEDY CK 1 1 1 90 0 1
51 WHITTENHORSE CK 1 1 1 90 0 1
61 DAVENPORT CK 1 1 1 90 0 1
2 BAY LAKE / 7 SEAS 2 1 1 90 0 1
3 UPPER L-405 1 1 1 90 0 0
4 C-4 1 1 1 90 0 0
5 L-403 - EPCOT 1 1 1 90 0 0
6 LOWER L-405 1 1 1 90 0 0
7 REEDY CK AB HWY 192 1 1 1 90 0 0
8 REEDY CK AB I-4 1 1 1 90 0 0
9 L MABEL / SOUTH L 1 1 1 90 0 1
10 L-105 1 1 1 90 0 0

```

11	L-103	1	1	1	90	0	0
12	L-107 / UPPER C-1	1	1	1	90	0	0
13	MIDDLE C-1	1	1	1	90	0	0
14	LOWER C-1	1	1	1	90	0	0
15	REEDY CK AT S-40	2	1	1	90	0	0
16	REEDY CK AT LOUGHMAN	1	1	1	90	0	0

END GEN-INFO

HYDR-PARM1

\*\*\* Flags for HYDR section

RCHRES	VC	A1	A2	A3	ODFVFG	for each	***	ODGTFG	for each	FUNCT	for each
x	-	x	FG	FG	FG	FG	possible	exit	***	possible	exit
							*	*	*	*	*
2			0	1	1	1	4	5		0	
3	14		0	1	1	1	4			0	
15			0	1	1	1	0	4		1	
16	61		0	1	1	1	4			0	

END HYDR-PARM1

HYDR-PARM2

*** RCHRES	FTABNO	LEN	DELTH	STCOR	KS	DB50
*** x - x		(miles)	(ft)	(ft)		(in)
2	2	1.00	0.1	62.5	0.0	0.01
3	3	5.56	0.1	.0	0.0	0.01
4	4	2.13	0.1	.0	0.0	0.01
5	5	3.36	0.1	.0	0.0	0.01
6	6	2.50	0.1	.0	0.0	0.01
7	7	2.01	0.1	.0	0.0	0.01
8	8	2.52	0.1	.0	0.0	0.01
9	9	2.00	0.1	88.25	0.0	0.01
10	10	1.77	0.1	.0	0.0	0.01
11	11	2.92	0.1	.0	0.0	0.01
12	12	6.75	0.1	.0	0.0	0.01
13	13	2.37	0.1	.0	0.0	0.01
14	14	4.51	0.1	.0	0.0	0.01
15	15	2.84	0.1	.0	0.0	0.01
16	16	1.0	0.1	-0.73	0.0	0.01
31	31	1.0	0.1	90.0	0.0	0.01
41	41	1.2	0.1	90.0	0.0	0.01
51	51	2.37	0.1	90.77	0.0	0.01
61	61	4.64	0.1	4.0	0.0	0.01

END HYDR-PARM2

HYDR-INIT

\*\*\* Initial conditions for HYDR section

*** RCHRES	VOL	CAT	Initial value	of COLIND	initial value	of OUTDGT						
*** x - x	ac-ft		for each possible	exit	for each possible	exit,ft3						
2	7230.0	0	4.0	5.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
3	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
4	2.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
5	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
6	2.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
7	5.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
8	2.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
9	2700.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0

10	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
11	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
12	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
13	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
14	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
15	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
16	0.1	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
31	3850.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
41	2820.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
51	2350.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0
61	250.0	0	4.0	4.0	4.0	4.0	4.0	0.0	0.0	0.0	0.0	0.0

END HYDR-INIT

\*\*\* Section RQUAL \*\*\*

BENTH-FLAG

RCHRES BENF \*\*\*

# - # \*\*\*

1 61 1

END BENTH-FLAG

SCOUR-PARMS

RCHRES SCRVEL SCRMUL \*\*\*

# - # \*\*\*

1 61 3. 1.

END SCOUR-PARMS

\*\*\* Section OXRX \*\*\*

OX-FLAGS

RCHRES REAM \*\*\*

# - # \*\*\*

2 61 3

END OX-FLAGS

OX-GENPARM

RCHRES KBOD20 TCBOB KODSET SUPSAT \*\*\*

# - # /hr \*\*\*

2 16 0.01 0.005

31 51 0.01 0.005

61 0.01 0.005

END OX-GENPARM

ELEV

\*\*\* RCHRES ELEV

\*\*\* x - x (ft)

2 16 80

31 41 120

51 110

61 100

END ELEV

OX-BENPARM

RCHRES	BENOD	TCBEN	EXPOD	BRBOD (1)	BRBOD (2)	EXPREL	***
# - #	mg/m2.hr			mg/m2.hr	mg/m2.hr		***
2	40	1.1	1.2	0.0001	0.0001	2.82	
3	40	1.1	1.2	0.0001	0.0001	2.82	
4	40	1.1	1.2	0.0001	0.0001	2.82	
5	40	1.1	1.2	0.0001	0.0001	2.82	
6	40	1.1	1.2	0.0001	0.0001	2.82	
7	40	1.1	1.2	0.0001	0.0001	2.82	
8	40	1.1	1.2	0.0001	0.0001	2.82	
9	40	1.1	1.2	0.0001	0.0001	2.82	
10	40	1.1	1.2	0.0001	0.0001	2.82	
11	40	1.1	1.2	0.0001	0.0001	2.82	
12	40	1.1	1.2	0.0001	0.0001	2.82	
13	40	1.1	1.2	0.0001	0.0001	2.82	
14	40	1.1	1.2	0.0001	0.0001	2.82	
15	40	1.1	1.2	0.0001	0.0001	2.82	
16	20	1.1	1.2	0.0001	0.0001	2.82	
31	80	1.1	1.2	0.0001	0.0001	2.82	
41	80	1.1	1.2	0.0001	0.0001	2.82	
51	80	1.1	1.2	0.0001	0.0001	2.82	
61	40	1.1	1.2	0.0001	0.0001	2.82	

END OX-BENPARM

OX-REAPARM

RCHRES	TCGINV	REAK	EXPRED	EXPREV	***
# - #		/hr			***
2	61	0.20	-1.1	1.1	

END OX-REAPARM

OX-INIT

RCHRES	DOX	BOD	SATDO	***
# - #	mg/l	mg/l	mg/l	***
2	61	6	0.1	

END OX-INIT

\*\*\* Section NUTRX \*\*\*

NUT-FLAGS

RCHRES	TAM	NO2	PO4	AMV	DEN	ADNH	ADPO	PHFL	***
# - #									***
1	61	1	0	1	1	0	0	2	

END NUT-FLAGS

NUT-AD-FLAGS

Atmospheric Deposition Flags \*\*\*

RCHRES	NO3	NH3	PO4	***
# - #	F C	F C	F C	***
1	61	-1 0	-1 0	0 0

END NUT-AD-FLAGS

NUT-BENPARM

RCHRES	BRTAM (1)	BRTAM (2)	BRPO4 (1)	BRPO4 (2)	ANAER	***
# - #	mg/m2.hr	mg/m2.hr	mg/m2.hr	mg/m2.hr	mg/l	***
2	61	0.0	0.0	0.0	0.005	

END NUT-BENPARM

NUT-NITDENIT

RCHRES	KTAM20	KNO220	TCNIT	KNO320	TCDEN	DENOXT ***
# - #	/hr	/hr		/hr		mg/l ***
2	0.015	0.002	1.07	0.001	1.04	5
3	0.015	0.002	1.07	0.001	1.04	5
4	0.015	0.002	1.07	0.001	1.04	5
5	0.015	0.002	1.07	0.001	1.04	5
6	0.015	0.002	1.07	0.001	1.04	5
7	0.015	0.002	1.07	0.001	1.04	5
8	0.015	0.002	1.07	0.001	1.04	5
9	0.015	0.002	1.07	0.001	1.04	5
10	0.015	0.002	1.07	0.001	1.04	5
11	0.015	0.002	1.07	0.001	1.04	5
12	0.015	0.002	1.07	0.001	1.04	5
13	0.015	0.002	1.07	0.001	1.04	5
14	0.015	0.002	1.07	0.001	1.04	5
15	0.015	0.002	1.07	0.001	1.04	5
16	0.015	0.002	1.07	0.001	1.04	5
31	0.003	0.002	1.07	0.001	1.04	5
41	0.003	0.002	1.07	0.001	1.04	5
51	0.003	0.002	1.07	0.001	1.04	5
61	0.015	0.002	1.07	0.001	1.04	5

END NUT-NITDENIT

NUT-NH3VOLAT

RCHRES	EXPNVG	EXPNVL ***
# - #		***
2	.50	0.6667
3	.50	0.6667
4	.50	0.6667
5	.50	0.6667
6	.50	0.6667
7	.50	0.6667
8	.50	0.6667
9	.50	0.6667
10	.50	0.6667
11	.50	0.6667
12	.50	0.6667
13	.50	0.6667
14	.50	0.6667
15	.50	0.6667
16	.50	0.6667
31	.50	0.6667
41	.50	0.6667
51	.50	0.6667
61	.50	0.6667

END NUT-NH3VOLAT

NUT-DINIT

RCHRES	NO3	TAM	NO2	PO4	PHVAL	***
# - #	mg/l	mg/l	mg/l	mg/l	ph units	***
2	.05	0.05	0.	.02	7.0	
3	.05	0.05	0.	.02	7.0	
4	.05	0.05	0.	.02	7.0	
5	.05	0.05	0.	.02	7.0	
6	.05	0.05	0.	.02	7.0	
7	.05	0.05	0.	.02	7.0	
8	.05	0.05	0.	.02	7.0	
9	.05	0.05	0.	.02	7.0	
10	.05	0.05	0.	.02	7.0	
11	.05	0.05	0.	.02	7.0	
12	.05	0.05	0.	.02	7.0	
13	.05	0.05	0.	.02	7.0	
14	.05	0.05	0.	.02	7.0	
15	.05	0.05	0.	.02	7.0	
16	.05	0.05	0.	.02	7.0	
31	.05	0.05	0.	.02	7.0	
41	.05	0.05	0.	.02	7.0	
51	.05	0.05	0.	.02	7.0	
61	.05	0.05	0.	.02	7.0	

END NUT-DINIT

\*\*\* Section PLANK \*\*\*

PLNK-FLAGS

RCHRES	PHYF	ZOOF	BALF	SDLT	AMRF	DECF	NSFG	ZFOO	***
# - #									***
1	61	1	0	0	0	1		1	

END PLNK-FLAGS

PLNK-PARM1

RCHRES	RATCLP	NONREF	LITSED	ALNPR	EXTB	MALGR	***
# - #					/ft	/hr	***
2	0.6	0.5	0.0	0.70	1.0	0.07	
3	0.6	0.5	0.0	0.70	1.0	0.07	
4	0.6	0.5	0.0	0.70	1.0	0.07	
5	0.6	0.5	0.0	0.70	1.0	0.07	
6	0.6	0.5	0.0	0.70	1.0	0.07	
7	0.6	0.5	0.0	0.70	1.0	0.07	
8	0.6	0.5	0.0	0.70	1.0	0.07	
9	0.6	0.5	0.0	0.70	1.0	0.07	
10	0.6	0.5	0.0	0.70	1.0	0.07	
11	0.6	0.5	0.0	0.70	1.0	0.07	
12	0.6	0.5	0.0	0.70	1.0	0.07	
13	0.6	0.5	0.0	0.70	1.0	0.07	
14	0.6	0.5	0.0	0.70	1.0	0.07	
15	0.6	0.5	0.0	0.70	1.0	0.07	
16	0.6	0.5	0.0	0.70	1.0	0.07	
31	0.6	0.5	0.0	0.70	1.0	0.07	
41	0.6	0.5	0.0	0.70	1.0	0.07	
51	0.6	0.5	0.0	0.70	1.0	0.07	
61	0.6	0.5	0.0	0.70	1.0	0.07	

END PLNK-PARM1

PLNK-PARM2

RCHRES	***	CMMLT	CMMN	CMMNP	CMMP	TALGRH	TALGRL	TALGRM	
#	-	#	***						
2		.010		0.025	.0001	.005	95.	-20.0	86.
3		.010		0.025	.0001	.005	95.	-20.0	86.
4		.010		0.025	.0001	.005	95.	-20.0	86.
5		.010		0.025	.0001	.005	95.	-20.0	86.
6		.010		0.025	.0001	.005	95.	-20.0	86.
7		.010		0.025	.0001	.005	95.	-20.0	86.
8		.010		0.025	.0001	.005	95.	-20.0	86.
9		.010		0.025	.0001	.005	95.	-20.0	86.
10		.010		0.025	.0001	.005	95.	-20.0	86.
11		.010		0.025	.0001	.005	95.	-20.0	86.
12		.010		0.025	.0001	.005	95.	-20.0	86.
13		.010		0.025	.0001	.005	95.	-20.0	86.
14		.010		0.025	.0001	.005	95.	-20.0	86.
15		.010		0.025	.0001	.005	95.	-20.0	86.
16		.010		0.025	.0001	.005	95.	-20.0	86.
31		.010		0.025	.0001	.005	95.	-20.0	86.
41		.010		0.025	.0001	.005	95.	-20.0	86.
51		.010		0.025	.0001	.005	95.	-20.0	86.
61		.010		0.025	.0001	.005	95.	-20.0	86.

END PLNK-PARM2

PLNK-PARM3

RCHRES	***	ALR20	ALDH	ALDL	OXALD	NALDH	PALDH	
#	-	#	***					
2		0.005		0.01	0.001	0.03	0.01	0.002
3		0.005		0.01	0.001	0.03	0.01	0.002
4		0.005		0.01	0.001	0.03	0.01	0.002
5		0.005		0.01	0.001	0.03	0.01	0.002
6		0.005		0.01	0.001	0.03	0.01	0.002
7		0.005		0.01	0.001	0.03	0.01	0.002
8		0.005		0.01	0.001	0.03	0.01	0.002
9		0.005		0.01	0.001	0.03	0.01	0.002
10		0.005		0.01	0.001	0.03	0.01	0.002
11		0.005		0.01	0.001	0.03	0.01	0.002
12		0.005		0.01	0.001	0.03	0.01	0.002
13		0.005		0.01	0.001	0.03	0.01	0.002
14		0.005		0.01	0.001	0.03	0.01	0.002
15		0.005		0.01	0.001	0.03	0.01	0.002
16		0.005		0.01	0.001	0.03	0.01	0.002
31		0.005		0.01	0.001	0.03	0.01	0.002
41		0.005		0.01	0.001	0.03	0.01	0.002
51		0.005		0.01	0.001	0.03	0.01	0.002
61		0.005		0.01	0.001	0.03	0.01	0.002

END PLNK-PARM3



PHYTO-PARM

RCHRES	SEED	MXSTAY	OREF	CLALDH	PHYSET	REFSET	***
# - #	mg/l	mg/l		ug/l			***
2	.5	2.	20.	20	.02	.02	
3	.5	2.	20.	20	.02	.02	
4	.5	2.	20.	20	.02	.02	
5	.5	2.	20.	20	.02	.02	
6	.5	2.	20.	20	.02	.02	
7	.5	2.	20.	20	.02	.02	
8	.5	2.	20.	20	.02	.02	
9	.5	2.	20.	20	.02	.02	
10	.5	2.	20.	20	.02	.02	
11	.5	2.	20.	20	.02	.02	
12	.5	2.	20.	20	.02	.02	
13	.5	2.	20.	20	.02	.02	
14	.5	2.	20.	20	.02	.02	
15	.5	2.	20.	20	.02	.02	
16	.5	2.	20.	20	.02	.02	
31	.5	2.	20.	20	.02	.02	
41	.5	2.	20.	20	.02	.02	
51	.5	2.	20.	20	.02	.02	
61	.5	2.	20.	20	.02	.02	

END PHYTO-PARM

PLNK-INIT

RCHRES	PHYTO	ZOO	BENAL	ORN	ORP	ORC	***
# - #	mg/l	org/l	mg/m2	mg/l	mg/l	mg/l	***
2 61	.05			.02	0.01	0.1	

END PLNK-INIT

END RCHRES

COPY

TIMESERIES

Copy-opn\*\*\*

*** x - x	NPT	NMN
101 106	7	
1 4	20	

END TIMESERIES

END COPY

EXT SOURCES

<-Volume-> <Member> SsysSgap<--Mult-->Tran <-Target vols> <-Grp> <-Member-> \*\*\*  
 <Name> x <Name> x tem strg<-factor->strg <Name> x x <Name> x x \*\*\*

\*\*\* Precip

\*\*\* DSN 70 = Disaggregated hourly rainfall for Conserv sites 601-604, based on  
 \*\*\* DSN 71 = Disaggregated hourly rainfall for L-101, based on Orlando r  
 \*\*\* DSN 73 = Disaggregated hourly rainfall for Conserv sites 701-901, based on  
 \*\*\* DSN 75 = Disaggregated hourly rainfall for L-410, modified based on 701-901

\*\*\* Segment 1

WDM1	71	PREC	0 ENGL	.45	PERLND	11	19	EXTNL	PREC	1	1
WDM1	75	PREC	0 ENGL	.50	PERLND	11	19	EXTNL	PREC	1	1
WDM1	73	PREC	0 ENGL	.05	PERLND	11	19	EXTNL	PREC	1	1
WDM1	71	PREC	0 ENGL	.45	IMPLND	14	0	EXTNL	PREC	1	1
WDM1	75	PREC	0 ENGL	.50	IMPLND	14	0	EXTNL	PREC	1	1
WDM1	73	PREC	0 ENGL	.05	IMPLND	14	0	EXTNL	PREC	1	1
WDM1	71	PREC	0 ENGL	.45	RCHRES	1	16	EXTNL	PREC	1	1
WDM1	75	PREC	0 ENGL	.50	RCHRES	1	16	EXTNL	PREC	1	1
WDM1	73	PREC	0 ENGL	.05	RCHRES	1	16	EXTNL	PREC	1	1

\*\*\* Segment 3

WDM1	70	PREC	0	ENGL	.15	PERLND	31	39	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.02	PERLND	31	39	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.80	PERLND	31	39	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.03	PERLND	31	39	EXTNL	PREC	1	1
WDM1	70	PREC	0	ENGL	.15	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.02	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.80	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.03	IMPLND	34	0	EXTNL	PREC	1	1
WDM1	70	PREC	0	ENGL	.15	RCHRES	31	41	EXTNL	PREC	1	1
WDM1	71	PREC	0	ENGL	.02	RCHRES	31	41	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.80	RCHRES	31	41	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.03	RCHRES	31	41	EXTNL	PREC	1	1

\*\*\* Segment 5

WDM1	75	PREC	0	ENGL	.80	PERLND	51	59	EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.20	PERLND	51	59	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.80	IMPLND	54		EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.20	IMPLND	54		EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	.80	RCHRES	51		EXTNL	PREC	1	1
WDM1	73	PREC	0	ENGL	.20	RCHRES	51		EXTNL	PREC	1	1

\*\*\* Segment 6

WDM1	75	PREC	0	ENGL	1.0	PERLND	61	65	EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	1.0	IMPLND	64		EXTNL	PREC	1	1
WDM1	75	PREC	0	ENGL	1.0	RCHRES	61		EXTNL	PREC	1	1

\*\*\* Evap

\*\*\* DSN 80 = PET from mo. pan coefficients x pan evap at Lisbon

WDM1	80	PET		ENGL		PERLND	11	69	EXTNL	PETINP		
WDM1	80	PET		ENGL		IMPLND	14	64	EXTNL	PETINP		
WDM1	80	PET		ENGL		RCHRES	1	61	EXTNL	POTEV		

\*\*\* RIBS application - dataset in units of acre-inches

\*\*\* Divide by total area of ribs for all three lines following

WDM1	91	RIBS		ENGL	.0384615	PERLND	19		EXTNL	PREC		
WDM1	91	RIBS		ENGL	.0316456	PERLND	39		EXTNL	PREC		
WDM1	91	RIBS		ENGL	.0355872	PERLND	59		EXTNL	PREC		

\*\*\* Well water pumped into Bay Lake and Seven Seas Lagoon

WDM	92	PUMP		ENGL		RCHRES	2		EXTNL	IVOL		
-----	----	------	--	------	--	--------	---	--	-------	------	--	--

\*\*\* Grove Irrigation as PREC (sprinkler) or SURLI (drip)

WDM1	94	IRRG		ENGL		PERLND	11		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	21		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	31		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	51		EXTNL	PREC		
WDM1	94	IRRG		ENGL		PERLND	61		EXTNL	PREC		

\*\*\* Buzzard site diversion

\*\*\* Data set units are in cubic feet per second

WDM	95	FLOW		ENGL		SAME	RCHRES	15		EXTNL	OUTDGT	1
-----	----	------	--	------	--	------	--------	----	--	-------	--------	---

\*\*\* Cypress Creek discharge (treated as a point)

WDM1 22 FLOW ENGL .082645SAME RCHRES 11 EXTNL IVOL

\*\*\*Cypress Creek water-quality (treated as point source)

\*\*\*do, bod, ammon, no3, po4, orn, orp, orc

WDM 820 DO ENGL DIV RCHRES 11 INFLOW OXIF 1  
WDM 821 BOD ENGL DIV RCHRES 11 INFLOW OXIF 2  
WDM 822 NH3 ENGL DIV RCHRES 11 INFLOW NUIF1 2  
WDM 823 NO3 ENGL DIV RCHRES 11 INFLOW NUIF1 1  
WDM 824 PO4 ENGL DIV RCHRES 11 INFLOW NUIF1 4

\*\*\* Hourly air temperature at ORL MCO (degrees F)

WDM1 85 TEMP ENGL PERLND 11 65 EXTNL GATMP  
WDM1 85 TEMP ENGL IMPLND 14 64 EXTNL GATMP  
WDM1 85 TEMP ENGL RCHRES 1 61 EXTNL GATMP

\*\*\* Daily wind speed (mph)

WDM1 82 WIND ENGL SAME RCHRES 1 61 EXTNL WIND

\*\*\* Hourly solar radiation at Daytona Beach (ly/hr)

WDM1 81 SOLR ENGL RCHRES 1 61 EXTNL SOLRAD

\*\*\* Water Temperature (degrees C)

WDM1 603 TH2O METR RCHRES 2 7 HTRCH TW  
WDM1 602 TH2O METR RCHRES 8 HTRCH TW  
WDM1 603 TH2O METR RCHRES 9 12 HTRCH TW  
WDM1 602 TH2O METR RCHRES 13 HTRCH TW  
WDM1 601 TH2O METR RCHRES 14 16 HTRCH TW  
WDM1 603 TH2O METR RCHRES 31 41 HTRCH TW  
WDM1 604 TH2O METR RCHRES 51 61 HTRCH TW

\*\*\* Atmospheric Deposition (lb/ac)

WDM1 86 NH4D ENGL DIV PERLND 11 65 EXTNL PQADFX 1 1  
WDM1 86 NH4D ENGL DIV IMPLND 14 64 EXTNL IQADFX 1  
WDM1 86 NH4D ENGL DIV RCHRES 1 61 EXTNL NUADFX 2 1  
WDM1 87 NO3D ENGL DIV PERLND 11 65 EXTNL PQADFX 2 1  
WDM1 87 NO3D ENGL DIV IMPLND 14 64 EXTNL IQADFX 2  
WDM1 87 NO3D ENGL DIV RCHRES 1 61 EXTNL NUADFX 1 1

END EXT SOURCES

EXT TARGETS

<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Volume-> <Member> Tsys Aggr Amd \*\*\*  
<Name> x <Name> x x<-factor->strg <Name> x <Name>qf tem strg strg\*\*\*

\*\*\* Seven Seas Lagoon/Bay Lake combined outflow (RCHRES 2)

RCHRES 2 HYDR RO WDM 102 FLOW ENGL AGGR REPL

\*\*\* Lake Mabel/South Lake Outflow (RCHRES 9)

RCHRES 9 HYDR RO WDM 109 FLOW ENGL AGGR REPL

\*\*\* Reedy Creek below S40 near Loughman

RCHRES 15 HYDR RO WDM 115 FLOW ENGL AGGR REPL

\*\*\* Upper East Reedy Creek - Lateral 405 at S-405A

RCHRES 31 HYDR RO WDM 131 FLOW ENGL AGGR REPL

\*\*\* Upper West Reedy Creek - Reedy Creek at S46 near Vineland

RCHRES 41 HYDR RO WDM 141 FLOW ENGL AGGR REPL

\*\*\* Whittenhorse creek stage

RCHRES 51 HYDR STAGE WDM 251 STAG ENGL AGGR REPL

\*\*\* Davenport creek stage

RCHRES 61 HYDR STAGE WDM 261 STAG ENGL AGGR REPL

\*\*\* Miscellaneous temporary calibration

RCHRES 2 OXRX SATDO WDM 1002 TEST ENGL AGGR REPL  
 RCHRES 3 OXRX SATDO WDM 1003 TEST ENGL AGGR REPL  
 RCHRES 4 OXRX SATDO WDM 1004 TEST ENGL AGGR REPL  
 RCHRES 5 OXRX SATDO WDM 1005 TEST ENGL AGGR REPL  
 RCHRES 6 OXRX SATDO WDM 1006 TEST ENGL AGGR REPL  
 RCHRES 7 OXRX SATDO WDM 1007 TEST ENGL AGGR REPL  
 RCHRES 8 OXRX SATDO WDM 1008 TEST ENGL AGGR REPL  
 RCHRES 9 OXRX SATDO WDM 1009 TEST ENGL AGGR REPL  
 RCHRES 10 OXRX SATDO WDM 1010 TEST ENGL AGGR REPL  
 RCHRES 11 OXRX SATDO WDM 1011 TEST ENGL AGGR REPL  
 RCHRES 12 OXRX SATDO WDM 1012 TEST ENGL AGGR REPL  
 RCHRES 13 OXRX SATDO WDM 1013 TEST ENGL AGGR REPL  
 RCHRES 14 OXRX SATDO WDM 1014 TEST ENGL AGGR REPL  
 RCHRES 15 OXRX SATDO WDM 1015 TEST ENGL AGGR REPL  
 RCHRES 16 OXRX SATDO WDM 1016 TEST ENGL AGGR REPL  
 RCHRES 31 OXRX SATDO WDM 1031 TEST ENGL AGGR REPL  
 RCHRES 41 OXRX SATDO WDM 1041 TEST ENGL AGGR REPL  
 RCHRES 51 OXRX SATDO WDM 1051 TEST ENGL AGGR REPL  
 RCHRES 61 OXRX SATDO WDM 1061 TEST ENGL AGGR REPL

\*\*\* WQ DSNS for Loughman \*\*\*

\*\*\* REACH 16 \*\*\*

RCHRES 16 NUTRX DNUST 1 AVER WDM1 2001 NO3X ENGL AGGR REPL  
 RCHRES 16 NUTRX DNUST 2 AVER WDM1 2002 NH3X ENGL AGGR REPL  
 RCHRES 16 PLANK PKST3 4 AVER WDM1 2003 ORGN ENGL AGGR REPL  
 RCHRES 16 PLANK PKST4 1 AVER WDM1 2004 TOTN ENGL AGGR REPL  
 RCHRES 16 NUTRX DNUST 4 AVER WDM1 2005 PO4X ENGL AGGR REPL  
 RCHRES 16 PLANK PKST3 5 AVER WDM1 2006 ORGP ENGL AGGR REPL  
 RCHRES 16 PLANK PKST4 2 AVER WDM1 2007 TOTP ENGL AGGR REPL  
 RCHRES 16 PLANK PHYCLA AVER WDM1 2008 CHLA ENGL AGGR REPL  
 RCHRES 16 PLANK PKST3 6 AVER WDM1 2009 TOCX ENGL AGGR REPL  
 RCHRES 16 OXRX DOX AVER WDM1 2010 DOXX ENGL AGGR REPL  
 RCHRES 16 OXRX BOD AVER WDM1 2011 BODX ENGL AGGR REPL  
 RCHRES 16 PLANK TPKCF1 4 SUM WDM1 2012 TNLD ENGL AGGR REPL  
 RCHRES 16 PLANK TPKCF1 5 SUM WDM1 2013 TPLD ENGL AGGR REPL  
 RCHRES 16 NUTRX NUCF1 1 SUM WDM1 2014 NO3L ENGL AGGR REPL  
 RCHRES 16 NUTRX NUCF1 2 SUM WDM1 2225 NH3L ENGL AGGR REPL  
 RCHRES 16 NUTRX NUCF1 4 SUM WDM1 2226 PO4L ENGL AGGR REPL

\*\*\* WQ DSNS for Davenport Creek \*\*\*

\*\*\* REACH 61 \*\*\*

RCHRES 61 NUTRX DNUST 1 AVER WDM1 2015 NO3X ENGL AGGR REPL  
 RCHRES 61 NUTRX DNUST 2 AVER WDM1 2016 NH3X ENGL AGGR REPL  
 RCHRES 61 PLANK PKST3 4 AVER WDM1 2017 ORGN ENGL AGGR REPL  
 RCHRES 61 PLANK PKST4 1 AVER WDM1 2018 TOTN ENGL AGGR REPL  
 RCHRES 61 NUTRX DNUST 4 AVER WDM1 2019 PO4X ENGL AGGR REPL  
 RCHRES 61 PLANK PKST3 5 AVER WDM1 2020 ORGP ENGL AGGR REPL  
 RCHRES 61 PLANK PKST4 2 AVER WDM1 2021 TOTP ENGL AGGR REPL

RCHRES	61	PLANK	PHYTO		AVER	WDM1	2022	CHLA	ENGL	AGGR	REPL
RCHRES	61	PLANK	PKST3	6	AVER	WDM1	2023	TOCX	ENGL	AGGR	REPL
RCHRES	61	OXR	DOX		AVER	WDM1	2024	DOXX	ENGL	AGGR	REPL
RCHRES	61	OXR	BOD		AVER	WDM1	2025	BODX	ENGL	AGGR	REPL
RCHRES	61	PLANK	TPKCF1	4	SUM	WDM1	2026	TNLD	ENGL	AGGR	REPL
RCHRES	61	PLANK	TPKCF1	5	SUM	WDM1	2027	TPLD	ENGL	AGGR	REPL
RCHRES	61	NUTRX	NUCF1	1	SUM	WDM1	2028	NO3L	ENGL	AGGR	REPL
RCHRES	61	NUTRX	NUCF1	2	SUM	WDM1	2227	NH3L	ENGL	AGGR	REPL
RCHRES	61	NUTRX	NUCF1	4	SUM	WDM1	2228	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Reedy Creek at S-40 \*\*\*

\*\*\* REACH 15 \*\*\*

RCHRES	15	NUTRX	DNUST	1	AVER	WDM1	2029	NO3X	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	2	AVER	WDM1	2030	NH3X	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	4	AVER	WDM1	2031	ORGN	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST4	1	AVER	WDM1	2032	TOTN	ENGL	AGGR	REPL
RCHRES	15	NUTRX	DNUST	4	AVER	WDM1	2033	PO4X	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	5	AVER	WDM1	2034	ORGP	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST4	2	AVER	WDM1	2035	TOTP	ENGL	AGGR	REPL
RCHRES	15	PLANK	PHYTO		AVER	WDM1	2036	CHLA	ENGL	AGGR	REPL
RCHRES	15	PLANK	PKST3	6	AVER	WDM1	2037	TOCX	ENGL	AGGR	REPL
RCHRES	15	OXR	DOX		AVER	WDM1	2038	DOXX	ENGL	AGGR	REPL
RCHRES	15	OXR	BOD		AVER	WDM1	2039	BODX	ENGL	AGGR	REPL
RCHRES	15	PLANK	TPKCF1	4	SUM	WDM1	2040	TNLD	ENGL	AGGR	REPL
RCHRES	15	PLANK	TPKCF1	5	SUM	WDM1	2041	TPLD	ENGL	AGGR	REPL
RCHRES	15	NUTRX	NUCF1	1	SUM	WDM1	2042	NO3L	ENGL	AGGR	REPL
RCHRES	15	NUTRX	NUCF1	2	SUM	WDM1	2229	NH3L	ENGL	AGGR	REPL
RCHRES	15	NUTRX	NUCF1	4	SUM	WDM1	2230	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Reedy Creek near Vineland \*\*\*

\*\*\* REACH 7 \*\*\*

RCHRES	7	NUTRX	DNUST	1	AVER	WDM1	2043	NO3X	ENGL	AGGR	REPL
RCHRES	7	NUTRX	DNUST	2	AVER	WDM1	2044	NH3X	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	4	AVER	WDM1	2045	ORGN	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST4	1	AVER	WDM1	2046	TOTN	ENGL	AGGR	REPL
RCHRES	7	NUTRX	DNUST	4	AVER	WDM1	2047	PO4X	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	5	AVER	WDM1	2048	ORGP	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST4	2	AVER	WDM1	2049	TOTP	ENGL	AGGR	REPL
RCHRES	7	PLANK	PHYTO		AVER	WDM1	2050	CHLA	ENGL	AGGR	REPL
RCHRES	7	PLANK	PKST3	6	AVER	WDM1	2051	TOCX	ENGL	AGGR	REPL
RCHRES	7	OXR	DOX		AVER	WDM1	2052	DOXX	ENGL	AGGR	REPL
RCHRES	7	OXR	BOD		AVER	WDM1	2053	BODX	ENGL	AGGR	REPL
RCHRES	7	PLANK	TPKCF1	4	SUM	WDM1	2054	TNLD	ENGL	AGGR	REPL
RCHRES	7	PLANK	TPKCF1	5	SUM	WDM1	2055	TPLD	ENGL	AGGR	REPL
RCHRES	7	NUTRX	NUCF1	1	SUM	WDM1	2056	NO3L	ENGL	AGGR	REPL
RCHRES	7	NUTRX	NUCF1	2	SUM	WDM1	2231	NH3L	ENGL	AGGR	REPL
RCHRES	7	NUTRX	NUCF1	4	SUM	WDM1	2232	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Bonnet Creek near Vineland \*\*\*

\*\*\* REACH 13 \*\*\*

RCHRES	13	NUTRX	DNUST	1	AVER	WDM1	2057	NO3X	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	2	AVER	WDM1	2058	NH3X	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	4	AVER	WDM1	2059	ORGN	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST4	1	AVER	WDM1	2060	TOTN	ENGL	AGGR	REPL
RCHRES	13	NUTRX	DNUST	4	AVER	WDM1	2061	PO4X	ENGL	AGGR	REPL

RCHRES	13	PLANK	PKST3	5	AVER	WDM1	2062	ORGP	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST4	2	AVER	WDM1	2063	TOTP	ENGL	AGGR	REPL
RCHRES	13	PLANK	PHYTO		AVER	WDM1	2064	CHLA	ENGL	AGGR	REPL
RCHRES	13	PLANK	PKST3	6	AVER	WDM1	2065	TOCX	ENGL	AGGR	REPL
RCHRES	13	OXR	DOX		AVER	WDM1	2066	DOXX	ENGL	AGGR	REPL
RCHRES	13	OXR	BOD		AVER	WDM1	2067	BODX	ENGL	AGGR	REPL
RCHRES	13	PLANK	TPKCF1	4	SUM	WDM1	2068	TNLD	ENGL	AGGR	REPL
RCHRES	13	PLANK	TPKCF1	5	SUM	WDM1	2069	TPLD	ENGL	AGGR	REPL
RCHRES	13	NUTRX	NUCF1	1	SUM	WDM1	2070	NO3L	ENGL	AGGR	REPL
RCHRES	13	NUTRX	NUCF1	2	SUM	WDM1	2233	NH3L	ENGL	AGGR	REPL
RCHRES	13	NUTRX	NUCF1	4	SUM	WDM1	2234	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Whittenhorse Creek \*\*\*

\*\*\* REACH 51 \*\*\*

RCHRES	51	NUTRX	DNUST	1	AVER	WDM1	2071	NO3X	ENGL	AGGR	REPL
RCHRES	51	NUTRX	DNUST	2	AVER	WDM1	2072	NH3X	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST3	4	AVER	WDM1	2073	ORGN	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST4	1	AVER	WDM1	2074	TOTN	ENGL	AGGR	REPL
RCHRES	51	NUTRX	DNUST	4	AVER	WDM1	2075	PO4X	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST3	5	AVER	WDM1	2076	ORGP	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST4	2	AVER	WDM1	2077	TOTP	ENGL	AGGR	REPL
RCHRES	51	PLANK	PHYTO		AVER	WDM1	2078	CHLA	ENGL	AGGR	REPL
RCHRES	51	PLANK	PKST3	6	AVER	WDM1	2079	TOCX	ENGL	AGGR	REPL
RCHRES	51	OXR	DOX		AVER	WDM1	2080	DOXX	ENGL	AGGR	REPL
RCHRES	51	OXR	BOD		AVER	WDM1	2081	BODX	ENGL	AGGR	REPL
RCHRES	51	PLANK	TPKCF1	4	SUM	WDM1	2082	TNLD	ENGL	AGGR	REPL
RCHRES	51	PLANK	TPKCF1	5	SUM	WDM1	2083	TPLD	ENGL	AGGR	REPL
RCHRES	51	NUTRX	NUCF1	1	SUM	WDM1	2084	NO3L	ENGL	AGGR	REPL
RCHRES	51	NUTRX	NUCF1	2	SUM	WDM1	2235	NH3L	ENGL	AGGR	REPL
RCHRES	51	NUTRX	NUCF1	4	SUM	WDM1	2236	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Upper West Reedy Creek @ S-46 \*\*\*

\*\*\* REACH 41 \*\*\*

RCHRES	41	NUTRX	DNUST	1	AVER	WDM1	2085	NO3X	ENGL	AGGR	REPL
RCHRES	41	NUTRX	DNUST	2	AVER	WDM1	2086	NH3X	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST3	4	AVER	WDM1	2087	ORGN	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST4	1	AVER	WDM1	2088	TOTN	ENGL	AGGR	REPL
RCHRES	41	NUTRX	DNUST	4	AVER	WDM1	2089	PO4X	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST3	5	AVER	WDM1	2090	ORGP	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST4	2	AVER	WDM1	2091	TOTP	ENGL	AGGR	REPL
RCHRES	41	PLANK	PHYTO		AVER	WDM1	2092	CHLA	ENGL	AGGR	REPL
RCHRES	41	PLANK	PKST3	6	AVER	WDM1	2093	TOCX	ENGL	AGGR	REPL
RCHRES	41	OXR	DOX		AVER	WDM1	2094	DOXX	ENGL	AGGR	REPL
RCHRES	41	OXR	BOD		AVER	WDM1	2095	BODX	ENGL	AGGR	REPL
RCHRES	41	PLANK	TPKCF1	4	SUM	WDM1	2096	TNLD	ENGL	AGGR	REPL
RCHRES	41	PLANK	TPKCF1	5	SUM	WDM1	2097	TPLD	ENGL	AGGR	REPL
RCHRES	41	NUTRX	NUCF1	1	SUM	WDM1	2098	NO3L	ENGL	AGGR	REPL
RCHRES	41	NUTRX	NUCF1	2	SUM	WDM1	2237	NH3L	ENGL	AGGR	REPL
RCHRES	41	NUTRX	NUCF1	4	SUM	WDM1	2238	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Upper East Reedy Creek @ S-405A \*\*\*

\*\*\* REACH 31 \*\*\*

RCHRES	31	NUTRX	DNUST	1	AVER	WDM1	2099	NO3X	ENGL	AGGR	REPL
RCHRES	31	NUTRX	DNUST	2	AVER	WDM1	2100	NH3X	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST3	4	AVER	WDM1	2101	ORGN	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST4	1	AVER	WDM1	2102	TOTN	ENGL	AGGR	REPL
RCHRES	31	NUTRX	DNUST	4	AVER	WDM1	2103	PO4X	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST3	5	AVER	WDM1	2104	ORGP	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST4	2	AVER	WDM1	2105	TOTP	ENGL	AGGR	REPL
RCHRES	31	PLANK	PHYTO		AVER	WDM1	2106	CHLA	ENGL	AGGR	REPL
RCHRES	31	PLANK	PKST3	6	AVER	WDM1	2107	TOCX	ENGL	AGGR	REPL
RCHRES	31	OXR	DOX		AVER	WDM1	2108	DOXX	ENGL	AGGR	REPL
RCHRES	31	OXR	BOD		AVER	WDM1	2109	BODX	ENGL	AGGR	REPL
RCHRES	31	PLANK	TPKCF1	4	SUM	WDM1	2110	TNLD	ENGL	AGGR	REPL
RCHRES	31	PLANK	TPKCF1	5	SUM	WDM1	2111	TPLD	ENGL	AGGR	REPL
RCHRES	31	NUTRX	NUCF1	1	SUM	WDM1	2112	NO3L	ENGL	AGGR	REPL
RCHRES	31	NUTRX	NUCF1	2	SUM	WDM1	2239	NH3L	ENGL	AGGR	REPL
RCHRES	31	NUTRX	NUCF1	4	SUM	WDM1	2240	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Lateral 405 at S-405 \*\*\*

\*\*\* REACH 3 \*\*\*

RCHRES	3	NUTRX	DNUST	1	AVER	WDM1	2113	NO3X	ENGL	AGGR	REPL
RCHRES	3	NUTRX	DNUST	2	AVER	WDM1	2114	NH3X	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST3	4	AVER	WDM1	2115	ORGN	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST4	1	AVER	WDM1	2116	TOTN	ENGL	AGGR	REPL
RCHRES	3	NUTRX	DNUST	4	AVER	WDM1	2117	PO4X	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST3	5	AVER	WDM1	2118	ORGP	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST4	2	AVER	WDM1	2119	TOTP	ENGL	AGGR	REPL
RCHRES	3	PLANK	PHYTO		AVER	WDM1	2120	CHLA	ENGL	AGGR	REPL
RCHRES	3	PLANK	PKST3	6	AVER	WDM1	2121	TOCX	ENGL	AGGR	REPL
RCHRES	3	OXR	DOX		AVER	WDM1	2122	DOXX	ENGL	AGGR	REPL
RCHRES	3	OXR	BOD		AVER	WDM1	2123	BODX	ENGL	AGGR	REPL
RCHRES	3	PLANK	TPKCF1	4	SUM	WDM1	2124	TNLD	ENGL	AGGR	REPL
RCHRES	3	PLANK	TPKCF1	5	SUM	WDM1	2125	TPLD	ENGL	AGGR	REPL
RCHRES	3	NUTRX	NUCF1	1	SUM	WDM1	2126	NO3L	ENGL	AGGR	REPL
RCHRES	3	NUTRX	NUCF1	2	SUM	WDM1	2241	NH3L	ENGL	AGGR	REPL
RCHRES	3	NUTRX	NUCF1	4	SUM	WDM1	2242	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Reedy Creek at I-4 \*\*\*

\*\*\* REACH 8 \*\*\*

RCHRES	8	NUTRX	DNUST	1	AVER	WDM1	2127	NO3X	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	2	AVER	WDM1	2128	NH3X	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	4	AVER	WDM1	2129	ORGN	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST4	1	AVER	WDM1	2130	TOTN	ENGL	AGGR	REPL
RCHRES	8	NUTRX	DNUST	4	AVER	WDM1	2131	PO4X	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	5	AVER	WDM1	2132	ORGP	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST4	2	AVER	WDM1	2133	TOTP	ENGL	AGGR	REPL
RCHRES	8	PLANK	PHYTO		AVER	WDM1	2134	CHLA	ENGL	AGGR	REPL
RCHRES	8	PLANK	PKST3	6	AVER	WDM1	2135	TOCX	ENGL	AGGR	REPL
RCHRES	8	OXR	DOX		AVER	WDM1	2136	DOXX	ENGL	AGGR	REPL
RCHRES	8	OXR	BOD		AVER	WDM1	2137	BODX	ENGL	AGGR	REPL
RCHRES	8	PLANK	TPKCF1	4	SUM	WDM1	2138	TNLD	ENGL	AGGR	REPL
RCHRES	8	PLANK	TPKCF1	5	SUM	WDM1	2139	TPLD	ENGL	AGGR	REPL
RCHRES	8	NUTRX	NUCF1	1	SUM	WDM1	2140	NO3L	ENGL	AGGR	REPL
RCHRES	8	NUTRX	NUCF1	2	SUM	WDM1	2243	NH3L	ENGL	AGGR	REPL
RCHRES	8	NUTRX	NUCF1	4	SUM	WDM1	2244	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Bay Lake/Seven Seas \*\*\*

\*\*\* REACH 2 \*\*\*

RCHRES	2	NUTRX	DNUST	1	AVER	WDM1	2141	NO3X	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	2	AVER	WDM1	2142	NH3X	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	4	AVER	WDM1	2143	ORGN	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST4	1	AVER	WDM1	2144	TOTN	ENGL	AGGR	REPL
RCHRES	2	NUTRX	DNUST	4	AVER	WDM1	2145	PO4X	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	5	AVER	WDM1	2146	ORGP	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST4	2	AVER	WDM1	2147	TOTP	ENGL	AGGR	REPL
RCHRES	2	PLANK	PHYTO		AVER	WDM1	2148	CHLA	ENGL	AGGR	REPL
RCHRES	2	PLANK	PKST3	6	AVER	WDM1	2149	TOCX	ENGL	AGGR	REPL
RCHRES	2	OXX	DOX		AVER	WDM1	2150	DOXX	ENGL	AGGR	REPL
RCHRES	2	OXX	BOD		AVER	WDM1	2151	BODX	ENGL	AGGR	REPL
RCHRES	2	PLANK	TPKCF1	4	SUM	WDM1	2152	TNLD	ENGL	AGGR	REPL
RCHRES	2	PLANK	TPKCF1	5	SUM	WDM1	2153	TPLD	ENGL	AGGR	REPL
RCHRES	2	NUTRX	NUCF1	1	SUM	WDM1	2154	NO3L	ENGL	AGGR	REPL
RCHRES	2	NUTRX	NUCF1	2	SUM	WDM1	2245	NH3L	ENGL	AGGR	REPL
RCHRES	2	NUTRX	NUCF1	4	SUM	WDM1	2246	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Lake Mabel/South Lake

\*\*\* REACH 9 \*\*\*

RCHRES	9	NUTRX	DNUST	1	AVER	WDM1	2155	NO3X	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	2	AVER	WDM1	2156	NH3X	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	4	AVER	WDM1	2157	ORGN	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST4	1	AVER	WDM1	2158	TOTN	ENGL	AGGR	REPL
RCHRES	9	NUTRX	DNUST	4	AVER	WDM1	2159	PO4X	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	5	AVER	WDM1	2160	ORGP	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST4	2	AVER	WDM1	2161	TOTP	ENGL	AGGR	REPL
RCHRES	9	PLANK	PHYTO		AVER	WDM1	2162	CHLA	ENGL	AGGR	REPL
RCHRES	9	PLANK	PKST3	6	AVER	WDM1	2163	TOCX	ENGL	AGGR	REPL
RCHRES	9	OXX	DOX		AVER	WDM1	2164	DOXX	ENGL	AGGR	REPL
RCHRES	9	OXX	BOD		AVER	WDM1	2165	BODX	ENGL	AGGR	REPL
RCHRES	9	PLANK	TPKCF1	4	SUM	WDM1	2166	TNLD	ENGL	AGGR	REPL
RCHRES	9	PLANK	TPKCF1	5	SUM	WDM1	2167	TPLD	ENGL	AGGR	REPL
RCHRES	9	NUTRX	NUCF1	1	SUM	WDM1	2168	NO3L	ENGL	AGGR	REPL
RCHRES	9	NUTRX	NUCF1	2	SUM	WDM1	2247	NH3L	ENGL	AGGR	REPL
RCHRES	9	NUTRX	NUCF1	4	SUM	WDM1	2248	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for Lower L-405 \*\*\*

\*\*\* REACH 6 \*\*\*

RCHRES	6	NUTRX	DNUST	1	AVER	WDM1	2169	NO3X	ENGL	AGGR	REPL
RCHRES	6	NUTRX	DNUST	2	AVER	WDM1	2170	NH3X	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST3	4	AVER	WDM1	2171	ORGN	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST4	1	AVER	WDM1	2172	TOTN	ENGL	AGGR	REPL
RCHRES	6	NUTRX	DNUST	4	AVER	WDM1	2173	PO4X	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST3	5	AVER	WDM1	2174	ORGP	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST4	2	AVER	WDM1	2175	TOTP	ENGL	AGGR	REPL
RCHRES	6	PLANK	PHYTO		AVER	WDM1	2176	CHLA	ENGL	AGGR	REPL
RCHRES	6	PLANK	PKST3	6	AVER	WDM1	2177	TOCX	ENGL	AGGR	REPL
RCHRES	6	OXX	DOX		AVER	WDM1	2178	DOXX	ENGL	AGGR	REPL
RCHRES	6	OXX	BOD		AVER	WDM1	2179	BODX	ENGL	AGGR	REPL
RCHRES	6	PLANK	TPKCF1	4	SUM	WDM1	2180	TNLD	ENGL	AGGR	REPL
RCHRES	6	PLANK	TPKCF1	5	SUM	WDM1	2181	TPLD	ENGL	AGGR	REPL
RCHRES	6	NUTRX	NUCF1	1	SUM	WDM1	2182	NO3L	ENGL	AGGR	REPL
RCHRES	6	NUTRX	NUCF1	2	SUM	WDM1	2249	NH3L	ENGL	AGGR	REPL
RCHRES	6	NUTRX	NUCF1	4	SUM	WDM1	2250	PO4L	ENGL	AGGR	REPL



\*\*\* WQ DSNS for L-103, Buena Vista \*\*\*

\*\*\* REACH 11 \*\*\*

RCHRES	11	NUTRX	DNUST	1	AVER	WDM1	2183	NO3X	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	2	AVER	WDM1	2184	NH3X	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	4	AVER	WDM1	2185	ORGN	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST4	1	AVER	WDM1	2186	TOTN	ENGL	AGGR	REPL
RCHRES	11	NUTRX	DNUST	4	AVER	WDM1	2187	PO4X	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	5	AVER	WDM1	2188	ORGP	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST4	2	AVER	WDM1	2189	TOTP	ENGL	AGGR	REPL
RCHRES	11	PLANK	PHYTO		AVER	WDM1	2190	CHLA	ENGL	AGGR	REPL
RCHRES	11	PLANK	PKST3	6	AVER	WDM1	2191	TOCX	ENGL	AGGR	REPL
RCHRES	11	OXR	DOX		AVER	WDM1	2192	DOXX	ENGL	AGGR	REPL
RCHRES	11	OXR	BOD		AVER	WDM1	2193	BODX	ENGL	AGGR	REPL
RCHRES	11	PLANK	TPKCF1	4	SUM	WDM1	2194	TNLD	ENGL	AGGR	REPL
RCHRES	11	PLANK	TPKCF1	5	SUM	WDM1	2195	TPLD	ENGL	AGGR	REPL
RCHRES	11	NUTRX	NUCF1	1	SUM	WDM1	2196	NO3L	ENGL	AGGR	REPL
RCHRES	11	NUTRX	NUCF1	2	SUM	WDM1	2251	NH3L	ENGL	AGGR	REPL
RCHRES	11	NUTRX	NUCF1	4	SUM	WDM1	2252	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-105 \*\*\*

\*\*\* REACH 10 \*\*\*

RCHRES	10	NUTRX	DNUST	1	AVER	WDM1	2197	NO3X	ENGL	AGGR	REPL
RCHRES	10	NUTRX	DNUST	2	AVER	WDM1	2198	NH3X	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST3	4	AVER	WDM1	2199	ORGN	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST4	1	AVER	WDM1	2200	TOTN	ENGL	AGGR	REPL
RCHRES	10	NUTRX	DNUST	4	AVER	WDM1	2201	PO4X	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST3	5	AVER	WDM1	2202	ORGP	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST4	2	AVER	WDM1	2203	TOTP	ENGL	AGGR	REPL
RCHRES	10	PLANK	PHYTO		AVER	WDM1	2204	CHLA	ENGL	AGGR	REPL
RCHRES	10	PLANK	PKST3	6	AVER	WDM1	2205	TOCX	ENGL	AGGR	REPL
RCHRES	10	OXR	DOX		AVER	WDM1	2206	DOXX	ENGL	AGGR	REPL
RCHRES	10	OXR	BOD		AVER	WDM1	2207	BODX	ENGL	AGGR	REPL
RCHRES	10	PLANK	TPKCF1	4	SUM	WDM1	2208	TNLD	ENGL	AGGR	REPL
RCHRES	10	PLANK	TPKCF1	5	SUM	WDM1	2209	TPLD	ENGL	AGGR	REPL
RCHRES	10	NUTRX	NUCF1	1	SUM	WDM1	2210	NO3L	ENGL	AGGR	REPL
RCHRES	10	NUTRX	NUCF1	2	SUM	WDM1	2253	NH3L	ENGL	AGGR	REPL
RCHRES	10	NUTRX	NUCF1	4	SUM	WDM1	2254	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-403 - EPCOT \*\*\*

\*\*\* REACH 5 \*\*\*

RCHRES	5	NUTRX	DNUST	1	AVER	WDM1	2211	NO3X	ENGL	AGGR	REPL
RCHRES	5	NUTRX	DNUST	2	AVER	WDM1	2212	NH3X	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST3	4	AVER	WDM1	2213	ORGN	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST4	1	AVER	WDM1	2214	TOTN	ENGL	AGGR	REPL
RCHRES	5	NUTRX	DNUST	4	AVER	WDM1	2215	PO4X	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST3	5	AVER	WDM1	2216	ORGP	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST4	2	AVER	WDM1	2217	TOTP	ENGL	AGGR	REPL
RCHRES	5	PLANK	PHYTO		AVER	WDM1	2218	CHLA	ENGL	AGGR	REPL
RCHRES	5	PLANK	PKST3	6	AVER	WDM1	2219	TOCX	ENGL	AGGR	REPL
RCHRES	5	OXR	DOX		AVER	WDM1	2220	DOXX	ENGL	AGGR	REPL
RCHRES	5	OXR	BOD		AVER	WDM1	2221	BODX	ENGL	AGGR	REPL
RCHRES	5	PLANK	TPKCF1	4	SUM	WDM1	2222	TNLD	ENGL	AGGR	REPL
RCHRES	5	PLANK	TPKCF1	5	SUM	WDM1	2223	TPLD	ENGL	AGGR	REPL
RCHRES	5	NUTRX	NUCF1	1	SUM	WDM1	2224	NO3L	ENGL	AGGR	REPL
RCHRES	5	NUTRX	NUCF1	2	SUM	WDM1	2255	NH3L	ENGL	AGGR	REPL
RCHRES	5	NUTRX	NUCF1	4	SUM	WDM1	2256	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for C-4 \*\*\*

\*\*\* REACH 4 \*\*\*

RCHRES	4	NUTRX	DNUST	1	AVER	WDM1	2257	NO3X	ENGL	AGGR	REPL
RCHRES	4	NUTRX	DNUST	2	AVER	WDM1	2258	NH3X	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST3	4	AVER	WDM1	2259	ORGN	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST4	1	AVER	WDM1	2260	TOTN	ENGL	AGGR	REPL
RCHRES	4	NUTRX	DNUST	4	AVER	WDM1	2261	PO4X	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST3	5	AVER	WDM1	2262	ORGP	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST4	2	AVER	WDM1	2263	TOTP	ENGL	AGGR	REPL
RCHRES	4	PLANK	PHYTO		AVER	WDM1	2264	CHLA	ENGL	AGGR	REPL
RCHRES	4	PLANK	PKST3	6	AVER	WDM1	2265	TOCX	ENGL	AGGR	REPL
RCHRES	4	OXX	DOX		AVER	WDM1	2266	DOXX	ENGL	AGGR	REPL
RCHRES	4	OXX	BOD		AVER	WDM1	2267	BODX	ENGL	AGGR	REPL
RCHRES	4	PLANK	TPKCF1	4	SUM	WDM1	2268	TNLD	ENGL	AGGR	REPL
RCHRES	4	PLANK	TPKCF1	5	SUM	WDM1	2269	TPLD	ENGL	AGGR	REPL
RCHRES	4	NUTRX	NUCF1	1	SUM	WDM1	2270	NO3L	ENGL	AGGR	REPL
RCHRES	4	NUTRX	NUCF1	2	SUM	WDM1	2271	NH3L	ENGL	AGGR	REPL
RCHRES	4	NUTRX	NUCF1	4	SUM	WDM1	2272	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for L-107/UPPER C-1 \*\*\*

\*\*\* REACH 12 \*\*\*

RCHRES	12	NUTRX	DNUST	1	AVER	WDM1	2273	NO3X	ENGL	AGGR	REPL
RCHRES	12	NUTRX	DNUST	2	AVER	WDM1	2274	NH3X	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST3	4	AVER	WDM1	2275	ORGN	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST4	1	AVER	WDM1	2276	TOTN	ENGL	AGGR	REPL
RCHRES	12	NUTRX	DNUST	4	AVER	WDM1	2277	PO4X	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST3	5	AVER	WDM1	2278	ORGP	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST4	2	AVER	WDM1	2279	TOTP	ENGL	AGGR	REPL
RCHRES	12	PLANK	PHYTO		AVER	WDM1	2280	CHLA	ENGL	AGGR	REPL
RCHRES	12	PLANK	PKST3	6	AVER	WDM1	2281	TOCX	ENGL	AGGR	REPL
RCHRES	12	OXX	DOX		AVER	WDM1	2282	DOXX	ENGL	AGGR	REPL
RCHRES	12	OXX	BOD		AVER	WDM1	2283	BODX	ENGL	AGGR	REPL
RCHRES	12	PLANK	TPKCF1	4	SUM	WDM1	2284	TNLD	ENGL	AGGR	REPL
RCHRES	12	PLANK	TPKCF1	5	SUM	WDM1	2285	TPLD	ENGL	AGGR	REPL
RCHRES	12	NUTRX	NUCF1	1	SUM	WDM1	2286	NO3L	ENGL	AGGR	REPL
RCHRES	12	NUTRX	NUCF1	2	SUM	WDM1	2287	NH3L	ENGL	AGGR	REPL
RCHRES	12	NUTRX	NUCF1	4	SUM	WDM1	2288	PO4L	ENGL	AGGR	REPL

\*\*\* WQ DSNS for LOWER C-1 \*\*\*

\*\*\* REACH 14 \*\*\*

RCHRES	14	NUTRX	DNUST	1	AVER	WDM1	2289	NO3X	ENGL	AGGR	REPL
RCHRES	14	NUTRX	DNUST	2	AVER	WDM1	2290	NH3X	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST3	4	AVER	WDM1	2291	ORGN	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST4	1	AVER	WDM1	2292	TOTN	ENGL	AGGR	REPL
RCHRES	14	NUTRX	DNUST	4	AVER	WDM1	2293	PO4X	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST3	5	AVER	WDM1	2294	ORGP	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST4	2	AVER	WDM1	2295	TOTP	ENGL	AGGR	REPL
RCHRES	14	PLANK	PHYTO		AVER	WDM1	2296	CHLA	ENGL	AGGR	REPL
RCHRES	14	PLANK	PKST3	6	AVER	WDM1	2297	TOCX	ENGL	AGGR	REPL
RCHRES	14	OXX	DOX		AVER	WDM1	2298	DOXX	ENGL	AGGR	REPL
RCHRES	14	OXX	BOD		AVER	WDM1	2299	BODX	ENGL	AGGR	REPL
RCHRES	14	PLANK	TPKCF1	4	SUM	WDM1	2300	TNLD	ENGL	AGGR	REPL
RCHRES	14	PLANK	TPKCF1	5	SUM	WDM1	2301	TPLD	ENGL	AGGR	REPL
RCHRES	14	NUTRX	NUCF1	1	SUM	WDM1	2302	NO3L	ENGL	AGGR	REPL
RCHRES	14	NUTRX	NUCF1	2	SUM	WDM1	2303	NH3L	ENGL	AGGR	REPL
RCHRES	14	NUTRX	NUCF1	4	SUM	WDM1	2304	PO4L	ENGL	AGGR	REPL

\*\*\* WHITTENHORSE CREEK

\*\*\* All acreage of segment 5 in Whittenhorse basin, i.e. area rch 51

RCHRES	51	HYDR	RO		1.0	WDM	411	FLOW	ENGL	AGGR	REPL
RCHRES	51	ROFLOW	ROVOL		.00163049	WDM	418	SIMQ	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	1	0.0001359	WDM	412	SURO	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	2	0.0001359	WDM	413	IFWO	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	3	0.0001359	WDM	414	AGWO	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	4	0.0001359	WDM	419	PETX	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	5	0.0001359	WDM	415	SAET	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	6	0.0001359	WDM	416	UZSX	ENGL	AGGR	REPL
COPY	102	OUTPUT	MEAN	7	0.0001359	WDM	417	LZSX	ENGL	AGGR	REPL

\*\*\* DAVENPORT CREEK

\*\*\* All acreage of segment 6 in Davenport basin, i.e. area rch 61

RCHRES	61	HYDR	RO		1.0	WDM	421	FLOW	ENGL	AGGR	REPL
RCHRES	61	ROFLOW	ROVOL		.00116923	WDM	428	SIMQ	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	1	0.0000974	WDM	422	SURO	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	2	0.0000974	WDM	423	IFWO	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	3	0.0000974	WDM	424	AGWO	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	4	0.0000974	WDM	429	PETX	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	5	0.0000974	WDM	425	SAET	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	6	0.0000974	WDM	426	UZSX	ENGL	AGGR	REPL
COPY	103	OUTPUT	MEAN	7	0.0000974	WDM	427	LZSX	ENGL	AGGR	REPL

\*\*\* REEDY CREEK @ HWY 192

\*\*\* Sum of areas rch 1, 2 (except half direct lake contrib area), rch 3-7

\*\*\* All segment 3

\*\*\* All Whittenhorse

RCHRES	7	HYDR	RO		1.0	WDM	431	FLOW	ENGL	AGGR	REPL
RCHRES	7	ROFLOW	ROVOL		2.7686E-4	WDM	438	SIMQ	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	1	2.3223E-5	WDM	432	SURO	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	2	2.3223E-5	WDM	433	IFWO	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	3	2.3223E-5	WDM	434	AGWO	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	4	2.3223E-5	WDM	439	PETX	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	5	2.3223E-5	WDM	435	SAET	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	6	2.3223E-5	WDM	436	UZSX	ENGL	AGGR	REPL
COPY	104	OUTPUT	MEAN	7	2.3223E-5	WDM	437	LZSX	ENGL	AGGR	REPL

\*\*\* BONNETT CREEK

\*\*\* Sum of areas rch 2 (except half direct lake contrib area), rch 9-13

\*\*\* All segment 2

RCHRES	13	HYDR	RO		1.0	WDM	441	FLOW	ENGL	AGGR	REPL
RCHRES	13	ROFLOW	ROVOL		1.3820E-3	WDM	448	SIMQ	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	1	1.1517E-4	WDM	442	SURO	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	2	1.1517E-4	WDM	443	IFWO	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	3	1.1517E-4	WDM	444	AGWO	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	4	1.1517E-4	WDM	449	PETX	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	5	1.1517E-4	WDM	445	SAET	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	6	1.1517E-4	WDM	446	UZSX	ENGL	AGGR	REPL
COPY	105	OUTPUT	MEAN	7	1.1517E-4	WDM	447	LZSX	ENGL	AGGR	REPL

\*\*\* REEDY CREEK @ LOUGHMAN

\*\*\* All segments 1-6

Code	Segment	Type	Value	Code	Segment	Type	Value	Code	Segment	Type	Value
RCHRES	16	HYDR RO	1.0	WDM	451	FLOW		ENGL	AGGR	REPL	
RCHRES	16	ROFLOW ROVOL	1.5678E-4	WDM	458	SIMQ		ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	1	1.3065E-5	WDM	452	SURO	ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	2	1.3065E-5	WDM	453	IFWO	ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	3	1.3065E-5	WDM	454	AGWO	ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	4	1.3065E-5	WDM	459	PETX	ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	5	1.3065E-5	WDM	455	SAET	ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	6	1.3065E-5	WDM	456	UZSX	ENGL	AGGR	REPL	
COPY	106	OUTPUT MEAN	7	1.3065E-5	WDM	457	LZSX	ENGL	AGGR	REPL	

END EXT TARGETS

SCHEMATIC

<-Volume->		<--Area-->		<-Volume->		<ML#>	***
<Name>	x	<-factor->		<Name>	x		***
*** Internal Basin							
PERLND	11	***	0.0	RCHRES	2	1	
PERLND	12		4.4	RCHRES	2	1	
PERLND	13	***	0.0	RCHRES	2	1	
PERLND	14		3.5	RCHRES	2	1	
PERLND	15		0.5	RCHRES	2	1	
IMPLND	14		19.6	RCHRES	2	2	
PERLND	11		2.0	RCHRES	3	1	
PERLND	12		219.6	RCHRES	3	1	
PERLND	13		1.3	RCHRES	3	1	
PERLND	14		287.3	RCHRES	3	1	
PERLND	15		555.7	RCHRES	3	1	
IMPLND	14		1622.3	RCHRES	3	2	
PERLND	11		149.8	RCHRES	4	1	
PERLND	12		65.5	RCHRES	4	1	
PERLND	13		5.5	RCHRES	4	1	
PERLND	14		192.7	RCHRES	4	1	
PERLND	16		792.8	RCHRES	4	1	
PERLND	19	***	0.0	RCHRES	4	1	
IMPLND	14		1904.0	RCHRES	4	2	
PERLND	11	***	0.0	RCHRES	5	1	
PERLND	12		4.4	RCHRES	5	1	
PERLND	13	***	0.0	RCHRES	5	1	
PERLND	14		96.7	RCHRES	5	1	
PERLND	15		86.6	RCHRES	5	1	
IMPLND	14		548.2	RCHRES	5	2	
PERLND	11		549.3	RCHRES	6	1	
PERLND	12		190.5	RCHRES	6	1	
PERLND	13		981.1	RCHRES	6	1	
PERLND	14		1006.9	RCHRES	6	1	
PERLND	16		3188.3	RCHRES	6	1	
IMPLND	14		2116.3	RCHRES	6	2	
PERLND	11		1.6	RCHRES	7	1	

PERLND	12		27.7	RCHRES	7	1
PERLND	13		31.7	RCHRES	7	1
PERLND	14		302.3	RCHRES	7	1
PERLND	15		1041.3	RCHRES	7	1
IMPLND	14		1675.8	RCHRES	7	2
PERLND	11		1088.3	RCHRES	8	1
PERLND	12		267.8	RCHRES	8	1
PERLND	13		189.5	RCHRES	8	1
PERLND	14		40.3	RCHRES	8	1
PERLND	18		1636.3	RCHRES	8	1
IMPLND	14		227.4	RCHRES	8	2
PERLND	11		138.2	RCHRES	9	1
PERLND	12		20.9	RCHRES	9	1
PERLND	13		163.5	RCHRES	9	1
PERLND	14		214.9	RCHRES	9	1
PERLND	15		447.2	RCHRES	9	1
IMPLND	14		68.2	RCHRES	9	2
PERLND	11	***	0.0	RCHRES	10	1
PERLND	12		0.2	RCHRES	10	1
PERLND	13		9.1	RCHRES	10	1
PERLND	14		79.0	RCHRES	10	1
PERLND	15		283.9	RCHRES	10	1
IMPLND	14		447.6	RCHRES	10	2
PERLND	11	***	0.0	RCHRES	11	1
PERLND	12		99.1	RCHRES	11	1
PERLND	13		8.8	RCHRES	11	1
PERLND	14		126.0	RCHRES	11	1
PERLND	15		333.8	RCHRES	11	1
IMPLND	14		1529.2	RCHRES	11	2
PERLND	11		60.9	RCHRES	12	1
PERLND	12		89.9	RCHRES	12	1
PERLND	13		15.6	RCHRES	12	1
PERLND	14		213.8	RCHRES	12	1
PERLND	15		822.8	RCHRES	12	1
IMPLND	14		806.2	RCHRES	12	2
PERLND	11	***	0.0	RCHRES	13	1
PERLND	12		202.8	RCHRES	13	1
PERLND	13		942.6	RCHRES	13	1
PERLND	14		87.7	RCHRES	13	1
PERLND	15		724.6	RCHRES	13	1
IMPLND	14		567.7	RCHRES	13	2
PERLND	11		332.8	RCHRES	14	1
PERLND	12		114.3	RCHRES	14	1
PERLND	13		684.0	RCHRES	14	1
PERLND	14		265.1	RCHRES	14	1
PERLND	17		2304.1	RCHRES	14	1
IMPLND	14		884.7	RCHRES	14	2

PERLND	11		1319.6	RCHRES	15	1
PERLND	12		120.3	RCHRES	15	1
PERLND	13		1267.8	RCHRES	15	1
PERLND	14		471.7	RCHRES	15	1
PERLND	18		2925.2	RCHRES	15	1
IMPLND	14		225.0	RCHRES	15	2
PERLND	11	***	0.0	RCHRES	16	1
PERLND	12		111.3	RCHRES	16	1
PERLND	13		530.0	RCHRES	16	1
PERLND	14		47.6	RCHRES	16	1
PERLND	18		1098.5	RCHRES	16	1
IMPLND	14		19.8	RCHRES	16	2
*** East Upper Reedy						
PERLND	31		2160.1	RCHRES	31	1
PERLND	32		169.6	RCHRES	31	1
PERLND	33		2305.3	RCHRES	31	1
PERLND	34		64.3	RCHRES	31	1
PERLND	35		2656.7	RCHRES	31	1
IMPLND	34		30.1	RCHRES	31	2
*** West Upper Reedy						
PERLND	31		3806.0	RCHRES	41	1
PERLND	32		215.9	RCHRES	41	1
PERLND	33		3555.4	RCHRES	41	1
PERLND	34		197.4	RCHRES	41	1
PERLND	35		2085.8	RCHRES	41	1
PERLND	39	***	0.0	RCHRES	41	1
IMPLND	34		392.6	RCHRES	41	2
*** Whittenhorse						
PERLND	51		2002.0	RCHRES	51	1
PERLND	52		173.3	RCHRES	51	1
PERLND	53		1398.0	RCHRES	51	1
PERLND	54		165.9	RCHRES	51	1
PERLND	55		3200.9	RCHRES	51	1
PERLND	59	***	0.0	RCHRES	51	1
IMPLND	54		428.5	RCHRES	51	2
*** Davenport						
PERLND	61		4863.9	RCHRES	61	1
PERLND	62		299.4	RCHRES	61	1
PERLND	63		1706.0	RCHRES	61	1
PERLND	64		388.9	RCHRES	61	1
PERLND	65		2853.8	RCHRES	61	1
IMPLND	64		156.3	RCHRES	61	2
*** Reach Connections						
RCHRES	31			RCHRES	3	3
RCHRES	41			RCHRES	4	3
RCHRES	51			RCHRES	4	3
RCHRES	2			RCHRES	3	4
RCHRES	2			RCHRES	10	5
RCHRES	3			RCHRES	6	3

RCHRES	4		RCHRES	6	3
RCHRES	5		RCHRES	6	3
RCHRES	6		RCHRES	7	3
RCHRES	7		RCHRES	8	3
RCHRES	8		RCHRES	15	3
RCHRES	9		RCHRES	12	3
RCHRES	10		RCHRES	12	3
RCHRES	11		RCHRES	13	3
RCHRES	12		RCHRES	13	3
RCHRES	13		RCHRES	14	3
RCHRES	14		RCHRES	15	3
RCHRES	61		RCHRES	15	3
RCHRES	15		RCHRES	16	5

\*\*\* HSPEXP Datasets

\*\*\* Whittenhorse 02266200

\*\*\* All acreage of Segment 5

PERLND	51	2002.0	COPY	102	90	
PERLND	52	173.3	COPY	102	90	
PERLND	53	1398.0	COPY	102	90	
PERLND	54	165.9	COPY	102	90	
PERLND	55	3200.9	COPY	102	90	
PERLND	59	***	0.0	COPY	102	90
IMPLND	54	428.5	COPY	102	91	

\*\*\* Davenport 02266480

\*\*\* All acreage of Segment 6

PERLND	61	4863.9	COPY	103	90
PERLND	62	299.4	COPY	103	90
PERLND	63	1706.0	COPY	103	90
PERLND	64	388.9	COPY	103	90
PERLND	65	2853.8	COPY	103	90
IMPLND	64	156.3	COPY	103	91

\*\*\* Reedy @ Hwy 192 02266300

\*\*\* sum areas rch 1, 2 (except half direct lake contrib area), 3-7

PERLND	11	8670.8	COPY	104	90	
PERLND	12	1068.7	COPY	104	90	
PERLND	13	8278.3	COPY	104	90	
PERLND	14	2315.2	COPY	104	90	
PERLND	15	9627.4	COPY	104	90	
PERLND	16	3981.1	COPY	104	90	
PERLND	19	***	0.0	COPY	104	90
IMPLND	14	7503.0	COPY	104	91	

\*\*\* all Segment 3

PERLND	31	5966.1	COPY	104	90	
PERLND	32	385.5	COPY	104	90	
PERLND	33	5860.7	COPY	104	90	
PERLND	34	261.7	COPY	104	90	
PERLND	35	4742.5	COPY	104	90	
PERLND	39	***	0.0	COPY	104	90
IMPLND	34	422.7	COPY	104	91	

\*\*\* all Whittenhorse

PERLND	51		2002.0	COPY	104	90
PERLND	52		173.3	COPY	104	90
PERLND	53		1398.0	COPY	104	90
PERLND	54		165.9	COPY	104	90
PERLND	55		3200.9	COPY	104	90
PERLND	59	***	0.0	COPY	104	90
IMPLND	54		428.5	COPY	104	91

\*\*\* Bonnett 02264100

\*\*\* sum areas rch 2 (half lake contrib area only), 9-13

PERLND	11		199.1	COPY	105	90
PERLND	12		415.2	COPY	105	90
PERLND	13		1139.6	COPY	105	90
PERLND	14		723.2	COPY	105	90
PERLND	15		2612.5	COPY	105	90
IMPLND	14		3428.8	COPY	105	91

\*\*\* Reedy @ Loughman 02266500

\*\*\* all segment 1

PERLND	11		3642.3	COPY	106	90
PERLND	12		1538.9	COPY	106	90
PERLND	13		4830.5	COPY	106	90
PERLND	14		3435.4	COPY	106	90
PERLND	15		4296.3	COPY	106	90
PERLND	16		3981.1	COPY	106	90
PERLND	17		2304.1	COPY	106	90
PERLND	18		5660.0	COPY	106	90
PERLND	19	***	0.0	COPY	106	90
IMPLND	14		11437.6	COPY	106	91

\*\*\* all segment 3

PERLND	31		5966.1	COPY	106	90
PERLND	32		385.5	COPY	106	90
PERLND	33		5860.7	COPY	106	90
PERLND	34		261.7	COPY	106	90
PERLND	35		4742.5	COPY	106	90
PERLND	39	***	0.0	COPY	106	90
IMPLND	34		422.7	COPY	106	91

\*\*\* all segment 5

PERLND	51		2002.0	COPY	106	90
PERLND	52		173.3	COPY	106	90
PERLND	53		1398.0	COPY	106	90
PERLND	54		165.9	COPY	106	90
PERLND	55		3200.9	COPY	106	90
PERLND	59	***	0.0	COPY	106	90
IMPLND	54		428.5	COPY	106	91

\*\*\* All Segment 6

PERLND	61		4863.9	COPY	106	90
PERLND	62		299.4	COPY	106	90
PERLND	63		1706.0	COPY	106	90
PERLND	64		388.9	COPY	106	90
PERLND	65		2853.8	COPY	106	90
IMPLND	64		156.3	COPY	106	91



\*\*\* Total loadings report

\*\*\* all segment 1

PERLND	11	3642.3	REPORT	1	8	1
PERLND	12	1538.9	REPORT	1	8	2
PERLND	13	4830.5	REPORT	1	8	3
PERLND	14	3435.4	REPORT	1	8	4
PERLND	15	4296.3	REPORT	1	8	5
PERLND	16	3981.1	REPORT	1	8	5
PERLND	17	2304.1	REPORT	1	8	5
PERLND	18	5660.0	REPORT	1	8	5
PERLND	19	*** 0.0	REPORT	1	8	6
IMPLND	14	11437.6	REPORT	1	9	7

\*\*\* all segment 3

PERLND	31	5966.1	REPORT	3	8	1
PERLND	32	385.5	REPORT	3	8	2
PERLND	33	5860.7	REPORT	3	8	3
PERLND	34	261.7	REPORT	3	8	4
PERLND	35	4742.5	REPORT	3	8	5
PERLND	39	*** 0.0	REPORT	3	8	6
IMPLND	34	422.7	REPORT	3	9	7

\*\*\* all segment 5

PERLND	51	2002.0	REPORT	5	8	1
PERLND	52	173.3	REPORT	5	8	2
PERLND	53	1398.0	REPORT	5	8	3
PERLND	54	165.9	REPORT	5	8	4
PERLND	55	3200.9	REPORT	5	8	5
PERLND	59	*** 0.0	REPORT	5	8	6
IMPLND	54	428.5	REPORT	5	9	7

\*\*\* all segment 6

PERLND	61	4863.9	REPORT	6	8	1
PERLND	62	299.4	REPORT	6	8	2
PERLND	63	1706.0	REPORT	6	8	3
PERLND	64	388.9	REPORT	6	8	4
PERLND	65	2853.8	REPORT	6	8	5
IMPLND	64	156.3	REPORT	6	9	7

\*\*\* Per acre loadings report \*\*\*

\*\*\* all segment 1

PERLND	11		REPORT	11	8	1
PERLND	12		REPORT	11	8	2
PERLND	13		REPORT	11	8	3
PERLND	14		REPORT	11	8	4
PERLND	15	.3444	REPORT	11	8	5
PERLND	16	.2361	REPORT	11	8	5
PERLND	17	.1282	REPORT	11	8	5
PERLND	18	.2913	REPORT	11	8	5
PERLND	19		REPORT	11	8	6
IMPLND	14		REPORT	11	9	7

```

*** all segment 3
PERLND 31          REPORT 13      8      1
PERLND 32          REPORT 13      8      2
PERLND 33          REPORT 13      8      3
PERLND 34          REPORT 13      8      4
PERLND 35          REPORT 13      8      5
PERLND 39          REPORT 13      8      6
IMPLND 34          REPORT 13      9      7

*** all segment 5
PERLND 51          REPORT 15      8      1
PERLND 52          REPORT 15      8      2
PERLND 53          REPORT 15      8      3
PERLND 54          REPORT 15      8      4
PERLND 55          REPORT 15      8      5
PERLND 59          REPORT 15      8      6
IMPLND 54          REPORT 15      9      7

*** all segment 6
PERLND 61          REPORT 16      8      1
PERLND 62          REPORT 16      8      2
PERLND 63          REPORT 16      8      3
PERLND 64          REPORT 16      8      4
PERLND 65          REPORT 16      8      5
IMPLND 64          REPORT 16      9      7

*** Percent loads report
*** all segment 1
PERLND 11          3642.3    REPORT 21      8      1
PERLND 12          1538.9    REPORT 21      8      2
PERLND 13          4830.5    REPORT 21      8      3
PERLND 14          3435.4    REPORT 21      8      4
PERLND 15          4296.3    REPORT 21      8      5
PERLND 16          3981.1    REPORT 21      8      5
PERLND 17          2304.1    REPORT 21      8      5
PERLND 18          5660.0    REPORT 21      8      5
PERLND 19          ***      0.0      REPORT 21      8      6
IMPLND 14          11437.6   REPORT 21      9      7

*** all segment 3
PERLND 31          5966.1    REPORT 23      8      1
PERLND 32          385.5     REPORT 23      8      2
PERLND 33          5860.7    REPORT 23      8      3
PERLND 34          261.7     REPORT 23      8      4
PERLND 35          4742.5    REPORT 23      8      5
PERLND 39          ***      0.0      REPORT 23      8      6
IMPLND 34          422.7     REPORT 23      9      7

*** all segment 5
PERLND 51          2002.0    REPORT 25      8      1
PERLND 52          173.3     REPORT 25      8      2
PERLND 53          1398.0    REPORT 25      8      3
PERLND 54          165.9     REPORT 25      8      4
PERLND 55          3200.9    REPORT 25      8      5
PERLND 59          ***      0.0      REPORT 25      8      6
IMPLND 54          428.5     REPORT 25      9      7

```

\*\*\* all segment 6

PERLND	61	4863.9	REPORT	26	8	1
PERLND	62	299.4	REPORT	26	8	2
PERLND	63	1706.0	REPORT	26	8	3
PERLND	64	388.9	REPORT	26	8	4
PERLND	65	2853.8	REPORT	26	8	5
IMPLND	64	156.3	REPORT	26	9	7

RCHRES	31		REPORT	100	10	1
RCHRES	41		REPORT	100	10	2
RCHRES	51		REPORT	100	10	3
RCHRES	61		REPORT	100	10	4
RCHRES	2		REPORT	100	10	5
RCHRES	3		REPORT	100	10	6
RCHRES	4		REPORT	100	10	7
RCHRES	5		REPORT	100	10	8
RCHRES	6		REPORT	100	10	9
RCHRES	7		REPORT	100	10	10
RCHRES	8		REPORT	100	10	11
RCHRES	9		REPORT	100	10	12
RCHRES	10		REPORT	100	10	13
RCHRES	11		REPORT	100	10	14
RCHRES	12		REPORT	100	10	15
RCHRES	13		REPORT	100	10	16
RCHRES	14		REPORT	100	10	17
RCHRES	15		REPORT	100	10	18
RCHRES	16		REPORT	100	10	19

END SCHEMATIC

MASS-LINK

MASS-LINK		10						
<-Volume->	<-Grp>	<-Member->	<--Mult-->	Tran	<-Target vols>	<-Grp>	<-Member->	***
<Name>		<Name>	x	x<-factor->	strg	<Name>	<Name>	x x ***
RCHRES	OXR	OXIF	1		REPORT	INPUT	TIMSER 1	
RCHRES	OXR	OXCF3	1		REPORT	INPUT	TIMSER 2	
RCHRES	OXR	OXCF3	2		REPORT	INPUT	TIMSER 3	
RCHRES	OXR	OXCF3	3		REPORT	INPUT	TIMSER 4	
RCHRES	OXR	OXCF3	4		REPORT	INPUT	TIMSER 5	
RCHRES	OXR	OXCF3	5		REPORT	INPUT	TIMSER 6	
RCHRES	OXR	OXIF	2		REPORT	INPUT	TIMSER 7	
RCHRES	OXR	OXCF4	1		REPORT	INPUT	TIMSER 8	
RCHRES	OXR	OXCF4	2		REPORT	INPUT	TIMSER 9	
RCHRES	OXR	OXCF4	3		REPORT	INPUT	TIMSER10	
RCHRES	OXR	OXCF4	4		REPORT	INPUT	TIMSER11	
RCHRES	OXR	OXCF4	5		REPORT	INPUT	TIMSER12	
RCHRES	NUTRX	NUIF1	2		REPORT	INPUT	TIMSER13	
RCHRES	NUTRX	NUCF5	1		REPORT	INPUT	TIMSER14	
RCHRES	NUTRX	NUCF5	2		REPORT	INPUT	TIMSER15	
RCHRES	NUTRX	NUCF5	3		REPORT	INPUT	TIMSER16	
RCHRES	NUTRX	NUCF5	4		REPORT	INPUT	TIMSER17	
RCHRES	NUTRX	NUCF5	5		REPORT	INPUT	TIMSER18	
RCHRES	NUTRX	NUIF1	1		REPORT	INPUT	TIMSER19	
RCHRES	NUTRX	NUCF4	1		REPORT	INPUT	TIMSER20	

RCHRES	NUTRX	NUCF4	2	REPORT	INPUT	TIMSER21
RCHRES	NUTRX	NUCF4	3	REPORT	INPUT	TIMSER22
RCHRES	NUTRX	NUCF4	4	REPORT	INPUT	TIMSER23
RCHRES	NUTRX	NUIF1	4	REPORT	INPUT	TIMSER24
RCHRES	NUTRX	NUCF7	1	REPORT	INPUT	TIMSER25
RCHRES	NUTRX	NUCF7	2	REPORT	INPUT	TIMSER26
RCHRES	NUTRX	NUCF7	3	REPORT	INPUT	TIMSER27
RCHRES	PLANK	PKIF	1	REPORT	INPUT	TIMSER28
RCHRES	PLANK	PKCF5	1	REPORT	INPUT	TIMSER29
RCHRES	PLANK	PKCF5	3	REPORT	INPUT	TIMSER30
RCHRES	PLANK	PKCF5	4	REPORT	INPUT	TIMSER31
RCHRES	PLANK	PKIF	3	REPORT	INPUT	TIMSER32
RCHRES	PLANK	PKCF8	1	REPORT	INPUT	TIMSER33
RCHRES	PLANK	PKCF8	2	REPORT	INPUT	TIMSER34
RCHRES	PLANK	PKIF	4	REPORT	INPUT	TIMSER35
RCHRES	PLANK	PKCF9	1	REPORT	INPUT	TIMSER36
RCHRES	PLANK	PKCF9	2	REPORT	INPUT	TIMSER37
RCHRES	PLANK	PKIF	5	REPORT	INPUT	TIMSER38
RCHRES	PLANK	PKCF10	1	REPORT	INPUT	TIMSER39
RCHRES	PLANK	PKCF10	2	REPORT	INPUT	TIMSER40

END MASS-LINK 10

MASS-LINK 9

<-Volume->	<-Grp>	<-Member->	<--Mult-->	Tran	<-Target vols>	<-Grp>	<-Member->	***
<Name>		<Name>	x	x<-factor->	strg	<Name>	<Name>	x x
IMPLND	IQUAL	SOQUAL	1		REPORT	INPUT	TIMSER	1
IMPLND	IQUAL	SOQUAL	2		REPORT	INPUT	TIMSER	2
IMPLND	IQUAL	SOQUAL	4	0.0480	REPORT	INPUT	TIMSER	3
IMPLND	IQUAL	SOQUAL	1		REPORT	INPUT	TIMSER	4
IMPLND	IQUAL	SOQUAL	2		REPORT	INPUT	TIMSER	4
IMPLND	IQUAL	SOQUAL	4	0.0480	REPORT	INPUT	TIMSER	4
IMPLND	IQUAL	SOQUAL	3		REPORT	INPUT	TIMSER	5
IMPLND	IQUAL	SOQUAL	4	0.0023	REPORT	INPUT	TIMSER	6
IMPLND	IQUAL	SOQUAL	3		REPORT	INPUT	TIMSER	7
IMPLND	IQUAL	SOQUAL	4	0.0023	REPORT	INPUT	TIMSER	7
IMPLND	IQUAL	SOQUAL	4	0.400	REPORT	INPUT	TIMSER	8
IMPLND	IQUAL	SOQUAL	4	0.301	REPORT	INPUT	TIMSER	9

END MASS-LINK 9

MASS-LINK 8

<-Volume->	<-Grp>	<-Member->	<--Mult-->	Tran	<-Target vols>	<-Grp>	<-Member->	***
<Name>		<Name>	x	x<-factor->	strg	<Name>	<Name>	x x
PERLND	PQUAL	POQUAL	1		REPORT	INPUT	TIMSER	1
PERLND	PQUAL	POQUAL	2		REPORT	INPUT	TIMSER	2
PERLND	PQUAL	POQUAL	4	0.0480	REPORT	INPUT	TIMSER	3
PERLND	PQUAL	POQUAL	1		REPORT	INPUT	TIMSER	4
PERLND	PQUAL	POQUAL	2		REPORT	INPUT	TIMSER	4
PERLND	PQUAL	POQUAL	4	0.0480	REPORT	INPUT	TIMSER	4
PERLND	PQUAL	POQUAL	3		REPORT	INPUT	TIMSER	5
PERLND	PQUAL	POQUAL	4	0.0023	REPORT	INPUT	TIMSER	6
PERLND	PQUAL	POQUAL	3		REPORT	INPUT	TIMSER	7
PERLND	PQUAL	POQUAL	4	0.0023	REPORT	INPUT	TIMSER	7
PERLND	PQUAL	POQUAL	4	0.400	REPORT	INPUT	TIMSER	8
PERLND	PQUAL	POQUAL	4	0.301	REPORT	INPUT	TIMSER	9

END MASS-LINK 8

```

    MASS-LINK          1
<-Volume-> <-Grp> <-Member-><--Mult--> Tran<-Target vols> <-Grp> <-Member->***
<Name>***          <Name> x x<-factor-> strg<Name>          <Name> x x
PERLND    PWATER  PERO          0.0833333    RCHRES          INFLOW  IVOL
PERLND    PWTGAS  PODOXM          RCHRES          INFLOW  OXIF    1
PERLND    PQUAL  POQUAL  1          RCHRES          INFLOW  NUIF1   2
PERLND    PQUAL  POQUAL  2          RCHRES          INFLOW  NUIF1   1
PERLND    PQUAL  POQUAL  3          RCHRES          INFLOW  NUIF1   4
PERLND    PQUAL  POQUAL  4          0.40           RCHRES          INFLOW  OXIF    2
PERLND    PQUAL  POQUAL  4          0.048          RCHRES          INFLOW  PKIF    3
PERLND    PQUAL  POQUAL  4          0.0023         RCHRES          INFLOW  PKIF    4
PERLND    PQUAL  POQUAL  4          0.301          RCHRES          INFLOW  PKIF    5
    END MASS-LINK    1

    MASS-LINK          2
<-Volume-> <-Grp> <-Member-><--Mult--> Tran<-Target vols> <-Grp> <-Member->***
<Name>***          <Name> x x<-factor-> strg<Name>          <Name> x x
IMPLND    IWATER  SURO          0.0833333    RCHRES          INFLOW  IVOL
IMPLND    IWTGAS  SODOXM          RCHRES          INFLOW  OXIF    1
IMPLND    IQUAL   SOQUAL  1          RCHRES          INFLOW  NUIF1   2
IMPLND    IQUAL   SOQUAL  2          RCHRES          INFLOW  NUIF1   1
IMPLND    IQUAL   SOQUAL  3          RCHRES          INFLOW  NUIF1   4
IMPLND    IQUAL   SOQUAL  4          0.40           RCHRES          INFLOW  OXIF    2
IMPLND    IQUAL   SOQUAL  4          0.048          RCHRES          INFLOW  PKIF    3
IMPLND    IQUAL   SOQUAL  4          0.0023         RCHRES          INFLOW  PKIF    4
IMPLND    IQUAL   SOQUAL  4          0.301          RCHRES          INFLOW  PKIF    5
    END MASS-LINK    2

    MASS-LINK          3
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    ROFLOW          RCHRES          INFLOW
    END MASS-LINK    3

    MASS-LINK          4
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          1          RCHRES          INFLOW
    END MASS-LINK    4

    MASS-LINK          5
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          2          RCHRES          INFLOW
    END MASS-LINK    5

    MASS-LINK          6
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          3          RCHRES          INFLOW
    END MASS-LINK    6

    MASS-LINK          7
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
RCHRES    OFLOW          4          RCHRES          INFLOW
    END MASS-LINK    7

```

```

    MASS-LINK          90
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
PERLND    PWATER  SURO          COPY          INPUT  MEAN    1
PERLND    PWATER  IFWO          COPY          INPUT  MEAN    2
PERLND    PWATER  AGWO          COPY          INPUT  MEAN    3
PERLND    PWATER  PET           COPY          INPUT  MEAN    4
PERLND    PWATER  TAET          COPY          INPUT  MEAN    5
PERLND    PWATER  UZS           COPY          INPUT  MEAN    6
PERLND    PWATER  LZS           COPY          INPUT  MEAN    7
    END MASS-LINK    90

```

```

    MASS-LINK          91
<-Volume-> <-Grp> <-Member-><--Mult-->Tran <-Target vols> <-Grp> <-Member-> ***
<Name>          <Name> x x<-factor->strg <Name>          <Name> x x ***
IMPLND    IWATER  SURO          COPY          INPUT  MEAN    1
IMPLND    IWATER  PET           COPY          INPUT  MEAN    4
IMPLND    IWATER  IMPEV         COPY          INPUT  MEAN    5
    END MASS-LINK    91
END MASS-LINK

```

FTABLES

```

    FTABLE          2
    14      5
    DEPTH          AREA          VOLUME          DISCH1          DISCH2 ***
    (FT)          (ACRES)        (AC-FT)         (CFS)           (CFS) ***
    0.0           0.0           0.0            0              0
    1.0           2.1           0.7            0              0
    6.0           8.2           29.9           0              0
    10.0          36.9          123.3          0              0
    14.0          124.6         408.1          0              0
    18.0          332.5         1054.3         0              0
    22.0          411.2         2424.5         0              0
    26.0          466.4         4185.8         0              0
    30.0          524.2         6178.6         0              0
    31.0          527.1         6702.8         0              0
    32.0          569.8         7229.9         0              0
    33.0          583.5         7745.6         52.00          208.01
    34.0          596.5         8266.5         104.52          418.08
    35.0          611.5         8788.3         157.14          628.55
    END FTABLE    2

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    FTABLE          3
    15      4
    DEPTH          AREA          VOLUME          DISCH ***
    (FT)          (ACRES)        (AC-FT)         (CFS) ***
    0.00           0.0           0.0            0.0
    0.74           25.1          17.1            13.6
    1.48           29.0          37.0            44.7
    2.21           32.9          59.9            91.3
    2.95           36.8          85.6            153.6
    3.69           40.7          114.2           231.9
    4.43           44.6          145.6           327.0
    5.90           52.4          217.2           570.9

```

7.38	60.2	300.2	892.0
8.85	68.0	394.8	1297.
11.80	635.5	1432.5	3104.
14.75	1203.1	4144.4	7550.
17.70	1770.6	8530.5	16025.
20.65	2338.1	14590.8	29680.
23.60	2905.6	22325.3	49543.

END FTABLE 3

FTABLE 4

15 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
1.00	2.3	1.9	0.2	
2.00	3.2	4.6	0.9	
3.00	4.1	8.2	1.9	
4.00	4.9	12.7	3.5	
5.00	5.8	18.1	5.6	
6.00	6.7	24.4	8.3	
8.00	8.5	39.5	15.9	
10.00	10.2	58.2	26.6	
12.00	12.0	80.4	40.9	
16.00	306.5	717.4	123.2	
20.00	601.0	2532.4	367.5	
24.00	895.5	5525.4	863.3	
28.00	1190.0	9696.5	1685.	
32.00	1484.5	15045.6	2898.	

END FTABLE 4

FTABLE 5

15 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
1.33	14.3	17.6	128.9	
2.67	16.7	38.3	423.1	
4.00	19.0	62.1	863.4	
5.33	21.4	89.0	1451.	
6.67	23.7	119.1	2190.	
8.00	26.0	152.2	3090.	
10.67	30.7	227.9	5399.	
13.33	35.4	316.1	8445.	
16.00	40.1	416.8	12294.	
21.33	660.3	2284.6	26168.	
26.67	1280.6	7460.3	50366.	
32.00	1900.8	15944.0	89001.	
37.33	2521.0	27735.5	145505.	
42.67	3141.3	42835.0	222956.	

END FTABLE 5

```

FTABLE      6
  15      4
    DEPTH      AREA      VOLUME      DISCH ***
      (FT)    (ACRES)    (AC-FT)    (CFS) ***
    0.00      0.0      0.0      0.0
    0.57     11.5      6.2      5.9
    1.13     12.7     13.0     19.1
    1.70     13.9     20.5     38.4
    2.27     15.1     28.7     63.4
    2.83     16.2     37.6     94.3
    3.40     17.4     47.1    131.0
    4.53     19.8     68.2    222.4
    5.67     22.2     92.0    339.0
    6.80     24.5    118.5    482.3
    9.07    220.8    396.5    997.8
   11.33   417.0   1119.4   1973.
   13.60   613.3   2287.1   3616.
   15.87   809.5   3899.7   6102.
   18.13  1005.8   5957.0   9584.
END FTABLE  6

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```

FTABLE      7
  15      4
    DEPTH      AREA      VOLUME      DISCH ***
      (FT)    (ACRES)    (AC-FT)    (CFS) ***
    0.00      0.0      0.0      0.0
    0.38    269.6     98.3     56.7
    0.77    296.0    206.7    184.0
    1.15    322.3    325.2    369.9
    1.53    348.7    453.8    611.7
    1.92    375.0    592.6    909.0
    2.30    401.4    741.4   1262.
    3.07    454.1   1069.3   2140.
    3.83    506.8   1437.7   3258.
    4.60    559.5   1846.4   4629.
    6.13    666.1   2786.1   8807.
    7.67    772.7   3889.2  14237.
    9.20    879.3   5155.6  20997.
   10.73    985.8   6585.5  29160.
   12.27   1092.4   8178.9  38800.
END FTABLE  7

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FTABLE      8
  15      4
    DEPTH      AREA      VOLUME      DISCH ***
      (FT)    (ACRES)    (AC-FT)    (CFS) ***
    0.00      0.0      0.0      0.0
    0.54     87.7     42.1     14.4
    1.08    107.6     95.0     48.7
    1.63    127.5    158.7    102.4
    2.17    147.4    233.1    176.5
    2.71    167.3    318.4    272.6
    3.25    187.2    414.4    392.5
    4.33    227.1    638.8    710.0
    5.42    266.9    906.4   1142.

```



6.50	306.7	1217.1	1701.
8.67	495.7	2086.4	3614.
10.83	684.7	3365.2	6436.
13.00	873.8	5053.6	10376.
15.17	1062.8	7151.5	15616.
17.33	1251.8	9658.9	22317.

END FTABLE 8

FTABLE		9		
10	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0	0	0	0	
0.01	406.641	0	0	
1	421.107	445.873	0	
2	435.720	896.251	0	
3	450.332	1346.628	0	
4	464.945	1797.005	0	
5	479.557	2247.382	0	
6	494.170	2697.760	0	
7	508.783	3148.137	227.1	
8	523.395	3598.514	454.1	

END FTABLE 9

FTABLE		10		
15	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0.00	0.0	0.0	0.0	
1.71	2.9	3.5	8.1	
3.42	4.4	9.8	32.4	
5.13	6.0	18.7	77.7	
6.83	7.6	30.3	148.3	
8.54	9.2	44.6	248.7	
10.25	10.7	61.6	382.6	
13.67	13.9	103.6	765.8	
17.08	17.0	156.4	1326.	
20.50	20.2	219.9	2089.	
27.33	439.0	1788.9	6256.	
34.17	857.9	6220.1	17971.	
41.00	1276.8	13513.7	41312.	
47.83	1695.7	23669.6	79656.	
54.67	2114.5	36687.8	136014.	

END FTABLE 10

FTABLE		11		
15	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0.00	0.0	0.0	0.0	
1.00	4.4	3.6	7.8	
2.00	6.0	8.8	28.0	
3.00	7.6	15.6	61.6	
4.00	9.2	24.0	110.6	
5.00	10.8	34.0	177.0	

6.00	12.4	45.6	262.6
8.00	15.6	73.5	498.6
10.00	18.7	107.8	832.1
12.00	21.9	148.5	1276.
16.00	425.9	1044.0	3792.
20.00	829.8	3555.3	11204.
24.00	1233.8	7682.5	26215.
28.00	1637.7	13425.4	51062.
32.00	2041.7	20784.1	87738.

END FTABLE 11

FTABLE		12		
15	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0.00	0.0	0.0	0.0	
1.27	14.6	14.7	16.8	
2.54	20.6	37.2	62.0	
3.81	26.7	67.2	139.9	
5.08	32.7	104.9	256.1	
6.35	38.7	150.3	415.9	
7.63	44.8	203.4	624.3	
10.17	56.8	332.5	1206.	
12.71	68.9	492.2	2039.	
15.25	80.9	682.5	3155.	
20.33	1269.2	4114.1	10265.	
25.42	2457.5	13586.3	32999.	
30.50	3645.9	29099.1	80174.	
35.58	4834.2	50652.5	159080.	
40.67	6022.5	78246.5	276217.	

END FTABLE 12

FTABLE		13		
15	4			
DEPTH	AREA	VOLUME	DISCH	***
(FT)	(ACRES)	(AC-FT)	(CFS)	***
0.00	0.0	0.0	0.0	
1.35	13.8	17.3	50.0	
2.70	15.8	37.3	163.9	
4.05	17.9	60.0	333.2	
5.40	19.9	85.5	557.7	
6.75	21.9	113.7	838.8	
8.10	23.9	144.6	1179.	
10.80	28.0	214.7	2045.	
13.50	32.0	295.7	3179.	
16.20	36.1	387.7	4603.	
21.60	479.3	1779.2	10436.	
27.00	922.5	5564.1	23326.	
32.40	1365.7	11742.4	46807.	
37.80	1809.0	20314.2	83810.	
43.20	2252.2	31279.3	136949.	

END FTABLE 13

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FTABLE      14
15      4
  DEPTH      AREA      VOLUME      DISCH ***
  (FT)      (ACRES)    (AC-FT)    (CFS) ***
  0.00      0.0        0.0        0.0
  1.32      28.0       34.8       76.0
  2.64      31.5       74.1      247.0
  3.96      34.9      117.9      498.1
  5.28      38.3      166.2      827.0
  6.60      41.7      219.1     1234.
  7.92      45.2      276.5     1721.
 10.57      52.0      404.9     2947.
 13.21      58.9      551.4     4527.
 15.85      65.7      716.0     6486.
 21.13     891.3     3244.2    14395.
 26.42    1716.9    10134.2   31869.
 31.70    2542.5    21386.0   63733.
 36.98    3368.0    36999.5  113983.
 42.27    4193.6    56974.8  186187.
END FTABLE 14

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FTABLE      15
15      4
  DEPTH      AREA      VOLUME      DISCH ***
  (FT)      (ACRES)    (AC-FT)    (CFS) ***
  0.00      0.0        0.0        0.0
  0.88     229.4      176.5     107.8
  1.76     286.8      403.4     368.7
  2.64     344.1      680.7     780.9
  3.52     401.5     1008.5    1357.
  4.40     458.8     1386.6    2110.
  5.28     516.2     1815.2    3057.
  7.03     630.9     2823.7    5585.
  8.79     745.6     4033.9    9054.
 10.55     860.3     5445.7   13572.
 14.07    1206.1     9079.1   28863.
 17.58    1551.8    13928.4  50439.
 21.10    1897.6    19993.6  79279.
 24.62    2243.3    27274.7  116247.
 28.13    2589.1    35771.7  162147.
END FTABLE 15

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FTABLE      16
16      4
  DEPTH      AREA      VOLUME      DISCH ***
  (FT)      (ACRES)    (AC-FT)    (CFS) ***
  0.00      0.00       0.0        0.0
  0.01      1.49       0.1        0.0
  0.23      1.72       0.2        0.14
  0.73      2.34       0.82       0.41
  1.23      3.18       2.34       1.11
  1.73      4.33       4.63       3.05
  2.23      5.89       7.69       8.34
  2.73      8.01      11.5       22.8
  3.23     10.9      16.1       62.4

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3.73	14.8	21.5	170.6
4.23	20.1	27.7	466.6
4.73	27.4	34.6	1276.
5.23	37.2	42.3	3491.
5.73	50.6	50.7	9550.
6.23	68.9	60.0	26121.
6.73	93.7	70.0	71450.

END FTABLE 16

FTABLE 31

10 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
0.01	600.0	3.0	0.0	
1.00	612.4	603.2	0.0	
2.00	625.1	1221.9	0.0	
3.00	637.9	1853.5	0.0	
4.00	650.9	2497.8	0.0	
5.00	663.9	3155.2	0.0	
6.00	677.1	3825.7	0.0	
7.00	690.4	4509.5	446.6	
8.00	703.9	5206.7	901.9	

END FTABLE 31

FTABLE 41

10 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.00	0.0	0.0	0.0	
0.01	435.8	2.2	0.0	
1.00	446.4	438.8	0.0	
2.00	457.2	890.6	0.0	
3.00	468.2	1353.3	0.0	
4.00	479.2	1827.0	0.0	
5.00	490.5	2311.9	0.0	
6.00	501.8	2808.0	0.0	
7.00	513.3	3315.6	331.5	
8.00	524.9	3834.7	670.5	

END FTABLE 41

FTABLE 51

15 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.0	820.00	0.00	0.0	
0.5	830.00	412.50	0.0	
1.0	840.00	830.00	0.0	
1.5	850.00	1252.50	0.0	
2.0	860.00	1680.00	0.0	
2.5	870.14	2112.54	0.1	
3.0	880.28	2550.14	4.0	
3.5	890.42	2992.82	17.0	
4.0	900.57	3440.56	60.0	
4.5	910.60	3893.36	280.0	

5.0	920.60	4351.16	1000.0
5.5	930.60	4813.96	4500.0
6.0	940.60	5281.76	17000.0
6.5	950.60	5754.56	75000.0
7.0	960.60	6232.36	250000.0

END FTABLE 51

FTABLE 61

22 4

DEPTH (FT)	AREA (ACRES)	VOLUME (AC-FT)	DISCH (CFS)	*** ***
0.0	61.6	0.0	0.0	
0.2	104.67	16.63	1.00	
0.4	146.76	41.77	1.80	
1.0	272.92	167.68	6.90	
1.5	377.94	330.39	13.0	
2.0	482.87	545.60	21.0	
2.5	587.74	813.25	37.0	
3.0	692.54	1133.32	53.0	
3.5	797.29	1505.78	79.0	
4.0	902.00	1930.60	140.0	
4.5	1006.66	2407.76	220.0	
5.0	1111.19	2937.23	350.0	
5.5	1283.64	3535.94	725.0	
6.0	1456.06	4220.86	1100.0	
6.5	1628.46	4992.00	2000.0	
7.0	1800.83	5849.32	2600.0	
7.5	1973.18	6792.82	4800.0	
8.0	2145.52	7822.50	7000.0	
8.5	2317.83	8938.33	13000.0	
9.0	2490.13	10140.32	19000.0	
9.5	2662.41	11428.46	29500.0	
10.0	2834.68	12802.73	40000.0	

END FTABLE 61

END FTABLES

END RUN