UNITED STATES DEPARTMENT OF AGRICULTURE Rural Utilities Service

## BULLETIN 1726C-115

SUBJECT: Checking Sag in a Conductor by the Return Wave Method
TO: RUS Electric Borrowers and RUS Electric Staff
EFFECTIVE DATE: Date of Approval
EXPIRATION DATE: Indefinite
OFFICE OF PRIMARY INTEREST: Electric Staff Division
PREVIOUS INSTRUCTIONS: This revised bulletin replaces RUS Bulletin 1726C-115, "Checking Sag in a Conductor by the Return Wave Method," issued October 20, 1992.

FILING INSTRUCTIONS: Discard RUS Bulletin 1726C-115, dated October 20, 1992, and replace with this revised issue. This bulletin is available on the Internet via the RUS electric web site: www.usda.gov/rus/electric.

PURPOSE: This guide publication presents a convenient and practical method for checking sag in a conductor regardless of span length, tension, size or type of the conductor.
/s/ BDS, Jr.
09/24/98

Bulletin 1726C-115
Page 2

# TABLE OF CONTENTS 

1. Introduction ..... 3
2. Discussion ..... 3-4

## ABBREVIATIONS

RUS Rural Utilities Service

## INDEX:

CONDUCTORS:
Sag Checking by Return Wave Method

## 1. INTRODUCTION

1.1 This bulletin describes a convenient method for checking sag in a conductor. This method has been used extensively in checking sag in conductors on RUS borrowers' systems.

## 2. DISCUSSION

2.1 The return wave method of checking the sag in a conductor is applicable regardless of the span length, tension, size or type of conductor. The time required for a wave initiated on a conductor suspended in air between two fixed supports to traverse between the supports is dependent on the amount of conductor sag. A conductor wave originating at one support will travel to the next support where it will be reflected back to the point of origin where it will again be reflected back to the adjacent support and the cycle repeats. This cyclic action continues until the wave is eventually damped out.
2.2 The relationship between the time required for a conductor wave to travel a number of times between supports and the conductor's sag is given by the equation:

$$
\begin{equation*}
\mathrm{D}=48.3\left[\frac{\mathrm{~T}}{2 \mathrm{~N}}\right]^{2} \tag{1}
\end{equation*}
$$

Where:

$$
\begin{aligned}
& \mathrm{D}=\text { conductor sag in inches } \\
& \mathrm{T}=\text { time in seconds } \\
& \mathrm{N}=\text { number of return waves counted }
\end{aligned}
$$

The Time-Sag Table on pages 5 \& 6 was calculated from the above equation.

To convert from inches to millimeters use Formula (2) as given by the equation:

$$
\begin{equation*}
x=25.4 D \tag{2}
\end{equation*}
$$

Where:

$$
\begin{aligned}
& \mathrm{D}=\text { conductor sag in inches } \\
& \mathrm{X}=\text { conductor sag in millimeters }
\end{aligned}
$$

2.3 A wave may be initiated in a conductor close to a support by striking the conductor or by throwing a light, dry, nonmetallic
rope or cord over the conductor and pulling the conductor down strongly and quickly releasing the conductor (cord). The return wave arrival may be felt by placing a finger on the conductor if the striking method is used, or if a cord is used, the return wave arrival may be felt in the cord by maintaining light tension on the conductor.
2.4 For an accurate determination of sag, it is important that the correct number of return waves be selected on the Time-Sag Table. The table was prepared for sags corresponding to 3, 5, 10, and 15 return waves. The choice of the number of return waves depends principally upon the span length and size of conductor. For long spans and large conductors, the number of return waves that can be accurately counted is less than for short spans and small conductors. The largest number of return waves should be used consistent with the conditions encountered as this minimizes errors in recording time.
2.5 The wave initiating impulse is not counted as a return wave. A stop watch is started when the wave initiating impulse is applied and stopped immediately as the last of the number of return waves of 3,5 , 10 , or 15 as previously selected is received.

Satisfactory results cannot be obtained when the conductor is in motion as a result of other stimuli. Conductor movement, due to wind or craftspeople working on the line, makes it difficult to count the number of return waves. Additionally, satisfactory results cannot be obtained if any objects, such as tree branches, are in contact with the conductor in the span being checked.
2.6 A sufficient number of tests should be made in each span until at least three equal readings are obtained.

Example:
A wave is initiated on a conductor span and a time of 14.1 seconds is measured upon receipt of the $10^{\text {th }}$ return wave. From formula (1) or from the Time Sag Table, it can be seen that the conductor sag is 24 in . ( 610 mm ).

Bulletin 1726C-115

TIME SAG TABLE

| Sag <br> (Inches) | Return of Wave |  |  |  | Sag (Inches) | Return of Wave |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | 15th <br> Time <br> (Sec.) |  |  |  | 10th <br> Time (Sec.) | 15th <br> Time <br> (Sec.) |
| 5 | 1.9 | 3.2 | 6.4 | 9.7 | 55 | 6.4 | 10.7 | 21.3 | 32.0 |
| 6 | 2.1 | 3.5 | 7.0 | 10.6 | 56 | 6.5 | 10.8 | 21.5 | 32.3 |
| 7 | 2.3 | 3.8 | 7.6 | 11.4 | 57 | 6.5 | 10.9 | 21.7 | 32.6 |
| 8 | 2.4 | 4.1 | 8.1 | 12.2 | 58 | 6.6 | 11.0 | 21.9 | 32.9 |
| 9 | 2.6 | 4.3 | 8.6 | 13.0 | 59 | 6.6 | 11.1 | 22.1 | 33.2 |
| 10 | 2.7 | 4.6 | 9.1 | 13.7 | 60 | 6.7 | 11.1 | 22.3 | 33.4 |
| 11 | 2.9 | 4.8 | 9.5 | 14.3 | 61 | 6.7 | 11.2 | 22.5 | 33.7 |
| 12 | 3.0 | 5.0 | 10.0 | 15.0 | 62 | 6.8 | 11.3 | 22.7 | 34.0 |
| 13 | 3.1 | 5.2 | 10.4 | 15.6 | 63 | 6.9 | 11.4 | 22.8 | 34.3 |
| 14 | 3.2 | 5.4 | 10.8 | 16.2 | 64 | 6.9 | 11.5 | 23.0 | 34.5 |
| 15 | 3.3 | 5.6 | 11.1 | 16.7 | 65 | 7.0 | 11.6 | 23.2 | 34.8 |
| 16 | 3.5 | 5.8 | 11.5 | 17.3 | 66 | 7.0 | 11.7 | 23.4 | 35.1 |
| 17 | 3.6 | 5.9 | 11.9 | 17.8 | 67 | 7.1 | 11.8 | 23.6 | 35.3 |
| 18 | 3.7 | 6.1 | 12.2 | 18.3 | 68 | 7.1 | 11.9 | 23.7 | 35.6 |
| 19 | 3.8 | 6.3 | 12.5 | 18.8 | 69 | 7.2 | 12.0 | 23.9 | 35.9 |
| 20 | 3.9 | 6.4 | 12.9 | 19.3 | 70 | 7.2 | 12.0 | 24.1 | 36.1 |
| 21 | 4.0 | 6.6 | 13.2 | 19.8 | 71 | 7.3 | 12.1 | 24.2 | 36.4 |
| 22 | 4.0 | 6.7 | 13.5 | 20.2 | 72 | 7.3 | 12.2 | 24.4 | 36.6 |
| 23 | 4.1 | 6.9 | 13.8 | 20.7 | 73 | 7.4 | 12.3 | 24.6 | 36.9 |
| 24 | 4.2 | 7.0 | 14.1 | 21.1 | 74 | 7.4 | 12.4 | 24.8 | 37.1 |
| 25 | 4.3 | 7.2 | 14.4 | 21.6 | 75 | 7.5 | 12.5 | 24.9 | 37.4 |
| 26 | 4.4 | 7.3 | 14.7 | 22.0 | 76 | 7.5 | 12.5 | 25.1 | 37.6 |
| 27 | 4.5 | 7.5 | 15.0 | 22.4 | 77 | 7.6 | 12.6 | 25.3 | 37.9 |
| 28 | 4.6 | 7.6 | 15.2 | 22.8 | 78 | 7.6 | 12.7 | 25.4 | 38.1 |
| 29 | 4.6 | 7.7 | 15.5 | 23.2 | 79 | 7.7 | 12.8 | 25.6 | 38.4 |
| 30 | 4.7 | 7.9 | 15.8 | 23.6 | 80 | 7.7 | 12.9 | 25.7 | 38.6 |
| 31 | 4.8 | 8.0 | 16.0 | 24.0 | 81 | 7.8 | 13.0 | 25.9 | 38.9 |
| 32 | 4.9 | 8.1 | 16.3 | 24.4 | 82 | 7.8 | 13.0 | 26.1 | 39.1 |
| 33 | 5.0 | 8.3 | 16.5 | 24.8 | 83 | 7.9 | 13.1 | 26.2 | 39.3 |
| 34 | 5.0 | 8.4 | 16.8 | 25.2 | 84 | 7.9 | 13.2 | 26.4 | 39.6 |
| 35 | 5.1 | 8.5 | 17.0 | 25.5 | 85 | 8.0 | 13.3 | 26.5 | 39.8 |
| 36 | 5.2 | 8.6 | 17.3 | 25.9 | 86 | 8.0 | 13.3 | 26.7 | 40.0 |
| 37 | 5.3 | 8.8 | 17.5 | 26.3 | 87 | 8.1 | 13.4 | 26.8 | 40.3 |
| 38 | 5.3 | 8.9 | 17.7 | 26.6 | 88 | 8.1 | 13.5 | 27.0 | 40.5 |
| 39 | 5.4 | 9.0 | 18.0 | 27.0 | 89 | 8.1 | 13.6 | 27.1 | 40.7 |
| 40 | 5.5 | 9.1 | 18.2 | 27.3 | 90 | 8.2 | 13.7 | 27.3 | 41.0 |
| 41 | 5.5 | 9.2 | 18.4 | 27.6 | 91 | 8.2 | 13.7 | 27.5 | 41.2 |
| 42 | 5.6 | 9.3 | 18.7 | 28.0 | 92 | 8.3 | 13.8 | 27.6 | 41.4 |
| 43 | 5.7 | 9.4 | 18.9 | 28.3 | 93 | 8.3 | 13.9 | 27.8 | 41.6 |
| 44 | 5.7 | 9.5 | 19.1 | 28.6 | 94 | 8.4 | 14.0 | 27.9 | 41.9 |
| 45 | 5.8 | 9.7 | 19.3 | 29.0 | 95 | 8.4 | 14.0 | 28.0 | 42.1 |
| 46 | 5.9 | 9.8 | 19.5 | 29.3 | 96 | 8.5 | 14.1 | 28.2 | 42.3 |
| 47 | 5.9 | 9.9 | 19.7 | 29.6 | 97 | 8.5 | 14.2 | 28.3 | 42.5 |
| 48 | 6.0 | 10.0 | 19.9 | 29.9 | 98 | 8.5 | 14.2 | 28.5 | 42.7 |
| 49 | 6.0 | 10.1 | 20.1 | 30.2 | 99 | 8.6 | 14.3 | 28.6 | 43.0 |
| 50 | 6.1 | 10.2 | 20.3 | 30.5 | 100 | 8.6 | 14.4 | 28.8 | 43.2 |
| 51 | 6.2 | 10.3 | 20.6 | 30.8 | 101 | 8.7 | 14.5 | 28.9 | 43.4 |
| 52 | 6.2 | 10.4 | 20.8 | 31.1 | 102 | 8.7 | 14.5 | 29.1 | 43.6 |
| 53 | 6.3 | 10.5 | 21.0 | 31.4 | 103 | 8.8 | 14.6 | 29.2 | 43.8 |
| 54 | 6.3 | 10.6 | 21.1 | 31.7 | 104 | 8.8 | 14.7 | 29.3 | 44.0 |

# Bulletin 1726C-115 <br> Page 7 

TIME SAG TABLE (con't.)

| Sag (Inches) | Return of Wave |  |  |  | Sag (Inches) | Return of Wave |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 3rd <br> Time (Sec.) | $\begin{gathered} \text { 5th } \\ \text { Time } \\ \text { (Sec.) } \\ \hline \end{gathered}$ | 10th <br> Time <br> (Sec.) | 15th <br> Time (Sec.) |  |  |  | $10 \mathrm{th}$ <br> Time (Sec.) | 15th <br> Time (Sec.) |
| 105 | 8.8 | 14.7 | 29.5 | 44.2 | 155 | 10.7 | 17.9 | 35.8 | 53.7 |
| 106 | 8.9 | 14.8 | 29.6 | 44.4 | 156 | 10.8 | 18.0 | 35.9 | 53.9 |
| 107 | 8.9 | 14.9 | 29.8 | 44.7 | 157 | 10.8 | 18.0 | 36.1 | 54.1 |
| 108 | 9.0 | 15.0 | 29.9 | 44.9 | 158 | 10.9 | 18.1 | 36.2 | 54.3 |
| 109 | 9.0 | 15.0 | 30.0 | 45.1 | 159 | 10.9 | 18.1 | 36.3 | 54.4 |
| 110 | 9.1 | 15.1 | 30.2 | 45.3 | 160 | 10.9 | 18.2 | 36.4 | 54.6 |
| 111 | 9.1 | 15.2 | 30.3 | 45.5 | 161 | 11.0 | 18.3 | 36.5 | 54.8 |
| 112 | 9.1 | 15.2 | 30.5 | 45.7 | 162 | 11.0 | 18.3 | 36.6 | 54.9 |
| 113 | 9.2 | 15.3 | 30.6 | 45.9 | 163 | 11.0 | 18.4 | 36.7 | 55.1 |
| 114 | 9.2 | 15.4 | 30.7 | 46.1 | 164 | 11.1 | 18.4 | 36.9 | 55.3 |
| 115 | 9.3 | 15.4 | 30.9 | 46.3 | 165 | 11.1 | 18.5 | 37.0 | 55.4 |
| 116 | 9.3 | 15.5 | 31.0 | 46.5 | 166 | 11.1 | 18.5 | 37.1 | 55.6 |
| 117 | 9.3 | 15.6 | 31.1 | 46.7 | 167 | 11.2 | 18.6 | 37.2 | 55.8 |
| 118 | 9.4 | 15.6 | 31.3 | 46.9 | 168 | 11.2 | 18.7 | 37.3 | 56.0 |
| 119 | 9.4 | 15.7 | 31.4 | 47.1 | 169 | 11.2 | 18.7 | 37.4 | 56.1 |
| 120 | 9.5 | 15.8 | 31.5 | 47.3 | 170 | 11.3 | 18.8 | 37.5 | 56.3 |
| 121 | 9.5 | 15.8 | 31.7 | 47.5 | 171 | 11.3 | 18.8 | 37.6 | 56.4 |
| 122 | 9.5 | 15.9 | 31.8 | 47.7 | 172 | 11.3 | 18.9 | 37.7 | 56.6 |
| 123 | 9.6 | 16.0 | 31.9 | 47.9 | 173 | 11.4 | 18.9 | 37.9 | 56.8 |
| 124 | 9.6 | 16.0 | 32.0 | 48.1 | 174 | 11.4 | 19.0 | 38.0 | 56.9 |
| 125 | 9.7 | 16.1 | 32.2 | 48.3 | 175 | 11.4 | 19.0 | 38.1 | 57.1 |
| 126 | 9.7 | 16.2 | 32.3 | 48.5 | 176 | 11.5 | 19.1 | 38.2 | 57.3 |
| 127 | 9.7 | 16.2 | 32.4 | 48.6 | 177 | 11.5 | 19.1 | 38.3 | 57.4 |
| 128 | 9.8 | 16.3 | 32.6 | 48.8 | 178 | 11.5 | 19.2 | 38.4 | 57.6 |
| 129 | 9.8 | 16.3 | 32.7 | 49.0 | 179 | 11.6 | 19.3 | 38.5 | 57.8 |
| 130 | 9.8 | 16.4 | 32.8 | 49.2 | 180 | 11.6 | 19.3 | 38.6 | 57.9 |
| 131 | 9.9 | 16.5 | 32.9 | 49.4 | 181 | 11.6 | 19.4 | 38.7 | 58.1 |
| 132 | 9.9 | 16.5 | 33.1 | 49.6 | 182 | 11.6 | 19.4 | 38.8 | 58.2 |
| 133 | 10.0 | 16.6 | 33.2 | 49.8 | 183 | 11.7 | 19.5 | 38.9 | 58.4 |
| 134 | 10.0 | 16.7 | 33.3 | 50.0 | 184 | 11.7 | 19.5 | 39.0 | 58.6 |
| 135 | 10.0 | 16.7 | 33.4 | 50.2 | 185 | 11.7 | 19.6 | 39.1 | 58.7 |
| 136 | 10.1 | 16.8 | 33.6 | 50.3 | 186 | 11.8 | 19.6 | 39.2 | 58.9 |
| 137 | 10.1 | 16.8 | 33.7 | 50.5 | 187 | 11.8 | 19.7 | 39.4 | 59.0 |
| 138 | 10.1 | 16.9 | 33.8 | 50.7 | 188 | 11.8 | 19.7 | 39.5 | 59.2 |
| 139 | 10.2 | 17.0 | 33.9 | 50.9 | 189 | 11.9 | 19.8 | 39.6 | 59.3 |
| 140 | 10.2 | 17.0 | 34.1 | 51.1 | 190 | 11.9 | 19.8 | 39.7 | 59.5 |
| 141 | 10.3 | 17.1 | 34.2 | 51.3 | 191 | 11.9 | 19.9 | 39.8 | 59.7 |
| 142 | 10.3 | 17.1 | 34.3 | 51.4 | 192 | 12.0 | 19.9 | 39.9 | 59.8 |
| 143 | 10.3 | 17.2 | 34.4 | 51.6 | 193 | 12.0 | 20.0 | 40.0 | 60.0 |
| 144 | 10.4 | 17.3 | 34.5 | 51.8 | 194 | 12.0 | 20.0 | 40.1 | 60.1 |
| 145 | 10.4 | 17.3 | 34.7 | 52.0 | 195 | 12.1 | 20.1 | 40.2 | 60.3 |
| 146 | 10.4 | 17.4 | 34.8 | 52.2 | 196 | 12.1 | 20.1 | 40.3 | 60.4 |
| 147 | 10.5 | 17.4 | 34.9 | 52.3 | 197 | 12.1 | 20.2 | 40.4 | 60.6 |
| 148 | 10.5 | 17.5 | 35.0 | 52.5 | 198 | 12.1 | 20.2 | 40.5 | 60.7 |
| 149 | 10.5 | 17.6 | 35.1 | 52.7 | 199 | 12.2 | 20.3 | 40.6 | 60.9 |
| 150 | 10.6 | 17.6 | 35.2 | 52.9 | 200 | 12.2 | 20.3 | 40.7 | 61.0 |
| 151 | 10.6 | 17.7 | 35.4 | 53.0 | 201 | 12.2 | 20.4 | 40.8 | 61.2 |
| 152 | 10.6 | 17.7 | 35.5 | 53.2 | 202 | 12.3 | 20.5 | 40.9 | 61.4 |
| 153 | 10.7 | 17.8 | 35.6 | 53.4 | 203 | 12.3 | 20.5 | 41.0 | 61.5 |
| 154 | 10.7 | 17.9 | 35.7 | 53.6 | 204 | 12.3 | 20.6 | 41.1 | 61.7 |

