United States Department of Agriculture Grain Inspection, Packers and Stockyards Administration Federal Grain Inspection Service
Directive

## FALLING NUMBER DETERMINATION FOR WHEAT

## 1. PURPOSE

This directive transmits procedures for determining and certificating falling number (FN) results for wheat only. The service is provided upon request under the authority of the Agricultural Marketing Act of 1946, as amended (AMA). Testing services are available at selected Federal Grain Inspection Service (FGIS) field offices, State agencies, and the Analytical, Reference, and Testing Services (ARTS) in Kansas City, Missouri.

## 2. REPLACEMENT HIGHLIGHTS

This directive supersedes FGIS Program Directive 918.38, Falling Number Determination, dated 9-17-93. This directive is updated to reflect organizational changes, new numbering system, and new format but does not revise policy.

## 3. BACKGROUND

Shortly before sprouting can be seen, there is a dramatic increase in the alpha-amylase enzyme activity of wheat kernels. Millers and bakers are very concerned about the level of alpha-amylase activity in wheat flour because excessive amounts break down starches to the extent that the flour's baking properties are adversely affected.

The FN determination indirectly measures alpha-amylase activity in a manner that simulates some of the changes flour undergoes during baking. Specifically, the "falling number" is the number of seconds required to stir and allow the stirrer to fall a measured distance through a hot aqueous flour gel undergoing liquefaction. A high falling number indicates low alpha-amylase activity or a viscous, gelled flour/water slurry. A low falling number indicates high alpha-amylase activity or a less viscous, thin flour/water slurry.

The FN test is especially sensitive to small differences between the boiling points of the water bath and sample slurry. The test procedure outlined in this directive includes specific precautions and a trouble-shooting section for ensuring that boiling points of the bath and the sample slurry are as nearly equal as possible.

For purposes of this directive, wheat prepared for the FN test by the prescribed grinding method is referred to as "flour." The AACC method for "wheat flour" (meaning milled wheat flour) differs slightly from the method described in this directive.

## 4. EQUIPMENT AND SUPPLIES

FN apparatuses are manually, semiautomatically, or automatically operated, depending on the model used. Some models perform one determination at a time; others perform two tests simultaneously. The FN apparatus can be obtained from: a) Perten Instruments North America, Inc., P.O. Box 7398, Reno, NV 89510-7398 or b) Perten Instruments AB, P.O. Box 5101, S-141 05 Huddinge Sweden. 1/

In addition to the FN apparatus itself, the following equipment and supplies are required.
a. Glass Tubes and Stoppers. The glass viscometer tubes are designed specifically for use with the FN apparatus and are manufactured to close tolerances (inner diameter, $21.00 \pm 0.02 \mathrm{~mm}$, outer diameter, $23.8 \pm 0.3 \mathrm{~mm}$, length $220.0 \pm 0.3$ mm ). The Board of Appeals and Review (BAR) must verify that all tubes used in official inspections are within tolerances.

Therefore, the BAR shall maintain an inventory of viscometer tubes for each field office that is active in the FN program. The BAR shall order the tubes, check them in advance, and ship them on request to each office. Tube requisitions shall be charged to management codes obtained from Field Management Division (FMD). FGIS field office managers shall assure that agencies use only approved visometer tubes.
b. Barometer. Barometers are used for checking the operating conditions of the FN bath. Use an aneroid barometer that is readable (with interpolation) to 0.5 mm per ft . ( 0.02 in per ft . or 0.07 kPa per meter) Hg pressure. Calibrate the barometer to agree with the "station pressure" of the nearest weather station. Observe the following precautions:

1/ The mention of firm names or trade products does not imply that they are endorsed or recommended by the U.S. Department of Agriculture over other firms or similar products not mentioned.
(1) Specifically ask for the "station pressure", or the "true barometric pressure." For weather forecasting, metrologists apply a correction to barometer readings to make them appear as if they were all taken at sea level.

Such "sea-level-corrected" readings are given by the media in the local weather report, and they may also be given by the National Weather Service over the phone. Use only the "station pressure" or the "true barometric pressure" to calibrate the laboratory barometer.
(2) If the laboratory altitude differs significantly from that of the weather station, the laboratory barometric pressure will also differ from the station pressure.

Atmospheric pressure drops approximately 0.027 mm Hg per ft. ( 0.012 kPa per meter or $0.001 \mathrm{in} . \mathrm{Hg}$ per ft .) of rise in elevation. Thus, if the laboratory is at a lower elevation than the weather station, the correction will be positive and if the laboratory is at a higher elevation, the correction will be negative. Apply the appropriate correction to the station pressure given by the weather station before calibrating the laboratory barometer. The maximum allowable difference between the altitudes of laboratory and weather station is $\pm 1,000$ feet.

Example: $\quad$ The pressure at the nearest weather station is $29.60 \mathrm{in} . \mathrm{Hg}$ ( 751.8 mm Hg or 100.2 kPa ), the weather station is at 550 ft . (168 meters) elevation, and the laboratory is at 700 ft . (213 meters) elevation.

Correction $=($ Station Elev. - Lab. Elev. $) \times 0.001$

## Calculation:

$$
\begin{aligned}
\text { Correction } & =(550 \mathrm{ft} .-700 \mathrm{ft} .) \times .001 \mathrm{in} . \mathrm{Hg} / \mathrm{ft} . \\
& =-150 \times 0.001=-0.15 \mathrm{in} . \mathrm{Hg} .
\end{aligned}
$$

The correction is negative and is subtracted from the weather station pressure. The true barometric pressure in this example is 29.60 in. $\mathrm{Hg}-0.15 \mathrm{in} . \mathrm{Hg}=29.45 \mathrm{in} . \mathrm{Hg}(748 \mathrm{~mm} \mathrm{Hg}$ or 99.73 kPa ) and is the reading used to calibrate the laboratory barometer.
(3) After each barometer adjustment, check the barometer again within a week, and after that, check the barometer once per month. If at any time the barometer deviates from the correct reading by more than $\pm 0.10 \mathrm{in}$. $( \pm 2.5 \mathrm{~mm}$ or $\pm 0.34 \mathrm{kPa}) \mathrm{Hg}$, adjust as needed and check it again within a week. Avoid calibrating or changing the barometer on days when the barometric pressure or the temperature is changing rapidly. Record the station pressure and the laboratory barometer readings in a permanent record.
c. Viscometer-stirrer. (supplied with the FN apparatus).
d. Thermometer. For checking the water bath temperature, use a thermometer (mercury of electronic type) which is marked in $0.2^{\circ} \mathrm{C}$, or smaller, divisions and is accurate to $\pm 0.3^{\circ} \mathrm{C}$.
e. Grinder. Falling Number Mill, model 3100, with a 0.8 mm screen. Replace the screen every 1,000 samples and whenever it appears damaged.
f. Balance. A precision-class balance with a specified accuracy of $\pm 0.02$ grams or better.
g. Water Dispenser. Graduated cylinder, 25.0 mL capacity, or an automatic pipet that delivers $25.0 \mathrm{~mL}( \pm 0.3 \mathrm{~mL})$. Once each week, check the accuracy of the cylinder or the automatic pipet by weighing (with the precision balance) the amount of distilled water dispensed. If the weight of the dispensed distilled water is outside the range of $25.0 \pm 0.3$ grams, replace or re-calibrate the dispenser.

Operator may use the precision balance to routinely weigh $25.0 \pm 0.3$ grams of distilled water into a beaker. To dispense the distilled water, pour it into the viscometer tube.
h. Distilled Water.
i. Test Tube Brush or Spolett Rapid Cleaner.
j. Powder Funnel.

## 5. BASIS OF DETERMINATION

The FN test is based on a 7-gram representative portion taken from 250 grams of flour which has been ground from the whole wheat sample. Sufficient wheat must be ground to yield 250 grams of flour. Remove dockage and stones from the sample before grinding. See section 6, b for more details.

FN results are reported on a 14 percent moisture basis unless the applicant specifies another moisture basis. The applicant may request to have the FN results reported on the "AS IS" moisture basis, the dry matter ( 0 percent moisture) basis, or any other specified moisture basis. Only one moisture basis is reported on any one certificate.

There are three certification options for export lots: a) composite sample representing the entire lot, b) individual sublot samples, or c) an average of sublots using the approved method (see section 7 for more details). Applicants must request the certification option prior to loading.

Perform all FN determinations in duplicate and report, on the official certificate, the average of the duplicate test results.

## 6. PROCEDURE

a. The Water Bath Temperature Verification. The FN apparatus water bath requires distilled water or deionized water. The FN value is affected by the boiling temperature of the water bath, which is a function of water purity and the atmospheric pressure. Elevated locations may obtain higher FN values than those determined at sea level. Therefore, altitude corrections are applied at locations having elevations at or above $2,000 \mathrm{ft}$. ( 610 meters).

Periodically check the water bath level while running FN tests. The FN apparatus includes an overflow tube on the water bath. The water level should be at the overflow level when viscometer tubes are in place. The water level is slightly below the overflow outlet after running the first set of tubes. Immediately after a FN test in which the water level was at the overflow outlet, mark the new water level on the water level indicator. Maintain the water height at the mark, so that when a set of FN tubes is inserted, the water will rise to the overflow outlet.

Before the initial test of each day and/or after adding distilled water to the bath, verify that the bath temperature is correct for the true barometric pressure measured in the laboratory (see attachment 4, table 4). If the bath temperature deviates from the predicted temperature (table 4) by more than $\pm 0.4^{\circ} \mathrm{C}$, correct the problem before proceeding. (Refer to the section on troubleshooting for help in diagnosis).

## DO NOT ADD CHEMICALS TO ADJUST THE WATER BATH TEMPERATURE AS THIS WILL LEAD TO ERRONEOUS RESULTS.

b. Moisture Determination and Sample Preparation of Whole Wheat. Determine the moisture content of the whole grain using the Motomco 919 moisture meter (refer to the Grain Inspection Handbook, book II, section 1.10, for more details).

If the whole grain moisture is above 15.9 percent, air dry the sample (on an open pan at room temperature) to a moisture content of 15.9 percent or less before grinding, unless results are reported on an "as is" basis.. Air drying to 15.9 percent moisture is not required for "as is" certification. Air dry enough grain so that the weight after drying is at least 250 grams (see attachment 3). Table 3 gives the predicted moisture content of the flour for whole grain moistures up to 15.9 percent.

A small number of sprouted kernels can affect the FN result significantly. To minimize sampling error, grind 250 grams of wheat (after removing dockage and stones). Place the ground sample in a clean container and cover it securely. Roll the container several times, then stir the sample with a spatula to blend it further. Run the grinder for 1 minute after each sample to allow the grinder to cool and to purge residual sample from the chamber to avoid contaminating samples. Clean the collection vessel after each sample. Clean the grinder daily and whenever sample build-up is observed.
c. FN Determination. Perform all FN determinations in duplicate as follows:
(l) Weigh 7.00 grams ( $\pm 0.05$ grams) of the blended ground sample into a clean, dry viscometer tube.
(2) Add $25.0 \mathrm{~mL}( \pm 0.3 \mathrm{~mL})$ distilled water (temperature $22^{\circ} \mathrm{C} \pm 2^{\circ} \mathrm{C}$ ). (If preferred, the water may be dispensed before the flour.)

## NOTE: As soon as possible, after dispensing the sample and water, proceed with steps (3), (4), and (5) below.

(3) Insert the rubber stopper. Holding the tube securely in upright position with the thumb over the stopper, shake the tube up and down 20 times. Make certain all the sample is suspended by upending the tube. If mixing is incomplete, repeat steps 6.c.(1) through 6.c.(3), above, and use a more brisk shaking action.
(4) Remove the stopper. Scrape the slurry coating from the stopper into the tube, then use the viscometer-stirrer to scrape down the slurry from the upper part of the tube. Thorough scraping of the stopper and tube is important.
(5) Place the tube and the viscometer-stirrer into the water bath tube holder within 40 seconds after the start of mixing. Start the timer immediately.
(a) When using the automatic apparatus, the stirring and settling cycle will begin automatically.
(b) When using the semiautomatic apparatus, swing the stirring motor unit into place over the top of the tube. When the timer registers exactly 5 seconds, push the lever on the motor unit to begin the stirring cycle. When the timer registers exactly 60 seconds, stop the stirring cycle with the viscometer-stirrer in its uppermost position. Swing the tripwire into place. When the test is completed, the timer will stop and a buzzer will sound.
(c) When using the manually-operated apparatus, begin stirring the sample exactly 5 seconds after placing the tube into the bath. Stir at the rate of exactly two strokes per second. Down and up is one stroke. After 110 strokes, 60 seconds will have elapsed. Stop stirring with the viscometer-stirrer up, then swing the tripwire into place. Note the position of the viscometer-stirrer closely; when it reaches the tripwire, stop the timer.
(6) At the conclusion of the test, record the time in seconds.

There is very little alpha-amylase activity in samples with a FN result above 400. Thus, when the FN results exceed 400 , record the results on the certificate as "more than 400." If an applicant requested the actual FN results or the actual result is needed for sublot analysis, allow the test to continue until completion.
(7) Hold the test tube under running water and remove the stirrer. Clean the stirrer and test tube thoroughly, making certain that all gelled material is removed from inside the black, ebonite neck of the viscometer-stirrer.
(8) If the FN apparatus holds two viscometer tubes, perform duplicate tests at the same time. If the FN apparatus holds one visometer tube, repeat the test using a second 7 -gram portion from the 250 -gram sample. Some variation between duplicate tests is expected. If duplicate results differ by more than $\pm 5$ percent from the average of the two tests, test a new duplicate set of sample portions. If both results are greater than 400 , do not check the repeatability.

Determine the allowable deviation by multiplying the average result by 0.05 .

Example: If the test results are 350 and 370 , calculate the allowable deviation and the acceptable range as follows:

Average FN readings $=(350+370) \div 2=360$
Allowable deviation $=360 \times 0.05= \pm 18$ from 360
Acceptable FN readings must fall between 378 and 342.
(9) Record the duplicate test results and their average.
d. Altitude Correction for Wheat Sample After Grinding in the FN Model 3100 Mill.
(1) If the laboratory altitude is lower than $2,000 \mathrm{ft}$. ( 610 meters), FN readings are reported without corrections.
(2) If the laboratory altitude is $2,000 \mathrm{ft}$. ( 610 meters) or higher, correct the FN reading as shown in table 1 (see attachment 1). For example, if the laboratory altitude is $3,000 \mathrm{ft}$. ( 914 meters) and the average FN reading is 325, the corrected FN is 283 (from table 1). For intermediate elevations and FN readings not listed in table 1, interpolate the results.
e. Moisture Correction. $\underline{1 /}$ Using the Motomco 919 moisture result (see section 6, b), estimate the moisture content of the ground sample from attachment 3 , table 3 , unless certification is requested on "AS IS" basis.

Record only one moisture basis on any one certificate.

[^0]Determine the moisture-corrected falling number for any specified moisture basis, other than "AS IS," using the following formula. For "AS IS" moisture basis, report FN reading without correction.

FN $($ specified $m b)=\underline{\text { Average FN }(\text { step d above }) \times(100-\mathrm{M})}$
$(100-\mathrm{P})$
Where M is a specified moisture basis and P is the predicted moisture of the flour from table 3 based on the Motomco percent moisture.

Example: Motomco percent moisture is 12.7, predicted moisture (P) from table 3 is 12.3 , and average FN result is 355.5 (AS IS). The moisture-corrected FN is calculated as follows:
a. For dry matter basis ( 0 percent moisture basis):

$$
\begin{aligned}
\mathrm{FN} & =(355.5 \times(100-0) \div(100-12.3) \\
& =(355.5 \times 100) \div 87.7=405.4=405
\end{aligned}
$$

b. For applicant specified moisture basis (example 12\% moisture basis):

$$
\begin{aligned}
\mathrm{FN} & =(355.5 \times(100-12)) \div(100-12.3) \\
& =(355.5 \times 88) \div 87.7=356.7=357
\end{aligned}
$$

c. For $14 \%$ moisture basis:

$$
\begin{aligned}
\mathrm{FN} & =(355.5 \times(100-14) \div(100-12.3) \\
& =(355.5 \times 86) \div 87.7=348.6=349
\end{aligned}
$$

## NOTE: The moisture-corrected FN result is rounded to the nearest whole number for certification.

## 7. AVERAGING SUBLOT RESULTS

A special formula is used to average the sublot results because FN values do not have additive properties. For example, with the formula, samples with FN values of 380 and 70 yield an average FN of 88. Low FN results have a pronounced affect in lowering the average FN result when combined with a sample having a high FN reading.

The FN result is calculated as follows:
STEP 1: Convert each sublot FN reading to its Liquefaction Number (LN) equivalent. Use attachment 2, table 2, or, for readings outside the range of table 2, use the following formula:

$$
\mathrm{LN}=6,000 \div(\mathrm{FN}-50)
$$

STEP 2: Average the sublot LN values.
STEP 3: Convert the average LN value to its FN equivalent. Use table 2 or, for readings not listed or outside the range of table 2 , use the following formula:

$$
\mathrm{FN}=(6,000 \div \text { Average } \mathrm{LN})+50
$$

## Example:

STEP 1: Record FN values, LN equivalents, and calculate total LN.

| S/L NO | FN | LN | S/L NO | FN | LN |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 300 | 24.0 | 7 | 325 | 21.8 |
| 2 | 375 | 18.5 | 8 | 250 | 30.0 |
| 3 | 100 | 120.0 | 9 | 350 | 20.0 |
| 4 | 200 | 40.0 | 10 | 275 | 26.7 |
| 5 | 225 | 34.3 | 11 | 325 | 21.8 |
| 6 | 400 | 17.1 | 12 | 500 | 13.3 |

Total LN $=387.5$
STEP 2: Average the LN values.
LN average $=387.5 \quad 12=32.29$
LN after rounding $=32.3$
STEP 3: $\mathrm{FN}=(6,000 \div 32.3)+50$
$=185.76+50$
$=235.76$
FN average after rounding $=236$

## 8. CERTIFICATION

Report FN results on the inspection certificate (lot or sample) in accordance with chapter 6 of the Processed Commodities Handbook.

On the certificate, describe the commodity as "Wheat." Under "Results of Inspection," report the FN result with the applicable statement below. FN results are reported for certification to the nearest whole number.
"Falling number: $\qquad$ , $\qquad$ percent moisture basis." (Use this statement to report FN results on any specified moisture basis.)
"Falling number: $\qquad$ , dry matter basis."
"Falling number: $\qquad$ , as is moisture basis."

Divided-original certificates are available upon request of the applicant.

## 9. RETEST AND APPEAL

A retest and/or appeal inspection is available upon request by the applicant. A retest is performed on the basis of the whole grain file sample, and an appeal is performed on the basis of the whole grain file sample or a new sample (AMA Part 868.33 and 868.35).
a. A retest inspection may be performed by the same office that performed the original inspection.
b. Appeal inspections may be performed by the BAR, the FGIS field office or Federal/State office that monitored the office that performed the original inspection or retest, or ARTS when requested by the applicant.

Official personnel must not perform a retest or appeal inspection if they participated in a previous inspection unless there is only one authorized person available at the time and place of the requested service. Also, whenever possible, the retest or appeal inspection should be performed on a different FN apparatus than the one used for the original inspection.

The applicant may also request a retest and appeal inspection of individual sublots without separate certification. That is, a single certificate for a shiplot may use original, retest, and appeal results for different sublots for the final certification.

The retest or appeal inspection is performed according to the procedures specified in this directive for original FN determinations.

## 10. QUALITY CONTROL

The BAR is responsible for the quality control of official FN tests performed at all service points. To accomplish this, the BAR will prepare check samples for service points every 3 months (quarterly). The check sample set will include a minimum of three wheat samples having FN levels ranging from approximately 200 to 350 . One or more of the_samples will be whole grain; the remainder will be meal or flour. Check sample sets will include instructions for completing the quarterly check.

The BAR will establish tolerances and action limits based on historical data and will provide statistical analysis and plots of results to field locations.

The BAR may distribute additional check samples periodically and may request monitoring samples from selected locations.

## 11. TROUBLE-SHOOTING

The following list of symptoms and possible causes is given as a help for diagnosing and correcting errors in the FN test. The list is not all-inclusive, but serves as an aid in conducting the local quality control program.
a. Discrepancy Between Bath Temperature and Barometric Pressure. Possible causes and solutions:
(1) Bath not yet up to temperature. The Model 1800 may switch to the ready mode before a full boil is reached. Wait for a rolling boil before reading the temperature.
(2) Heater malfunction. Interruption of heating may be caused by a burnt-out fuse or heater element. The Model 1800 does not give a "bath cold" error message until the temperature has fallen to about $90^{\circ} \mathrm{C}$.
(3) Thermometer too close to heater coil. Local superheating near the heater coil may raise the thermometer reading by as much as two degrees. The thermometer should be perpendicular and immersed in water up to the immersion line.
(4) Impure bath water. Impurities may change the boiling temperature of the bath water. Use only distilled or deionized water in the bath. Do not add chemicals to the bath water. Routinely replace the bath water at least once a week.
(5) Barometer inaccuracy. Verify the barometer calibration as described in section 4.b.
(6) Thermometer inaccuracy. A precision thermometer becomes inaccurate when a separation or a gas bubble exists in the mercury column. Follow the manufacturer's instructions for removing separations/bubbles.
(7) Thermometer calibration error. Thermometer accuracy can be altered by exposure to extreme temperatures, e.g., heating it in a flame to remove column mercury separations, or by exposure to high temperature for long periods of time. If you doubt the reading of the thermometer, check it against a second thermometer that is known to be correct within $\pm 0.2^{\circ} \mathrm{C}$ by comparing the readings of the two in the boiling water bath.
b. Sources of Error in the FN Test. Possible causes and solutions.
(1) Error in measuring bath temperature and/or barometric pressure. The daily temperature-pressure check serves as a test for hidden errors. For a typical sample with FN of 300 , a forced increase of $0.2^{\circ} \mathrm{C}$ will decrease the FN test result by about 20 seconds. If measured temperature differs from predicted temperature (table 4 ) by more than $\pm 0.4^{\circ} \mathrm{C}$, refer to section 11. a., above.
(2) Incomplete mixing of samples. Samples for FN analysis must be mixed until uniform throughout. (See section 6. b.).
(3) Balance error. For a typical sample with FN of 300, an increase of 0.05 grams will increase the FN test result by about 5 seconds. Check the balance using standard weights totaling 7.00 grams. A balance error exceeding $\pm 0.02$ grams indicates that balance service or repair is needed.
(4) Water dispenser error. For a typical sample with FN of 300, an increase of 1 mL will decrease the FN test result by about 5 seconds. Check the dispenser accuracy as described in section 4. g. Liquid dispensers,
although convenient, have hidden sources of error. For example, raising the plunger too rapidly may cause a short burst of liquid to eject from the tip when the adjustable stop is contacted. Furthermore, expelling the syringe too rapidly often causes liquid to briefly continue flowing from the tip after the syringe is emptied. Fill and empty the dispenser only at rates which accurately and reproducibly dispense the 25.0 mL of water.
(5) Incorrect temperature of sample water. For a typical sample with FN of 300, an increase in sample water temperature of $1^{\circ} \mathrm{C}$ will decrease the FN test result by about 2 seconds. Determine the temperature of the sample water. If needed, place the dispenser reservoir in a cool or warm bath to bring it to $20-24^{\circ} \mathrm{C}$.
(6) Impure sample dilution water. The use of tap water, rather than distilled/deionized water, for mixing with the ground sample usually has a small, but measurable, effect on the FN result. Use only distilled or deionized water as the sample water.
(7) Failure to scrape. Failure to scrape the slurry residue from the stopper into the tube and from the tube walls down into the slurry will decrease the FN test result.
(8) Improper timing. Exceeding the 40 -second time limit for scraping the stopper, scraping the tube walls, inserting the tubes, and starting the timer will affect the FN test result.
(9) Improper mixing. Failure to hold the tube vertically while mixing the slurry may affect the test result.
(10) Incomplete mixing. Check for incomplete mixing by momentarily inverting the tube. If lumps or pockets of thick slurry are seen, a more brisk mixing action is needed. Repeat the test rather than continuing shaking.
(11) Incorrect bath level. Check the bath level between analyses to assure that it does not fall below the mark (section 6. a.). Adjust the bath level by adding distilled water to the bath, then wait until a full boil is restored before checking temperature and running the next test.
(12) Error in moisture correction. An error of 1 percent in the moisture reading will cause an error of approximately 1 percent in the FN result, after correction to 14 percent moisture basis.
(13) Erosion of grinder screen. Stones in FN samples can quickly erode or damage the grinder screen, thus permitting particles larger than 0.8 mm to exit the grinding chamber. A coarse grind will decrease the FN test result. If in doubt about the condition of the screen replace it with a new 0.8 mm screen.
(14) Incorrect stirrer weight. The manufacturer's specification for the stirrer weight-plunger assembly (without plastic collar) is $25.00 \pm 0.05 \mathrm{~g}$.
(15) Out-of-tolerance viscosity tubes. For tube specifications, refer to section 4. a.
(16) Operator differences. Non-agreement between operators has often been traced to different mixing actions and/or timing of procedural steps.
c. Consistent small difference between sides of the Model 1800.
(1) Differences in treatment of duplicate tests. The timing of each step in the test procedure, especially mixing, scraping, inserting the tubes, and starting the timer, should be as nearly identical as possible. Also, the mixing action applied to each tube should be as identical as possible.
(2) Asymmetry of heater shape has been reported to cause different results between the left and right sides. The orientation of the heater element is adjustable, within limits, by turning the bath vessel on its base. One field location reported that the left and right sides were brought into agreement by this method. Matching index marks were then made on the edges of the vessel and lid. Test results of the two sides were kept in agreement by aligning the two marks each time the bath was assembled.
(3) Hot spot on heater element.

## /s/David Orr

David Orr, Acting Director<br>Field Management Division

Attachments

Attachment 1
FGIS PROGRAM DIRECTIVE 9180.38
5-1-97
TABLE 1
ALTITUDE-CORRECTED FN VALUES FOR WHEAT AT DIFFERENT LABORATORY ALTITUDES (FT. ABOVE SEA LEVEL)

| FALLING NUMBER | ALTITUDE (FT. ABOVE SEA LEVEL) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TEST RESULTS | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 |
| 100 | 84 | 81 | 80 | 78 | 77 | 77 | 77 |
| 105 | 88 | 86 | 84 | 82 | 81 | 81 | 80 |
| 110 | 93 | 90 | 88 | 86 | 85 | 85 | 84 |
| 115 | 97 | 95 | 92 | 91 | 89 | 89 | 88 |
| 120 | 102 | 99 | 97 | 95 | 94 | 93 | 92 |
| 125 | 107 | 104 | 101 | 99 | 98 | 97 | 96 |
| 130 | 111 | 108 | 105 | 103 | 102 | 101 | 100 |
| 135 | 116 | 113 | 110 | 108 | 106 | 105 | 104 |
| 140 | 120 | 117 | 114 | 112 | 110 | 109 | 108 |
| 145 | 125 | 122 | 119 | 116 | 114 | 113 | 112 |
| 150 | 130 | 126 | 123 | 121 | 118 | 117 | 116 |
| 155 | 134 | 131 | 127 | 125 | 123 | 121 | 120 |
| 160 | 139 | 135 | 132 | 129 | 127 | 125 | 124 |
| 165 | 144 | 140 | 136 | 133 | 131 | 129 | 128 |
| 170 | 148 | 144 | 141 | 138 | 135 | 133 | 132 |
| 175 | 153 | 149 | 145 | 142 | 140 | 137 | 135 |
| 180 | 158 | 153 | 150 | 146 | 144 | 141 | 139 |
| 185 | 162 | 158 | 154 | 151 | 148 | 145 | 143 |
| 190 | 167 | 163 | 159 | 155 | 152 | 150 | 147 |
| 195 | 172 | 167 | 163 | 160 | 156 | 154 | 151 |
| 200 | 176 | 172 | 168 | 164 | 161 | 158 | 155 |
| 205 | 181 | 176 | 172 | 168 | 165 | 162 | 159 |
| 210 | 186 | 181 | 177 | 173 | 169 | 166 | 163 |
| 215 | 191 | 186 | 181 | 177 | 173 | 170 | 167 |
| 220 | 195 | 190 | 186 | 182 | 178 | 174 | 171 |
| 225 | 200 | 195 | 190 | 186 | 182 | 178 | 175 |
| 230 | 205 | 200 | 195 | 190 | 186 | 183 | 179 |
| 235 | 210 | 204 | 199 | 195 | 191 | 187 | 183 |
| 240 | 214 | 209 | 204 | 199 | 195 | 191 | 187 |
| 245 | 219 | 214 | 209 | 204 | 199 | 195 | 191 |
| 250 | 224 | 218 | 213 | 208 | 204 | 199 | 195 |
| 255 | 229 | 223 | 218 | 213 | 208 | 203 | 199 |
| 260 | 234 | 228 | 222 | 217 | 212 | 207 | 203 |
| 265 | 239 | 233 | 227 | 222 | 216 | 212 | 207 |
| 270 | 243 | 237 | 232 | 226 | 221 | 216 | 211 |

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TEST RESULTS | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 |
| 275 | 248 | 242 | 236 | 231 | 225 | 220 | 215 |
| 280 | 253 | 247 | 241 | 235 | 229 | 224 | 219 |
| 285 | 258 | 252 | 245 | 240 | 234 | 228 | 223 |
| 290 | 263 | 256 | 250 | 244 | 238 | 232 | 227 |
| 295 | 268 | 261 | 255 | 249 | 243 | 237 | 231 |
| 300 | 272 | 266 | 259 | 253 | 247 | 241 | 235 |
| 305 | 277 | 271 | 264 | 258 | 251 | 245 | 239 |
| 310 | 282 | 275 | 269 | 262 | 256 | 249 | 243 |
| 315 | 287 | 280 | 273 | 267 | 260 | 253 | 1247 |
| 320 | 292 | 285 | 278 | 271 | 264 | 258 | 251 |
| 325 | 297 | 290 | 283 | 276 | 269 | 262 | 255 |
| 330 | 302 | 295 | 287 | 280 | 273 | 266 | 259 |
| 335 | 307 | 299 | 292 | 285 | 277 | 270 | 263 |
| 340 | 312 | 304 | 297 | 289 | 282 | 274 | 267 |
| 345 | 317 | 309 | 302 | 294 | 286 | 279 | 271 |
| 350 | 321 | 314 | 306 | 298 | 291 | 283 | 275 |
| 355 | 326 | 319 | 311 | 303 | 295 | 287 | 279 |
| 360 | 331 | 324 | 316 | 308 | 299 | 291 | 283 |
| 365 | 336 | 328 | 320 | 312 | 304 | 295 | 287 |
| 370 | 341 | 333 | 325 | 317 | 308 | 300 | 291 |
| 375 | 346 | 338 | 330 | 321 | 313 | 304 | 295 |
| 380 | 351 | 342 | 335 | 326 | 317 | 308 | 299 |
| 385 | 356 | 348 | 339 | 331 | 322 | 312 | 303 |
| 390 | 361 | 353 | 344 | 335 | 326 | 316 | 307 |
| 395 | 366 | 358 | 349 | 340 | 330 | 321 | 311 |
| 400 | 371 | 363 | 354 | 344 | 335 | 325 | 315 |
| 405 | 376 | 367 | 358 | 349 | 339 | 329 | 319 |
| 410 | 381 | 372 | 363 | 354 | 344 | 333 | 323 |
| 415 | 386 | 377 | 368 | 358 | 348 | 338 | 327 |
| 420 | 391 | 382 | 373 | 363 | 353 | 342 | 331 |
| 425 | 396 | 387 | 377 | 367 | 357 | 346 | 335 |
| 430 | 401 | 392 | 382 | 372 | 361 | 350 | 339 |
| 435 | 406 | 397 | 387 | 377 | 366 | 355 | 343 |
| 440 | 411 | 402 | 392 | 381 | 370 | 359 | 347 |
| 445 | 416 | 407 | 397 | 386 | 375 | 363 | 351 |

TABLE 1
ALTITUDE-CORRECTED FN VALUES FOR WHEAT AT DIFFERENT LABORATORY ALTITUDES (FT. ABOVE SEA LEVEL)

| FALLING NUMBER | ALTITUDE (FT. ABOVE SEA LEVEL) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TEST RESULTS | 2000 | 2500 | 3000 | 3500 | 4000 | 4500 | 5000 |
| 450 | 421 | 411 | 4501 | 391 | 379 | 367 | 355 |
| 455 | 426 | 416 | 406 | 395 | 384 | 372 | 359 |
| 460 | 431 | 421 | 411 | 400 | 388 | 376 | 363 |
| 465 | 436 | 426 | 416 | 405 | 393 | 380 | 367 |
| 470 | 441 | 431 | 421 | 409 | 397 | 384 | 371 |
|  |  |  |  |  |  |  |  |
| 475 | 446 | 436 | 425 | 414 | 402 | 389 | 375 |
| 480 | 451 | 441 | 430 | 419 | 406 | 393 | 379 |
| 485 | 456 | 446 | 435 | 423 | 411 | 397 | 383 |
| 490 | 461 | 451 | 440 | 428 | 415 | 401 | 387 |
| 495 | 466 | 456 | 445 | 433 | 420 | 406 | 391 |
| 500 | 471 | 461 | 450 | 437 | 424 | 410 | 395 |

TABLE 2
TABLE FOR CONVERTING BETWEEN
FALLING NUMBER (FN) AND LIQUEFACTION NUMBER (LN) VALUES

| FN | LN | FN | LN | FN | LN | FN | LN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 70.0 | 300.0 | 100.0 | 120.0 | 130.0 | 75.0 | 160.0 | 54.5 |
| 71.0 | 285.7 | 101.0 | 117.6 | 131.0 | 74.1 | 161.0 | 54.1 |
| 72.0 | 272.7 | 102.0 | 115.4 | 132.0 | 73.2 | 162.0 | 53.6 |
| 73.0 | 260.9 | 103.0 | 113.2 | 133.0 | 72.3 | 163.0 | 53.1 |
| 74.0 | 250.0 | 104.0 | 111.1 | 134.0 | 71.4 | 164.0 | 52.6 |
|  |  |  |  |  |  |  |  |
| 75.0 | 240.0 | 105.0 | 109.1 | 135.0 | 70.6 | 165.0 | 52.2 |
| 76.0 | 230.8 | 106.0 | 107.1 | 136.0 | 69.8 | 166.0 | 51.7 |
| 77.0 | 222.2 | 107.0 | 105.3 | 137.0 | 69.0 | 167.0 | 51.3 |
| 78.0 | 214.3 | 108.0 | 103.4 | 138.0 | 68.2 | 168.0 | 50.8 |
| 79.0 | 206.9 | 109.0 | 101.7 | 139.0 | 67.4 | 169.0 | 50.4 |
|  |  |  |  |  |  |  |  |
| 80.0 | 200.0 | 110.0 | 100.0 | 140.0 | 66.7 | 170.0 | 50.0 |
| 81.0 | 193.5 | 111.0 | 98.4 | 141.0 | 65.9 | 171.0 | 49.6 |
| 82.0 | 187.5 | 112.0 | 96.8 | 142.0 | 65.2 | 172.0 | 49.2 |
| 83.0 | 181.8 | 113.0 | 95.2 | 143.0 | 64.5 | 173.0 | 48.8 |
| 84.0 | 176.5 | 114.0 | 93.8 | 144.0 | 63.8 | 174.0 | 48.4 |
|  |  |  |  |  |  |  |  |
| 85.0 | 171.4 | 115.0 | 92.3 | 145.0 | 63.2 | 175.0 | 48.0 |
| 86.0 | 166.7 | 116.0 | 90.9 | 146.0 | 62.5 | 176.0 | 47.6 |
| 87.0 | 162.2 | 117.0 | 89.6 | 147.0 | 61.9 | 177.0 | 47.2 |
| 88.0 | 157.9 | 118.0 | 88.2 | 148.0 | 61.2 | 178.0 | 46.9 |
| 89.0 | 153.8 | 119.0 | 87.0 | 149.0 | 60.6 | 179.0 | 46.5 |
| 90.0 |  |  |  |  |  |  | 180.0 |
| 91.0 | 150.0 | 120.0 | 85.7 | 150.0 | 60.0 | 46.2 |  |
| 92.0 | 146.3 | 121.0 | 84.5 | 151.0 | 59.4 | 181.0 | 45.8 |
| 93.0 | 142.9 | 122.0 | 83.3 | 152.0 | 58.8 | 182.0 | 45.5 |
| 94.0 | 139.5 | 123.0 | 82.2 | 153.0 | 58.3 | 183.0 | 45.1 |
| 95.0 | 136.4 | 124.0 | 81.1 | 154.0 | 57.7 | 184.0 | 44.8 |
| 96.0 | 133.3 | 125.0 | 80.0 | 155.0 | 57.1 | 185.0 | 44.4 |
| 97.0 | 130.4 | 126.0 | 78.9 | 156.0 | 56.6 | 186.0 | 44.1 |
| 98.0 | 127.7 | 127.0 | 77.9 | 157.0 | 56.1 | 187.0 | 43.8 |
| 99.0 | 125.0 | 128.0 | 76.9 | 158.0 | 55.5 | 188.0 | 43.5 |
|  | 122.4 | 129.0 | 75.9 | 159.0 | 55.0 | 189.0 | 43.2 |

When converting LN to FN :

1. If the LN corresponds to two (2) FN values, use the EVEN FN value. Example: LN 23.3 converts to FN value of 308 .
2. If the LN corresponds to three (3) FN values, use the MIDDLE FN value. Example: LN 16.9 converts to FN value of 495 .
3. If the LN is 13.5 , USE the FN value of 495.
4. If the LN is not listed, use the nearest LN on the table or use the formula " $\mathrm{FN}=(6000 \div \mathrm{LN})+50$ " to calculate the FN equivalent.

Attachment 2

## FGIS PROGRAM DIRECTIVE 9180.38

5-1-97
TABLE 2
TABLE FOR CONVERTING BETWEEN
FALLING NUMBER (FN) AND LIQUEFACTION NUMBER (LN) VALUES

| FN | LN | FN | LN | FN | LN | FN | LN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 190.0 | 42.9 | 220.0 | 35.3 | 250.0 | 30.0 | 280.0 | 26.1 |
| 191.0 | 42.6 | 221.0 | 35.1 | 251.0 | 29.9 | 281.0 | 26.0 |
| 192.0 | 42.3 | 222.0 | 34.9 | 252.0 | 29.7 | 282.0 | 25.9 |
| 193.0 | 42.0 | 223.0 | 34.7 | 253.0 | 29.6 | 283.0 | 25.8 |
| 194.0 | 41.7 | 224.0 | 34.5 | 254.0 | 29.4 | 284.0 | 25.6 |
|  |  |  |  |  |  |  |  |
| 195.0 | 41.4 | 225.0 | 34.3 | 255.0 | 29.3 | 285.0 | 25.5 |
| 196.0 | 41.1 | 226.0 | 34.1 | 256.0 | 29.1 | 286.0 | 25.4 |
| 197.0 | 40.8 | 227.0 | 33.9 | 257.0 | 29.0 | 287.0 | 25.3 |
| 198.0 | 40.5 | 228.0 | 33.7 | 258.0 | 28.8 | 288.0 | 25.2 |
| 199.0 | 40.3 | 229.0 | 33.5 | 259.0 | 28.7 | 289.0 | 25.1 |
|  |  |  |  |  |  |  |  |
| 200.0 | 40.0 | 230.0 | 33.3 | 260.0 | 28.6 | 290.0 | 25.0 |
| 201.0 | 39.7 | 231.0 | 33.1 | 261.0 | 28.4 | 291.0 | 24.9 |
| 202.0 | 39.5 | 232.0 | 33.0 | 262.0 | 28.3 | 292.0 | 24.8 |
| 203.0 | 39.2 | 233.0 | 32.8 | 263.0 | 28.2 | 293.0 | 24.7 |
| 204.0 | 39.0 | 234.0 | 32.6 | 264.0 | 28.0 | 294.0 | 24.6 |
|  |  |  |  |  |  |  |  |
| 205.0 | 38.7 | 235.0 | 32.4 | 265.0 | 27.9 | 295.0 | 24.5 |
| 206.0 | 38.5 | 236.0 | 32.3 | 266.0 | 27.8 | 296.0 | 24.4 |
| 207.0 | 38.2 | 237.0 | 32.1 | 267.0 | 27.6 | 297.0 | 24.3 |
| 208.0 | 38.0 | 238.0 | 31.9 | 268.0 | 27.5 | 298.0 | 24.2 |
| 209.0 | 37.7 | 239.0 | 31.7 | 269.0 | 27.4 | 299.0 | 24.1 |
| 210.0 |  |  |  |  |  |  | 30.0 |
| 211.0 | 37.5 | 240.0 | 31.6 | 270.0 | 27.3 | 300.0 | 24.0 |
| 212.0 | 37.3 | 241.0 | 31.4 | 271.0 | 27.1 | 301.0 | 23.9 |
| 213.0 | 36.8 | 242.0 | 31.3 | 272.0 | 27.0 | 302.0 | 23.8 |
| 214.0 | 36.6 | 244.0 | 31.1 | 273.0 | 26.9 | 303.0 | 23.7 |
| 215.0 | 36.4 | 245.0 | 30.9 | 274.0 | 26.8 | 304.0 | 23.6 |
| 216.0 | 36.1 | 246.0 | 30.6 | 275.0 | 26.7 | 305.0 | 23.5 |
| 217.0 | 35.9 | 247.0 | 30.5 | 277.0 | 26.5 | 306.0 | 23.4 |
| 218.0 | 35.7 | 248.0 | 30.3 | 278.0 | 26.4 | 307.0 | 23.3 |
| 219.0 | 35.5 | 249.0 | 30.2 | 279.0 | 26.3 | 308.0 | 23.3 |
|  |  |  |  |  | 309.0 | 23.2 |  |

When converting LN to FN :

1. If the LN corresponds to two (2) FN values, use the EVEN FN value. Example: LN 23.3 converts to FN value of 308 .
2. If the LN corresponds to three (3) FN values, use the MIDDLE FN value. Example: LN 16.9 converts to FN value of 495 .
3. If the LN is 13.5 , USE the FN value of 495.
4. If the LN is not listed, use the nearest LN on the table or use the formula " $\mathrm{FN}=(6000 \div \mathrm{LN})+50$ " to calculate the FN equivalent.

TABLE 2
TABLE FOR CONVERTING BETWEEN
FALLING NUMBER (FN) AND LIQUEFACTION NUMBER (LN) VALUES

| FN | LN | FN | LN | FN | LN | FN | LN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 310.0 | 23.1 | 340.0 | 20.7 | 370.0 | 18.8 | 400.0 | 17.1 |
| 311.0 | 23.0 | 341.0 | 20.6 | 371.0 | 18.7 | 401.0 | 17.1 |
| 312.0 | 22.9 | 342.0 | 20.5 | 372.0 | 18.6 | 402.0 | 17.0 |
| 313.0 | 22.8 | 343.0 | 20.5 | 373.0 | 18.6 | 403.0 | 17.0 |
| 314.0 | 22.7 | 344.0 | 20.4 | 374.0 | 18.5 | 404.0 | 16.9 |
| 315.0 | 22.6 | 345.0 | 20.3 | 375.0 | 18.5 | 405.0 | 16.9 |
| 316.0 | 22.6 | 346.0 | 20.3 | 376.0 | 18.4 | 406.0 | 16.9 |
| 317.0 | 22.5 | 347.0 | 20.2 | 377.0 | 18.3 | 407.0 | 16.8 |
| 318.0 | 22.4 | 348.0 | 20.1 | 378.0 | 18.3 | 408.0 | 16.8 |
| 319.0 | 22.3 | 349.0 | 20.1 | 379.0 | 18.2 | 409.0 | 16.7 |
| 320.0 | 22.2 | 350.0 | 20.0 | 380.0 | 18.2 | 410.0 | 16.7 |
| 321.0 | 22.1 | 351.0 | 19.9 | 381.0 | 18.1 | 411.0 | 16.6 |
| 322.0 | 22.1 | 352.0 | 19.9 | 382.0 | 18.1 | 412.0 | 16.6 |
| 323.0 | 22.0 | 353.0 | 19.8 | 383.0 | 18.0 | 413.0 | 16.5 |
| 324.0 | 21.9 | 354.0 | 19.7 | 384.0 | 18.0 | 414.0 | 16.5 |
| 325.0 |  |  |  |  |  |  |  |
| 326.0 | 21.8 | 355.0 | 19.7 | 385.0 | 17.9 | 415.0 | 16.4 |
| 327.0 | 21.7 | 356.0 | 19.6 | 386.0 | 17.9 | 416.0 | 16.4 |
| 328.0 | 21.7 | 357.0 | 19.5 | 387.0 | 17.8 | 417.0 | 16.3 |
| 329.0 | 21.6 | 358.0 | 19.5 | 388.0 | 17.8 | 418.0 | 16.3 |
| 330.0 |  | 359.0 | 19.4 | 389.0 | 17.7 | 419.0 | 16.3 |
| 331.0 | 21.4 | 360.0 | 19.4 | 390.0 | 17.6 | 420.0 | 16.2 |
| 332.0 | 21.4 | 361.0 | 19.3 | 391.0 | 17.6 | 421.0 | 16.2 |
| 333.0 | 21.2 | 362.0 | 19.2 | 392.0 | 17.5 | 422.0 | 16.1 |
| 334.0 | 21.1 | 363.0 | 19.2 | 393.0 | 17.5 | 423.0 | 16.1 |
| 335.0 | 21.1 | 365.0 | 19.0 | 394.0 | 17.4 | 424.0 | 16.0 |
| 336.0 | 21.0 | 366.0 | 19.0 | 395.0 | 17.4 | 425.0 | 16.0 |
| 337.0 | 20.9 | 367.0 | 18.9 | 396.0 | 17.3 | 426.0 | 16.0 |
| 338.0 | 20.8 | 368.0 | 18.9 | 398.0 | 17.3 | 427.0 | 15.9 |
| 339.0 | 20.8 | 369.0 | 18.8 | 399.0 | 17.2 | 428.0 | 15.9 |
|  |  |  |  |  | 429.0 | 15.8 |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |

When converting LN to FN:

1. If the LN corresponds to two (2) FN values, use the EVEN FN value. Example: LN 23.3 converts to FN value of 308 .
2. If the LN corresponds to three (3) FN values, use the MIDDLE FN value. Example: LN 16.9 converts to FN value of 495 .
3. If the LN is 13.5 , USE the FN value of 495.
4. If the LN is not listed, use the nearest LN on the table or use the formula " $\mathrm{FN}=(6000 \div \mathrm{LN})+50$ " to calculate the FN equivalent.

## Page 3

Attachment 2

## FGIS PROGRAM DIRECTIVE 9180.38

5-1-97
TABLE 2
TABLE FOR CONVERTING BETWEEN
FALLING NUMBER (FN) AND LIQUEFACTION NUMBER (LN) VALUES

| FN | LN | FN | LN | FN | LN | FN | LN |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 430.0 | 15.8 | 448.0 | 15.1 | 466.0 | 14.4 | 484.0 | 13.8 |
| 431.0 | 15.7 | 449.0 | 15.0 | 467.0 | 14.4 | 485.0 | 13.8 |
| 432.0 | 15.7 | 450.0 | 15.0 | 468.0 | 14.4 | 486.0 | 13.8 |
| 433.0 | 15.7 | 451.0 | 15.0 | 469.0 | 14.3 | 487.0 | 13.7 |
| 434.0 | 15.6 | 452.0 | 14.9 | 470.0 | 14.3 | 488.0 | 13.7 |
|  |  |  |  |  |  |  |  |
| 435.0 | 15.6 | 453.0 | 14.9 | 471.0 | 14.3 | 489.0 | 13.7 |
| 436.0 | 15.5 | 454.0 | 14.9 | 472.0 | 14.2 | 490.0 | 13.6 |
| 437.0 | 15.5 | 455.0 | 14.8 | 473.0 | 14.2 | 491.0 | 13.6 |
| 438.0 | 15.5 | 456.0 | 14.8 | 474.0 | 14.2 | 492.0 | 13.6 |
| 439.0 | 15.4 | 457.0 | 14.7 | 475.0 | 14.1 | 493.0 | 13.5 |
|  |  |  |  |  |  |  |  |
| 440.0 | 15.4 | 458.0 | 14.7 | 476.0 | 14.1 | 494.0 | 13.5 |
| 441.0 | 15.3 | 459.0 | 14.7 | 477.0 | 14.1 | 495.0 | 13.5 |
| 442.0 | 15.3 | 460.0 | 14.6 | 478.0 | 14.0 | 496.0 | 13.5 |
| 443.0 | 15.3 | 461.0 | 14.6 | 479.0 | 14.0 | 497.0 | 13.4 |
| 444.0 | 15.2 | 462.0 | 14.6 | 480.0 | 14.0 | 498.0 | 13.4 |
| 445.0 |  |  |  |  |  |  |  |
| 446.0 | 15.2 | 463.0 | 14.5 | 481.0 | 13.9 | 499.0 | 13.4 |
| 447.0 | 15.2 | 464.0 | 14.5 | 482.0 | 13.9 | 500.0 | 13.3 |

When converting LN to FN:

1. If the LN corresponds to two (2) FN values, use the EVEN FN value. Example: LN 23.3 converts to FN value of 308 .
2. If the LN corresponds to three (3) FN values, use the MIDDLE FN value. Example: LN 16.9 converts to FN value of 495 .
3. If the LN is 13.5 , USE the FN value of 495.
4. If the LN is not listed, use the nearest LN on the table or use the formula " $\mathrm{FN}=(6000 \div \mathrm{LN})+50$ " to calculate the FN equivalent.

## Page 4

TABLE 3
CONVERSION TABLE FOR PREDICTING PERCENT MOISTURE OF WHEAT SAMPLES
GROUND IN THE FN MILL (MODEL 3100)
Predicted Moisture $=1.904606+(0.81661$ x M $)$
Where $\mathrm{M}=$ Motomco 919 Moisture

| Motomco Moisture \% | Predicted <br> Moisture for FN | Motomco Moisture \% | Predicted <br> Moisture for FN |
| :---: | :---: | :---: | :---: |
| $\leq 8.0$ | 8.4 | 12.0 | 11.7 |
| 8.1 | 8.5 | 12.1 | 11.8 |
| 8.2 | 8.6 | 12.2 | 11.9 |
| 8.3 | 8.7 | 12.3 | 11.9 |
| 8.4 | 8.8 | 12.4 | 12.0 |
| 8.5 | 8.8 | 12.5 | 12.1 |
| 8.6 | 8.9 | 12.6 | 12.2 |
| 8.7 | 9.0 | 12.7 | 12.3 |
| 8.8 | 9.1 | 12.8 | 12.4 |
| 8.9 | 9.2 | 12.9 | 12.4 |
| 9.0 | 9.3 | 13.0 | 12.5 |
| 9.1 | 9.3 | 13.1 | 12.6 |
| 9.2 | 9.4 | 13.2 | 12.7 |
| 9.3 | 9.5 | 13.3 | 12.8 |
| 9.4 | 9.6 | 13.4 | 12.8 |
| 9.5 | 9.7 | 13.5 | 12.9 |
| 9.6 | 9.7 | 13.6 | 13.0 |
| 9.7 | 9.8 | 13.7 | 13.1 |
| 9.8 | 9.9 | 13.8 | 13.2 |
| 9.9 | 10.0 | 13.9 | 13.3 |
| 10.0 | 10.1 | 14.0 | 13.3 |
| 10.1 | 10.2 | 14.1 | 13.4 |
| 10.2 | 10.2 | 14.2 | 13.5 |
| 10.3 | 10.3 | 14.3 | 13.6 |
| 10.4 | 10.4 | 14.4 | 13.7 |
| 10.5 | 10.5 | 14.5 | 13.7 |
| 10.6 | 10.6 | 14.6 | 13.8 |
| 10.7 | 10.6 | 14.7 | 13.9 |
| 10.8 | 10.7 | 14.8 | 14.0 |
| 10.9 | 10.8 | 14.9 | 14.1 |
| 11.0 | 10.9 | 15.0 | 14.2 |
| 11.1 | 11.0 | 15.1 | 14.2 |
| 11.2 | 11.1 | 15.2 | 14.3 |
| 11.3 | 11.1 | 15.3 | 14.4 |
| 11.4 | 11.2 | 15.4 | 14.5 |
| 11.5 | 11.3 | 15.5 | 14.6 |
| 11.6 | 11.4 | 15.6 | 14.6 |
| 11.7 | 11.5 | 15.7 | 14.7 |
| 11.8 | 11.5 | 15.8 | 14.8 |
| 11.9 | 11.6 | 15.9 | 14.9 |

TABLE 4
BOILING POINT OF DISTILLED WATER (DEGREES C) REFERENCED TO BAROMETRIC PRESSURE

Source: CRC Handbook of Chemistry and Physics, 50th Ed.
(Boiling Point Values were Corrected for the Effect of Water Vapor-Saturated Headspace)

| Barometric Pressure |  |  | Boiling <br> Point <br> $(\mathrm{C})$ |
| :---: | :---: | :---: | :---: |
| $(\mathrm{mm} \mathrm{Hg})$ | (in. Hg) | kPa |  |
| 680 | 26.77 | 90.66 | 97.5 |
| 685 | 26.97 | 91.33 | 97.7 |
| 690 | 27.17 | 91.99 | 97.9 |
| 695 | 27.36 | 92.66 | 98.1 |
| 700 | 27.56 | 93.33 | 98.3 |
| 705 | 27.76 | 93.99 | 98.5 |
| 710 | 27.95 | 94.66 | 98.7 |
| 715 | 28.15 | 95.33 | 98.9 |
| 720 | 28.35 | 95.99 | 99.1 |
| 725 | 28.54 | 96.66 | 99.3 |
| 730 | 28.74 | 97.33 | 99.5 |
| 735 | 28.94 | 97.99 | 99.7 |
| 740 | 29.13 | 98.66 | 99.8 |
| 745 | 29.33 | 99.32 | 100.0 |
| 750 | 29.53 | 99.99 | 100.2 |
| 755 | 29.72 | 100.66 | 100.4 |
| 760 | 29.92 | 101.32 | 100.6 |
| 765 | 30.12 | 101.99 | 100.8 |
| 770 | 30.31 | 102.66 | 100.9 |
| 775 | 30.51 | 103.32 | 101.1 |
| 780 | 30.71 | 103.99 | 101.3 |
| 790 | 30.91 | 104.66 | 101.5 |
| 800 | 31.10 | 105.32 | 101.7 |
|  | 31.30 | 105.99 | 101.8 |
| 1.50 | 106.66 |  |  |

$\mathrm{kPa}=$ Kilopascal
$\mathrm{mm}=$ Millimeter
$\mathrm{in}=$ Inch
$\mathrm{C}=$ Centigrade


[^0]:    1/ Use rounding procedures in the Grain Inspection Handbook, book II, section 1.16.

